

CFEM

$$\int_D w \left(\frac{d\sigma_T}{dt} + \nabla \cdot q - Q \right) dV + \int_{\partial D_p} w (\bar{q} - q \cdot n) dS = 0$$

CFEM
WRS

cancel this weak form

$$w(\nabla \cdot q) = \nabla \cdot (wq) - (\nabla w) \cdot q$$

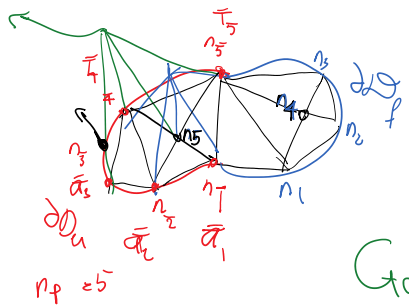
$$\int_D w(\nabla \cdot q) dV = \int_D \nabla \cdot (wq) dV - \int_D (\nabla w) \cdot q dV$$

$$\int_D w \nabla \cdot q dV = \int_{\partial D} (wq) \cdot n dS - \int_D (\nabla w) \cdot q dV$$

$$\int_D w \left(\frac{d\sigma_T}{dt} - Q \right) dV + \int_{\partial D_p} w q \cdot n dS - \int_D \nabla w \cdot q dV + \int_{\partial D_p} w \bar{q} dS = 0$$



$$\int_D w \left(\frac{d\sigma_T}{dt} - Q \right) dV - \int_D \nabla w \cdot q dV + \int_{\partial D_p} w \bar{q} dS = 0$$



$$T = [N_1 \ N_2 \ \dots \ N_{n_p}] \begin{bmatrix} a_1 \\ \vdots \\ a_{n_p} \end{bmatrix}$$

we have n_p d.o.f
 $\rightarrow n_p$ weights $\begin{bmatrix} w_1 \\ \vdots \\ w_{n_p} \end{bmatrix}$

Galerkin: $w = N_f$

$$\begin{bmatrix} w_1 \\ w_2 \\ \vdots \\ w_{n_p} \end{bmatrix} = \begin{bmatrix} N_1 \\ \vdots \\ N_{n_p} \end{bmatrix}$$

as can be seen $\begin{bmatrix} w_1 \\ \vdots \\ w_{n_p} \end{bmatrix} = 0 \quad \forall x \in \partial D_p$

CFEM weak statement

$$\int_D w \left(\frac{d\sigma_T}{dt} - Q \right) dV - \int_D \nabla w \cdot q dV + \int_{\partial D_p} w \bar{q} dS = 0$$

$q = \dots (kT, \nabla T) \dots$ constitutive eqn

Fourier heat law $q = -k \nabla T$
 symmetric, positive definite 2nd order tensor

$$\int_D w \left(\frac{d\sigma_T}{dt} - Q \right) dV - \int_D \nabla w \cdot q dV + \int_{\partial D_p} w \bar{q} dS = 0$$

$$\int_D \left(\rho \frac{d^2 u}{dt^2} - \rho \right) dV + \int_D \nabla w \cdot \nabla T dV + \int_{\partial \Omega_p} \omega \bar{q} dS = 0 \quad (1)$$

Weak statement

Discretize:

$$T = \underbrace{N_p}_{\Phi} a_p + \underbrace{N_q}_{\Psi} a_q$$

Galarkin

$$w = \begin{bmatrix} a_1 \\ \vdots \\ a_n \end{bmatrix} = \begin{bmatrix} N_1 \\ \vdots \\ N_n \end{bmatrix} = N_p^T$$

$$T = N_p a_p + N_q a_q \rightarrow \nabla T = \underbrace{\begin{bmatrix} \frac{\partial N_p}{\partial x_1} & \dots & \frac{\partial N_p}{\partial x_2} \end{bmatrix}}_{B_p} \begin{bmatrix} a_p \\ a_q \end{bmatrix}$$

$$+ \underbrace{\begin{bmatrix} \frac{\partial N_q}{\partial x_1} & \dots & \frac{\partial N_q}{\partial x_2} \end{bmatrix}}_{B_q} \begin{bmatrix} a_1 \\ \vdots \\ a_n \end{bmatrix}$$

$$B \in L_m N \quad (\text{here } L_m = \nabla)$$

$$\nabla w = B_p^T$$

$$\int_D \left(\rho \frac{d^2 u}{dt^2} - \rho \right) dV + \int_D \nabla w \cdot \nabla T dV + \int_{\partial \Omega_p} \omega \bar{q} dS = 0$$

