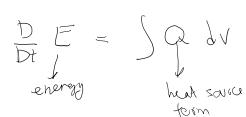
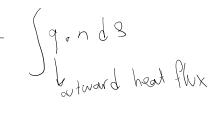
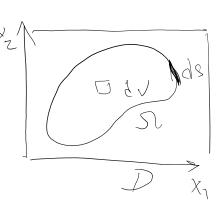
DG2010/01/13

Monday, January 13, 2020

We start by comparing CFEM and DG formulation of thermal heat conduction:







C = SedV Jenergy lansity e=CrT Volumetric heat capacity (other contributions to)

BCTOW SQW - Sq. n/8 no advedion (D(CT) & V -) QdV = /-7-9 d V

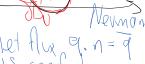


(CT)+7-9-Q] dv=0 D (CT)+ 7-9-Q=0

Now we define all the residuals pertained to PDE and BCs:

$$R_{i} = \frac{D_{i}}{D_{i}}(CT) + \nabla \cdot q - Q$$

$$R_{i} = T - T$$



Rs = 9-9-

T(X,0) = G(X)

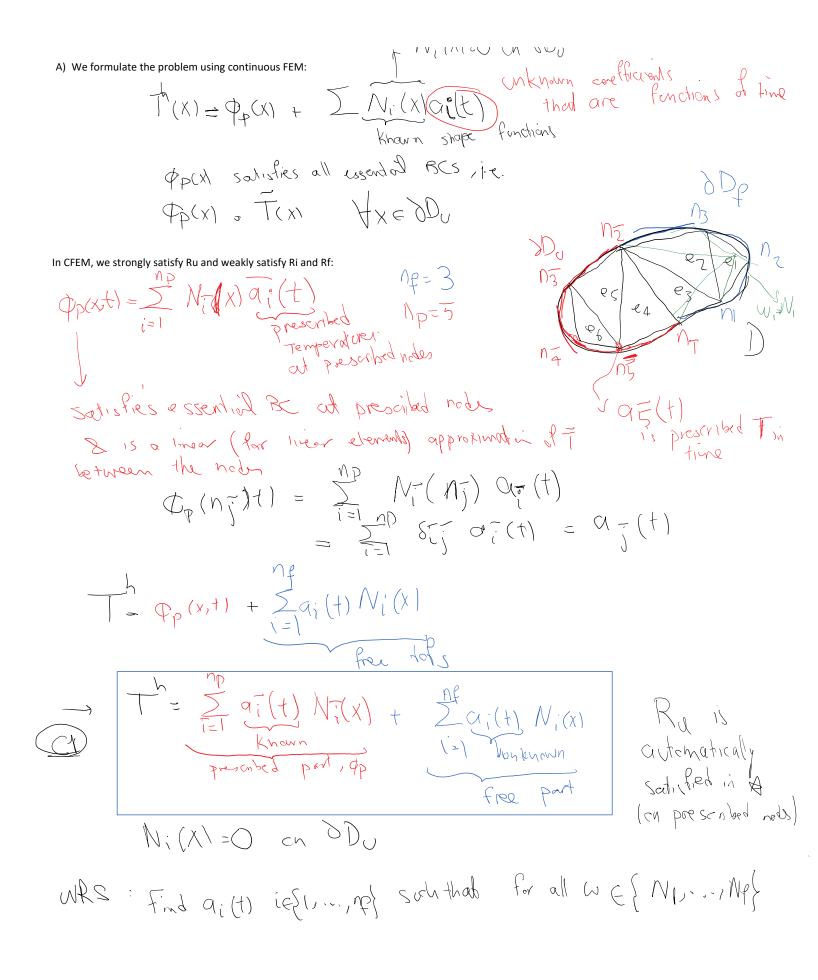
Next, we discretize this IBVP with two different methods (discretization is in space only). This is what we call semi-discrete form:

Ma+Ka=F

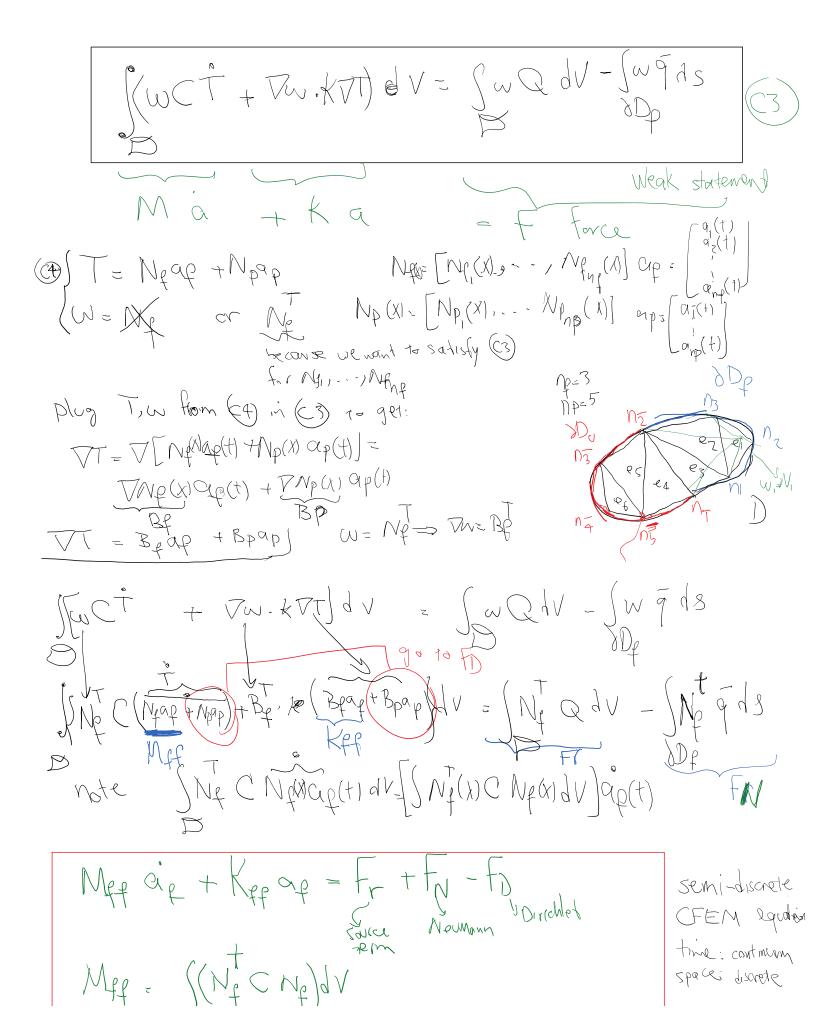
discretized in spaced, not discretized in time (semi-discrete

A) We formulate the problem using continuous FEM:

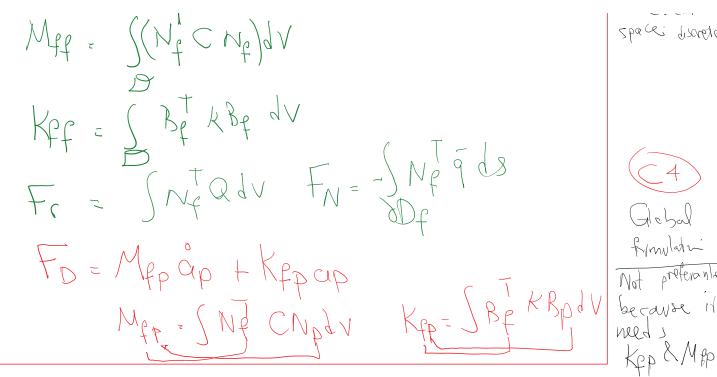
N; (XI co on 800 unknown coefficients.



Juridu + Jurgos. 0 $\int_{\mathcal{A}} \omega \left(\frac{\partial}{\partial t} (CT) + \frac{\partial}{\partial t} Q - Q \right) dt + \int_{\mathcal{A}} \omega \left(\frac{\partial}{\partial t} - Q \cdot n \right) ds = 0$ I since 9 = - KVT (Fairer hed low) Oth or be Use divergence therein to balance derivatives V. (wg) = Vw.9 + WV39 Ju V-9 dv = J.V. (oug) dv - J. Vw.9 dv = Swandy - SJw.gdV Jwkt-2) 11 + Jw(9-9,n) 18 + [-57~9dv + 5~9~~15.] =0 Jact - 7w9 - wa) dv + Sw9 + [sw1.nd8 - [w9.nd8]] 9= KT | and egnabere w= N; = O on D by noting we get



DG Page 4



Kep & Mpp

Local (element-level) calculations circumvent the calculation of global

Mfp and Kfp: