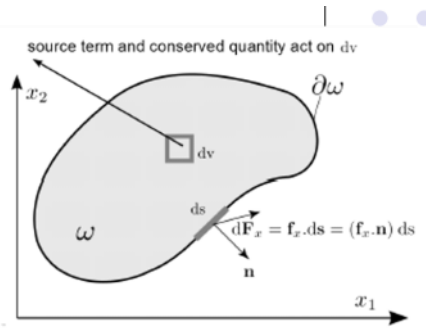


For a general conservation law let:

- f_t : conserved quantity = temporal flux
- f_x : total outward spatial flux
- r : source term

then the balance law for dynamics reads:



$$\forall \omega \subset \mathcal{D} \wedge \forall t: \int_{\omega} r \, dv - \int_{\partial\omega} f_x \cdot ds = \int_{\omega} r \, dv - \int_{\partial\omega} (f_x \cdot n) \, ds = \frac{d}{dt} \int_{\omega} f_t \, dv \quad (13)$$

- Application of divergence theorem on the flux term yields,

$$\int_{\partial\omega} f_x \cdot n \, ds = \int_{\omega} \nabla \cdot f_x \, dv$$

- By taking $\frac{\partial(\cdot)}{\partial t}$ inside the integral in the balance law we have,

$$\forall \omega \subset \mathcal{D} \int_{\omega} \left\{ \frac{\partial f_t}{\partial t} + \nabla \cdot f_x - r \right\} dv = 0$$

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- Since $\omega \subset \mathcal{D}$ is arbitrary, by using the localization theorem we obtain the strong form of the problem,

$$\frac{\partial f_t}{\partial t} + \nabla \cdot f_x - r = 0 \quad \text{that is in 3D} \quad f_{t,t} + f_{1,1} + f_{2,2} + f_{3,3} = r$$

where f_1, f_2, f_3 are the components of the spatial flux $f_x = [f_1, f_2, f_3]$.

- **Quasilinear systems:** If f_t or f_x depend on the unknown vector u in addition of x and t the system of PDE is nonlinear. We can write it in the form,

$$f_{t,t} + f_{1,1} + f_{2,2} + f_{3,3} = r \quad \Leftrightarrow \quad A_t u_{,t} + A_1 u_{,1} + A_2 u_{,2} + A_3 u_{,3} = 0 \quad \text{where}$$

$$A_t(\mathbf{u}, \mathbf{x}, t) := \nabla_{\mathbf{u}} f_t \quad \text{that is} \quad (A_t)_{ij} = \frac{\partial (f_t)_i}{\partial u_j} \quad \text{similarly}$$

$$A_i(\mathbf{u}, \mathbf{x}, t) := \nabla_{\mathbf{u}} f_{i,j} \quad \text{that is} \quad (A_i)_{ij} = \frac{\partial (f_i)_j}{\partial u_j} \quad i \leq 3$$

If A_t and A_i ($i \leq 3$) do not depend on u the system is linear or semi-linear; otherwise it is quasi-linear.

$$\dot{q} + \nabla \cdot f_q = 0$$

1-arrang 2-arrang

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Euler's eqn

scalar

$$q = \begin{bmatrix} f_p \\ f_v \\ f_p v_1 \\ f_p v_2 \\ f_p v_3 \end{bmatrix}$$

vector



- If further \mathbf{u} is chosen to be the temporal flux \mathbf{f}_t is the primary field \mathbf{u} then $\mathbf{A}_t = \mathbf{I}$ and we have,

$$\mathbf{u}_{,t} + \mathbf{f}_{1,1} + \mathbf{f}_{2,2} + \mathbf{f}_{3,3} = r \quad \Leftrightarrow \quad \mathbf{u}_{,t} + \mathbf{A}_1 \mathbf{u}_{,1} + \mathbf{A}_2 \mathbf{u}_{,2} + \mathbf{A}_3 \mathbf{u}_{,3} = 0$$

- For a scalar system clearly \mathbf{A}_i are scalar.
- In 1D $\mathbf{f}_2 = \mathbf{f}_3 = 0$ ($\mathbf{A}_2 = \mathbf{A}_3 = 0$).
- Consider a general **scalar quasilinear conservation law**,

$$\begin{aligned} u_{,t} + f_{1,1}(u) + f_{2,2}(u) + f_{3,3}(u) &= r & \Leftrightarrow \\ u_{,t} + g_1(u, x, t)u_{,1} + g_2(u, x, t)u_{,2} + g_3(u, x, t)u_{,3} &= 0 \end{aligned}$$

which for 1D it simply is

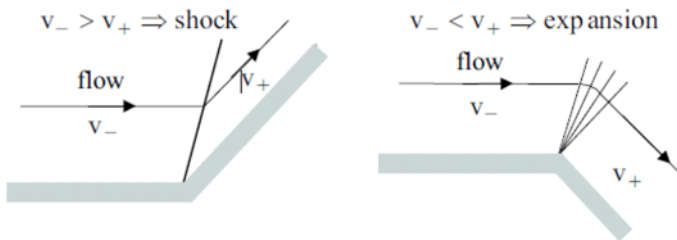
$$u_{,t} + f_{,x}(u) = r \quad \Leftrightarrow \quad u_{,t} + g(u, x, t)u_{,x} = 0$$

- If $g(u, x, t)$ depends on u the solution behavior for u can be very different from linear/semilinear first order systems and may exhibit **shocks and expansion waves**.

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Quasi-linear first order equations and why shocks are formed:

Motivation: **Shock and expansion waves:**



Example: **Burger's equation**

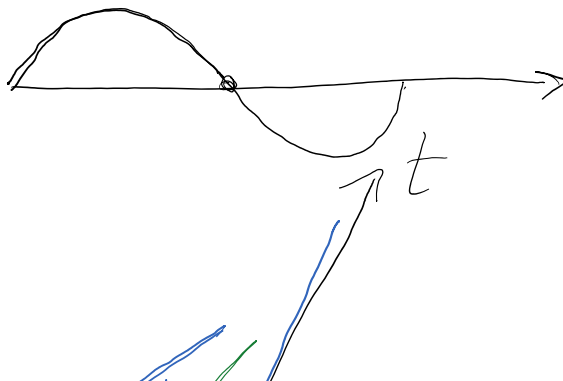
$$\frac{\partial u}{\partial t} + \frac{\partial}{\partial x} \left(\frac{1}{2} u^2 \right) = 0, \quad \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} = 0.$$

spatial flux

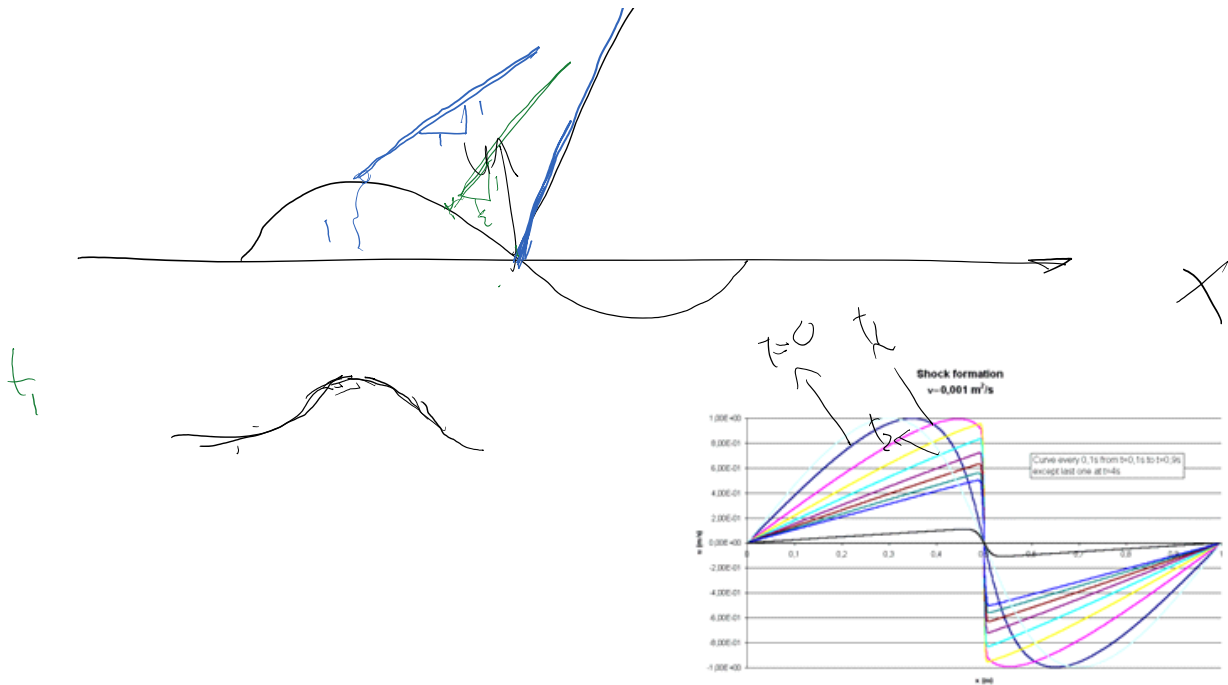
$$f(u) = u^2/2 \quad \Rightarrow \quad g(u) = f'(u) = u$$

$$\frac{\partial u}{\partial t} + \underbrace{A(u)}_{A(u)=u} \frac{\partial u}{\partial x} = 0$$

speed in advection equation



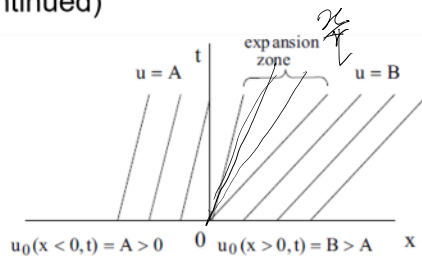
$u(0)$
IC



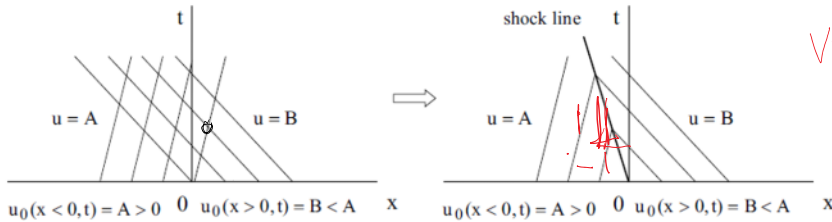
Example: **Burger's equation** (continued)

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} = 0, \quad -\infty < x < \infty, t > 0$$

$$u(x, 0) = \begin{cases} A, & x < 0 \\ B, & x \geq 0. \end{cases}$$



invalid



valid

Figure IV.6 If the signal travels slower at the rear than at the front ($A < B$), the characteristic network is under-determined. Conversely, if the signal travels faster at the rear than in front ($A > B$), the characteristic network is over determined: the tentative network that displays intersecting characteristics, has to be modified to show a discontinuity line (curve).

Source: [Loret, 2008]

Question: How to get the speed of shock?

- Quasi-linear PDE ($q(u)$)

temporal flux

$$\frac{\partial u}{\partial t} + \frac{\partial q}{\partial x} = 0$$

spatial flux

- We define the jump operator

$$[\cdot] = (\cdot)_+ - (\cdot)_-$$

where + and - refer to the two sides for the jump

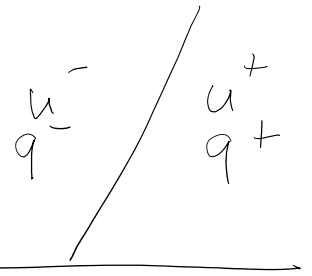
$$[\cdot] = (\cdot)_+ - (\cdot)_-$$

where + and - refer to the two sides for the jump.

- If $X_s(t)$ is the position of the jump manifold in time, its equation is given by

$$\frac{dX_s(t)}{dt} = \frac{[q]}{[u]} = \frac{q_+ - q_-}{u_+ - u_-}$$

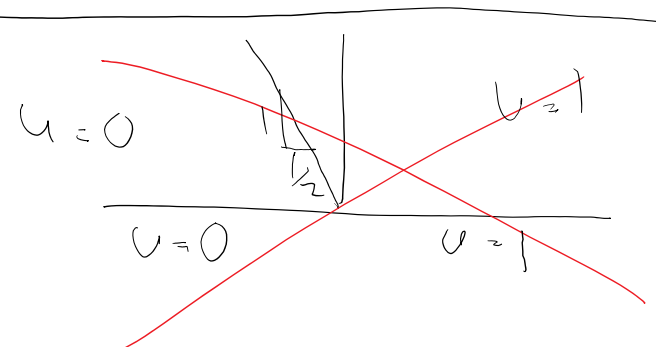
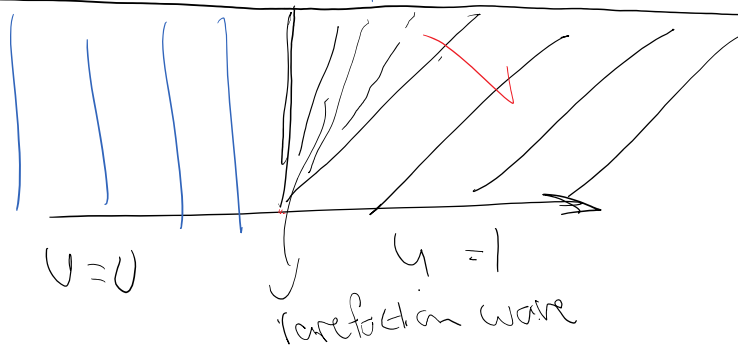
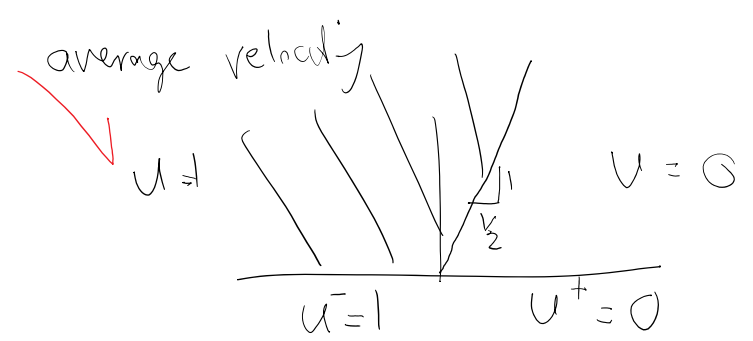
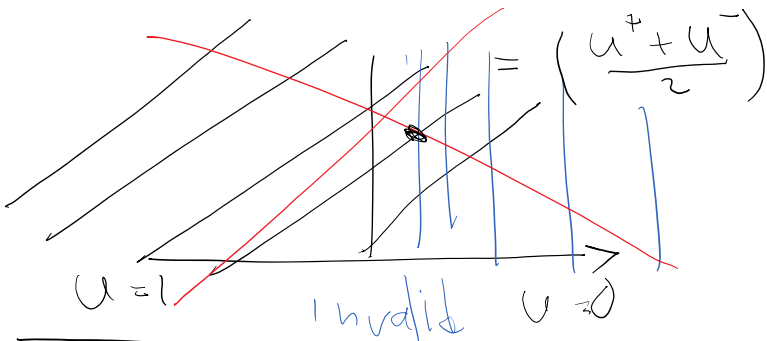
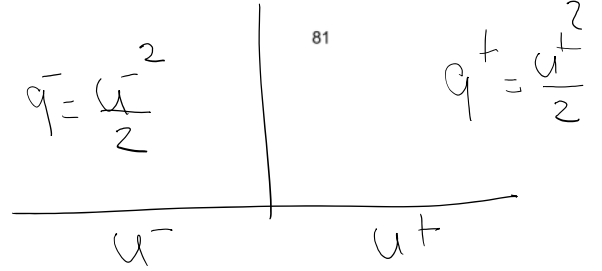
This is called the jump or Rankine-Hugoniot condition.



Source: [Loret, 2008]

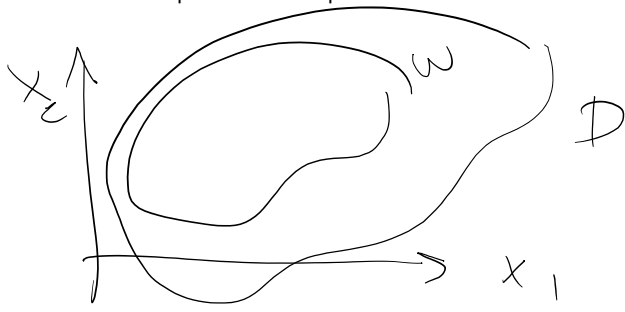
Burgers eqn

speed of shock = $\frac{\frac{u^+{}^2}{2} - \frac{u^-{}^2}{2}}{u^+ - u^-}$



IK exact
approximate

Where does the equation for the speed of shock come from?



$$\frac{d}{dt} \int_{\Omega} f_{\pm} dv = - \int_{\partial\Omega} f_{\pm} n_{\pm} ds + \int_{\Omega} r_{\pm} dv$$

balanced quantity
advective spatial flux

$$\frac{d}{dt} \int_{\Omega} f_{\pm} dv + \int_{\partial\Omega} f_{\pm} n_{\pm} ds = \int_{\Omega} r_{\pm} dv$$

steady state

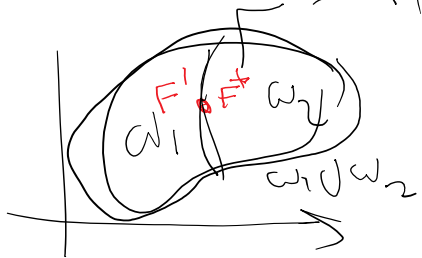
Writing this balance laws in space time



$$\int_{\partial\Omega} F_{\pm} N_{\pm} dS = \int_{\Omega} r_{\pm} dV$$

spacetime flux

$$F = \begin{bmatrix} p \\ f_{\pm} \end{bmatrix} \quad N = \begin{bmatrix} n_x \\ n_t \end{bmatrix}$$



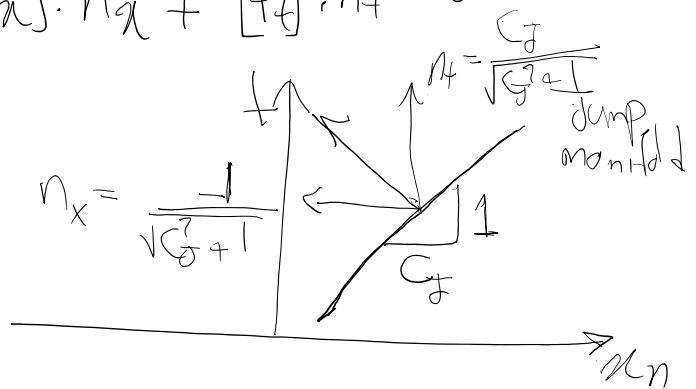
Jump condition

Jump condition: $[F] \cdot N = 0$

$$\begin{bmatrix} [p] \\ [f_{\pm}] \end{bmatrix} \cdot \begin{bmatrix} n_x \\ n_t \end{bmatrix} = 0 \Rightarrow [p] \cdot n_x + [f_{\pm}] \cdot n_t = 0$$

$G_J = \text{speed of jump} = ?$

$$[p] \left(\frac{-1}{\sqrt{G^2 + 1}} \right) + [f_{\pm}] \cdot \frac{G}{\sqrt{G^2 + 1}} = 0$$



$$C_J = \frac{[f_x] \cdot \tilde{n}_x}{[f_t]}$$

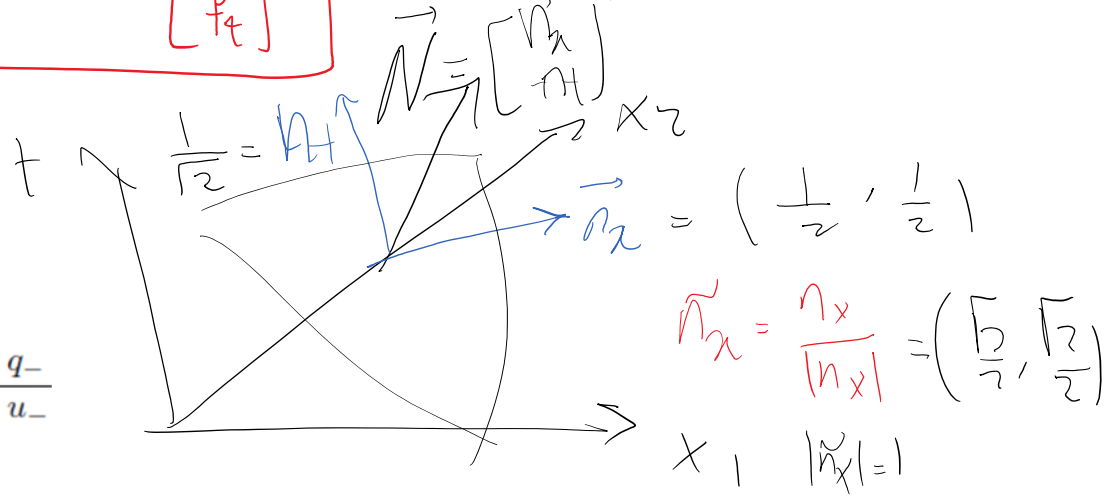
$$|\tilde{n}_x| = 1$$

$$|n_x|^2 + |n_t|^2 = 1$$

Does it match

$$C_J = \frac{dX_s(t)}{dt} = \frac{[q]}{[u]} = \frac{q_+ - q_-}{u_+ - u_-}$$

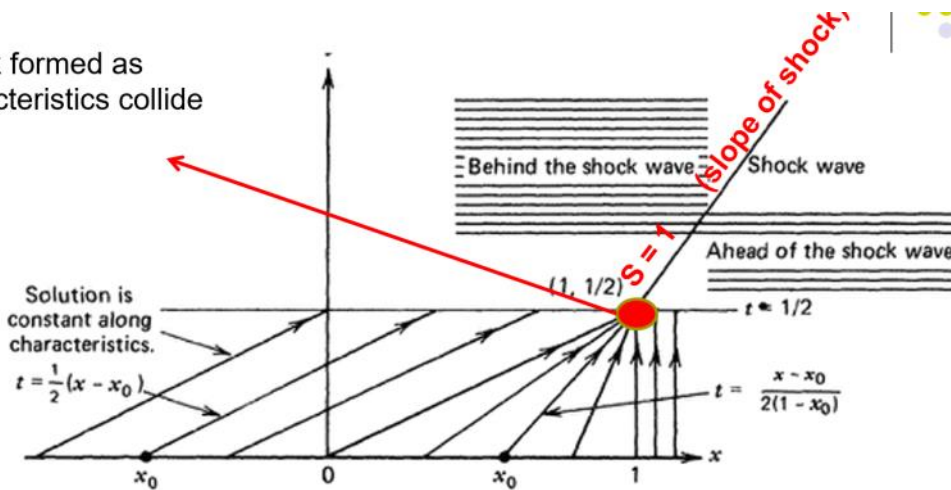
$$u + q_x = 0$$



- Jumps cannot propagate with arbitrary speed and we cannot have arbitrary jumps in f_x and f_t . Their jumps are related and determines the speed of jump
- For semi-linear sys. Of convs law the speeds of discontinuities are the wave speeds.

Example:

Shock formed as characteristics collide



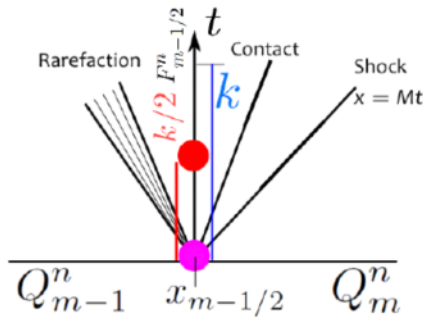
$$S = \frac{f(u_R) - f(u_L)}{u_R - u_L} = \frac{0 - 1}{0 - 1} = 1$$

$$\text{Flux} = u^2$$

Source: [Farlow, 2012, lesson 28]

1.5.1 Introduction and Motivation

- In many instances we need to find the flux on an extruded facet in space time. For example, in Finite Volume (FV) method:
 - PDE from the balance law is $q_{,t}(x, t) + f_{,x}(q(x, t)) = 0$.
 - We need to calculate spatial flux $f(q(x, t))$ average
 - which for the boundary between cells $m-1$ and m is represented / approximated by numerical flux $F_{m-1/2}^n$.
- We solve a **local** problem with initial conditions Q_{m-1}^n, Q_m^n to find the value for solution at position in the figure. This is called a **Riemann solution**. Sometimes, we opt to choose substitutes or approximations for Riemann solution as it solution is too expensive or not available.



- The Riemann solution set-up in the figure is for the Euler's equation, where for constant states at the left and right we obtain different regions in spacetime with distinct solutions.

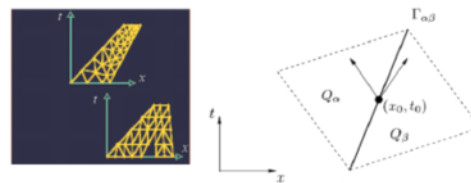
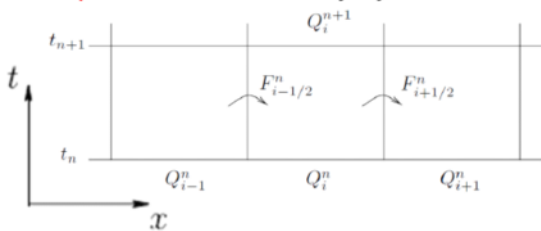
1. PDE type classification and analytical methods:

1.5 Riemann solutions: linear and nonlinear hyperbolic PDES

- The **red dot** is the position where we position we may seek the solution for a FV scheme, Discontinuous Galerkin (DG), etc. (to represent the average of flux on the cell boundary).
- For quasilinear systems we may have complex solutions with rarefaction waves and shocks.
- This explains why we may use approximate Riemann solutions.
- Riemann solution may be required for nonvertical directions as well.

Vertical position: FV method & majority of DG methods

Nonvertical position: Unstructured spacetime grids



1. PDE type classification and analytical methods:

1.5 Riemann solutions: linear and nonlinear hyperbolic PDES

Approach 1: Using characteristic values (linear PDEs)

1.5.2 Approach 1: Using characteristic values (linear PDEs)

- Characteristic values $\omega = \mathbf{L}\mathbf{q}$ are constant (or solved as ODEs) along characteristic directions
- Primary field \mathbf{q} has n components

$$\mathbf{q} = \begin{bmatrix} q_1 \\ q_2 \\ \vdots \\ q_n \end{bmatrix}$$

- **Transfer to characteristic variables and directions** For the system on \mathbf{q} we transfer to characteristics by,

$$\text{For } \dot{\mathbf{q}} + \mathbf{A}\mathbf{q}_{,x} = 0 \quad \mathbf{L}\mathbf{A} = \mathbf{L}\mathbf{\Lambda}, \quad \text{for } \mathbf{\Lambda} = \text{diag}(c_1, \dots, c_n)$$

ω

- Eigenvalues (wave speeds) are $c_1 \leq c_2 \leq \dots \leq c_n$

1. PDE type classification and analytical methods:

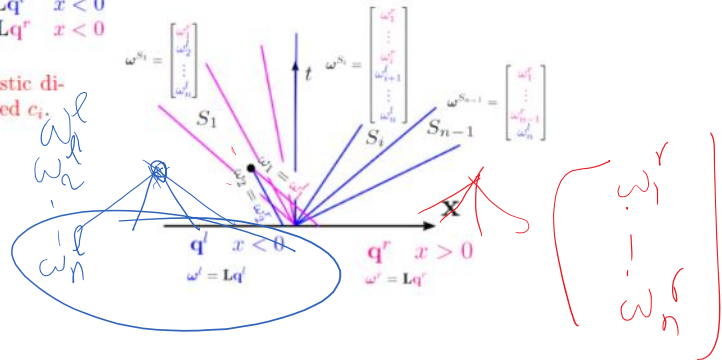
1.5 Riemann solutions: linear and nonlinear hyperbolic PDES

- Initial conditions are

$$q(x, 0) = q_0 = \begin{cases} q^l & x < 0 \\ q^r & x > 0 \end{cases} \Rightarrow \omega(x, 0) = \omega_0 = \begin{cases} \omega^l = Lq^l & x < 0 \\ \omega^r = Lq^r & x > 0 \end{cases}$$

- Characteristic values $\omega = Lq$ are constant along characteristic directions; i.e., ω_i is constant along the wave moving with speed c_i .
- Thus, for sample segments S^1, S^i, S^{n-1} we have,

$$\omega^{S_1} = \begin{bmatrix} \omega_1^l \\ \omega_2^l \\ \vdots \\ \omega_n^l \end{bmatrix} \quad \omega^{S_i} = \begin{bmatrix} \omega_1^r \\ \vdots \\ \omega_i^r \\ \vdots \\ \omega_{i+1}^r \\ \vdots \\ \omega_n^l \end{bmatrix} \quad \omega^{S_{n-1}} = \begin{bmatrix} \omega_1^r \\ \vdots \\ \omega_{n-1}^r \\ \omega_n^l \end{bmatrix}$$



- Transfer back to primary variables and fluxes is by using L:

$$q^{S_i} = L^{-1}\omega^{S_i}$$

Approach 2: Using Jump shapes from right eigenvectors (linear PDEs)

1.5.3 Approach 2: Using Jump shapes determined by right eigenvectors

- Again, consider the system,

$$\dot{q} + Aq_x = 0$$

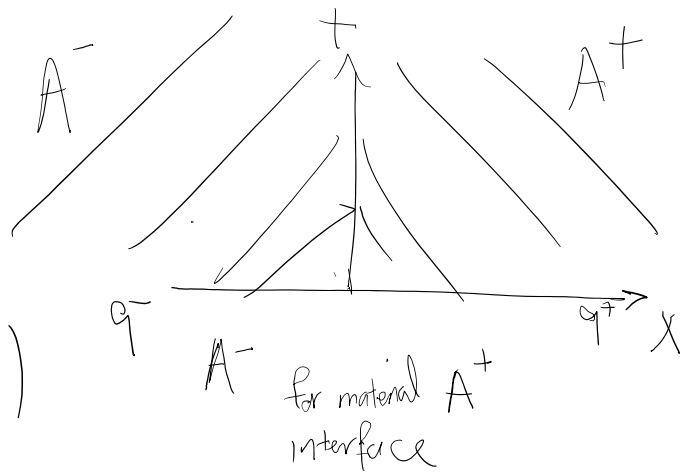
$$\frac{dq}{dt} + p(q) \frac{dx}{dt} = 0 \quad f_t + \nabla \cdot f_x = S$$

1D first & semi-linear

$$C_J = \frac{[f_x]}{[f_t]} = \frac{[Aq]}{[q]}$$

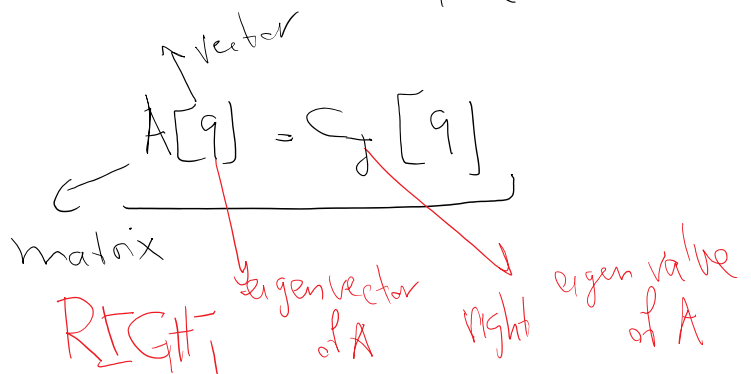
Jump speed $C_J = \frac{[Aq]}{[q]}$

if $C_J \neq 0$ then $[A] = 0$
 (we deal with A^- $C_J < 0$
 A^+ $C_J > 0$)



call it A:

$$C_J = \frac{[Aq]}{[q]} = \frac{A[q]}{[q]}$$



For $c \neq 0$, right eigenvectors are the shapes of the discontinuity across a discontinuity line and corresponding eigenvalues are the speed of discontinuity.

For $c = 0$:

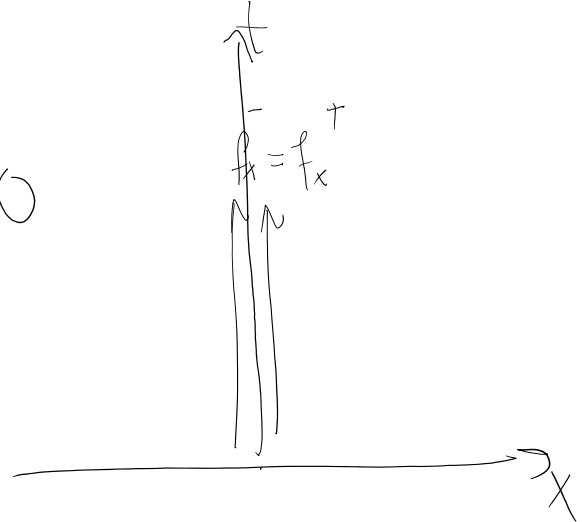
$$[f_x] \cdot n_x = c [f_t]$$

$$[Aq] = c [f_t] \quad c = 0$$

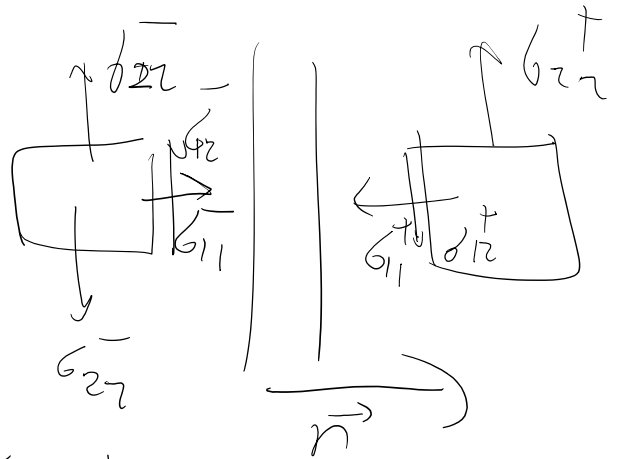
$$\boxed{[Aq] = 0}$$

$$A^- q^- = A^+ q^+$$

$$f_{x,n}^- = f_{x,n}^+$$



$$\begin{pmatrix} \epsilon_{11} & \sigma_{12} \\ \sigma_{21} & \sigma_{22} \end{pmatrix} \begin{pmatrix} 1 \\ a \end{pmatrix} = 0$$



net flux $\begin{bmatrix} \sigma_{11} \\ \sigma_{21} \end{bmatrix}$ continuous $[\sigma_{22}] \neq 0$

$$\begin{bmatrix} \epsilon_{11} & \epsilon_{12} \\ \epsilon_{21} & \epsilon_{22} \end{bmatrix}$$

$$b = \rho_{xx} \epsilon_{xx} \epsilon$$

$$[\epsilon] \neq 0$$

$$[v] = 0$$

$$[p] \neq 0$$

$$p = pV$$