$\int_D \rho \frac{d^2 u}{dt^2} dV \rightarrow (N_p a_p + N_q a_q)$
 $\int_D \nabla w \cdot \nabla T dV \rightarrow (B_p a_p + B_q a_q)$
 $\int_{\partial \Omega_p} \omega \bar{q} dS \rightarrow N_q$

$$\int_D N_p^T \frac{d^2 (N_p a_p + N_q a_q)}{dt^2} dV + \int_D B_p^T K (B_p a_p + B_q a_q) dV = \int_D N_p^T \rho dV - \int_{\partial \Omega_p} N_q^T \bar{q} dS$$

$$1) \frac{d^2 T(x,t)}{dt^2} = \frac{d^2 (N_p a_p(t) + N_q a_q(t))}{dt^2} = N_p \ddot{a}_p + N_q \ddot{a}_q$$

2) take up terms to the RHS

$$\left(\int_D (N_p^T C_p N_p) dV \right) \ddot{a}_p + \left(\int_D (B_p^T K B_p) dV \right) a_p = \int_D N_p^T \rho dV - \int_{\partial \Omega_p} N_q^T \bar{q} dS$$

$\int_D (N_p^T C_p N_p) dV$ Mass matrix
 $M_{pp} = M = \text{mass matrix}$
 $\int_D (B_p^T K B_p) dV$ stiffness matrix
 $K_{pp} = K$
 $\int_D N_p^T \rho dV$ Force from Natural/Neumann BC
 F_N
 $-\int_{\partial \Omega_p} N_q^T \bar{q} dS$ prescribed BC
 $-F_D$ Drained F_D

(2a)

$$M \ddot{a} + K a = F_N + F_D - F_D \quad \text{solid Mechanics}$$

$$M_{pp} = M = \int_D N_p^T C_p N_p dV$$

$$a = a_p$$

$$M \ddot{a} + C \dot{a} + K a = \dots$$

$$M = \int_D (N_p^T C_p N_p) dV$$

$$M_R = M = \int_V N_p^T C_V N_p dV \quad a = a_f$$

$$K_f = K = \int_V B_p^T D B_p dV$$

material / section property here = κ

$$F_r = \int_V N_p^T Q dV \quad F_w = \int_S N_p^T \bar{f} dS$$

$$F_D = \left(\int_V B_p^T D B_p dV \right) a_p + \left(\int_V N_p^T C_V N_p dV \right) \dot{a}_p$$

$$F_D = M_{pp} \dot{a}_p + K_{pp} a_p$$

$$M = \int_V (N_p^T \rho N_p) dV$$

$$C = \int_V N_p^T \eta N_p dV$$

damping

$$K = \int_V B_p^T D B_p dV$$

$$L_m = \epsilon(\cdot) \quad \epsilon(N)$$

$$D = C \quad \text{stiffness matrix} \quad (2b)$$

system of ODEs (semi-discrete form)

space is discretized
but time still is not

Global approach OR node/dof centered

Local approach or element centered

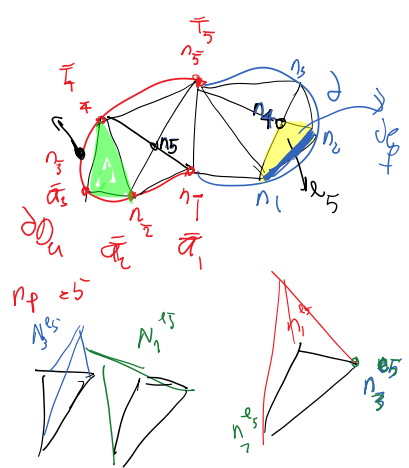
We take care of the contributions of each element to M, K, and the right hand side

$$k_e^e = \int_e B_e^T D B_e dV \quad M_e^e = \int_e N_e^T C_V N_e dV$$

$$f_r^e = \int_e N_e^T Q dV \quad f_w^e = \int_e N_e^T \bar{q} dS$$

$$f_D^e = M_e^e \dot{a}^e + K_e^e a^e \quad \text{local}$$

$$F_D = M_{pp} \dot{a}_p + K_{pp} a_p \quad \text{global}$$



$$N^e = [N_1^e \quad N_2^e \quad N_3^e]$$

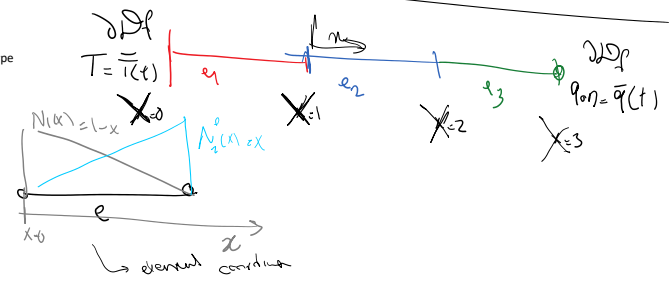
$$B^e = \nabla N^e = \begin{bmatrix} N_{1,1} & N_{2,1} & N_{3,1} \\ N_{1,2} & N_{2,2} & N_{3,2} \end{bmatrix}$$

Example of 1D heat conduction

Color coding is done based on the element not the BC type

For simplicity all elements are identical

$$k_e = 1, \quad C_V = 1$$

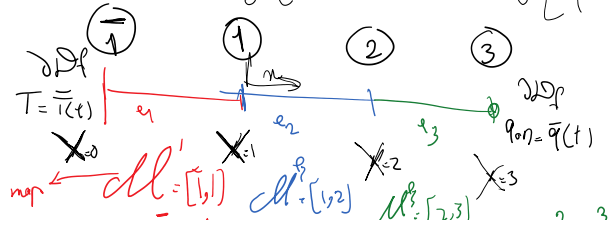


$$N = [N_1 \quad N_2] = [1-x \quad x]$$

$$B = \nabla N = N_{,x} = [-1 \quad 1]$$

$$K^e = \int_e B^T D B dx = \int_0^1 \begin{bmatrix} -1 \\ 1 \end{bmatrix} k \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} dx = \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

$$M^e = \int_e N^T C_V N dx = \int_0^1 \begin{bmatrix} 1-x \\ x \end{bmatrix} 1 \begin{bmatrix} 1-x & x \end{bmatrix} dx = \frac{1}{6} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix}$$



$$n_f = 3$$

$$n_p = 1$$

x_0 x_1 x_2 x_3 $y_0 = \bar{q}(t)$ $n_p = 1$
 $\text{map} \leftarrow d11 = \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix}$ $d12 = \begin{bmatrix} 1 & 2 \\ 1 & 2 \end{bmatrix}$ $d13 = \begin{bmatrix} 2 & 3 \\ 2 & 3 \end{bmatrix}$
 $K^1 = \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix}$ $K^2 = \begin{bmatrix} 1 & 2 \\ 1 & 2 \end{bmatrix}$ $K^3 = \begin{bmatrix} 1 & 2 \\ 1 & 2 \end{bmatrix}$
 $M^1 = \frac{1}{\delta} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix}$ $M^2 = \frac{1}{\delta} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix}$ $M^3 = \frac{1}{\delta} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix}$

$$K_{3 \times 3} = \begin{bmatrix} 1 & 1 & 1 \\ 1 & 1 & 1 \\ 1 & 1 & 1 \end{bmatrix}$$

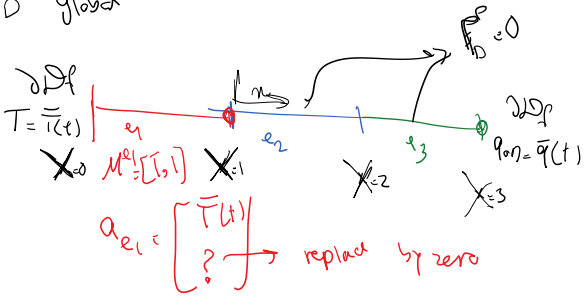
$$M = \frac{1}{\delta} \begin{bmatrix} 2+2 & 1 & 1 \\ 1 & 2+2 & 1 \\ 1 & 1 & 2 \end{bmatrix}$$

$$K = \begin{bmatrix} 2 & 1 & 0 \\ -1 & 2 & -1 \\ 1 & -1 & 1 \end{bmatrix}$$

$$M = \begin{bmatrix} 4 & 1 & 1 \\ 1 & 4 & 1 \\ 1 & 1 & 2 \end{bmatrix}$$

$F_r = 0$ no source term

F_D global



$$f^a = M^q a_{e1} + K^{e1} a_{e1} = \frac{1}{\delta} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix} \begin{bmatrix} \dot{\bar{T}} \\ 0 \end{bmatrix} + \begin{bmatrix} 1 & 1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} \bar{T} \\ 0 \end{bmatrix}$$

$$= \begin{bmatrix} \frac{1}{\delta} \dot{\bar{T}} + \bar{T} & \bar{T} \\ \frac{1}{\delta} \dot{\bar{T}} - \bar{T} & 1 \end{bmatrix}$$

$$F_D = \begin{bmatrix} \frac{1}{\delta} \dot{\bar{T}} - \bar{T} & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$$