

Some examples for the jump condition

Elastostatics

$$f = -\sigma$$

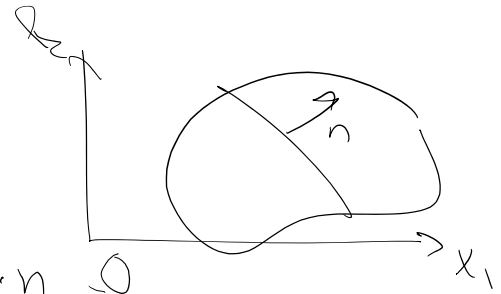
$$r = \rho b$$

jump condition is $(\sigma^+ - \sigma^-) \cdot n = 0$

action reaction law

$$\sigma^+ \cdot n^- = \sigma^- \cdot n^+$$

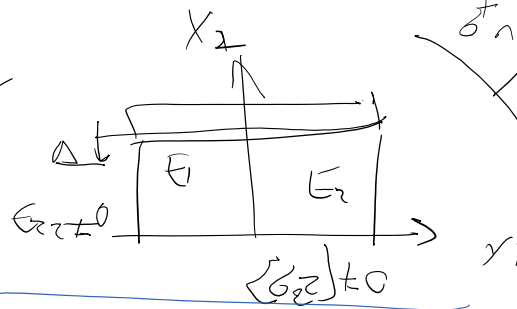
$$\sigma^+ \cdot n^+ = \sigma^- \cdot n^-$$



Tractions are equal, but of opposite direction.

Clearly, we do not have the condition that

$$[\sigma] = 0$$



Jump conditions are more interesting for dynamic problems.

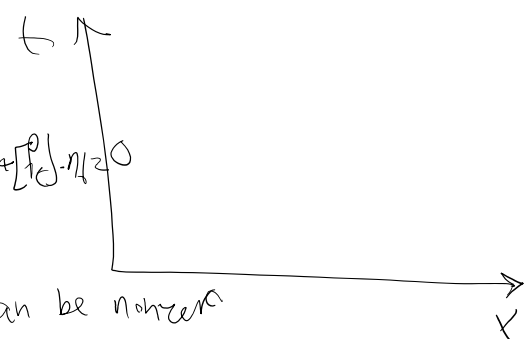
For a dynamic problem:

$$F = \begin{bmatrix} f_x \\ f_t \end{bmatrix}$$

$$[F] \cdot N = 0 \Leftrightarrow [f_x] \cdot n_x + [f_t] \cdot n_t = 0$$

So both

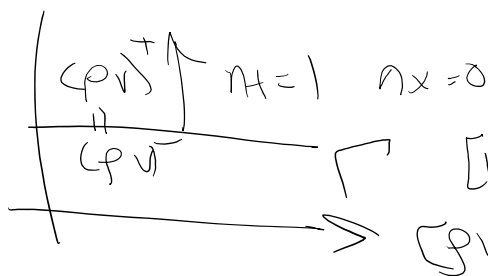
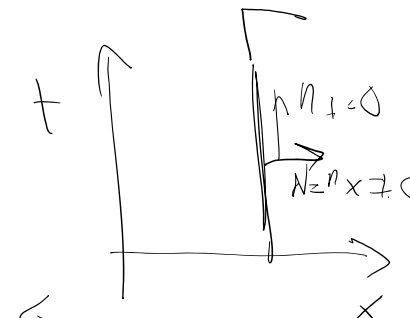
$[f_x] n_x$ & $[f_t] n_t$ can be nonzero



Example from Elastodynamics

$$\begin{aligned} f_x &= -\sigma \\ f_t &= p = \rho v \end{aligned}$$

$$-\left[\sigma \right] \cdot n_x + [p] n_t = 0$$



$$[p] \cdot n_t = [p] = 0$$

$$[\rho v] = 0$$

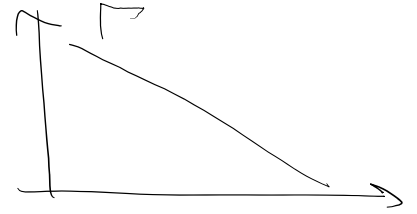
tractions are equal & opposite sign

$$[\sigma] \cdot n_x = 0$$

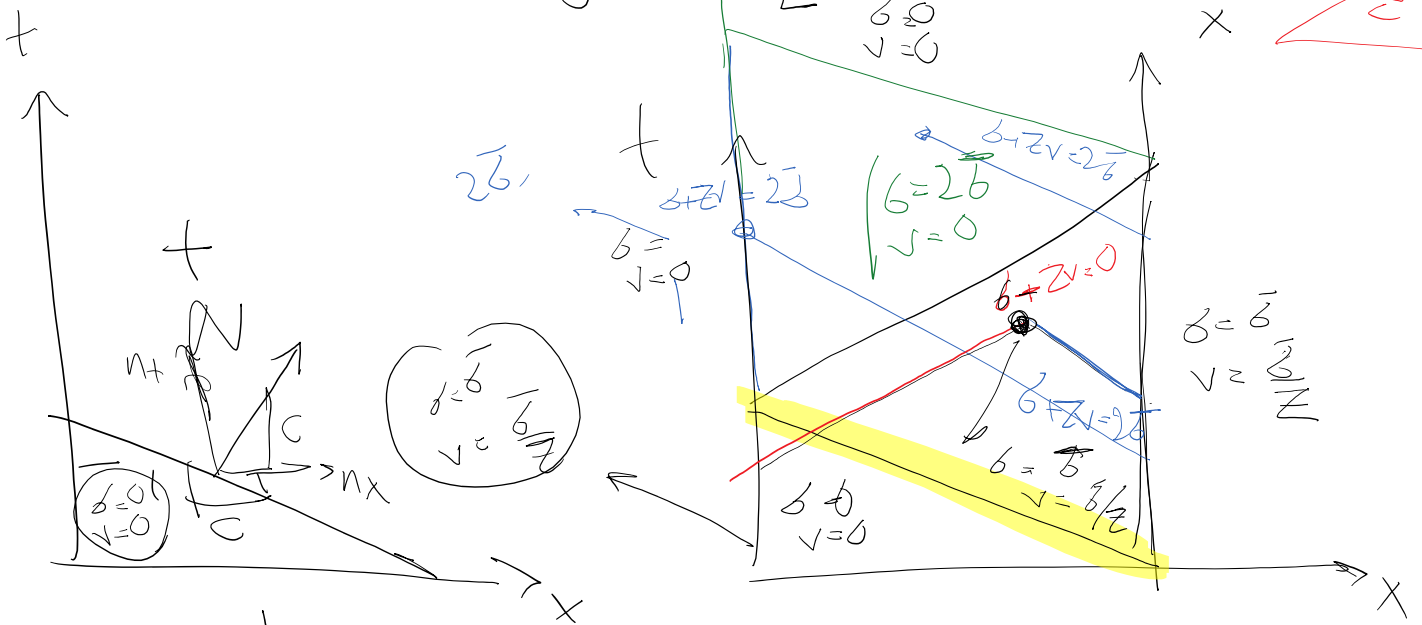
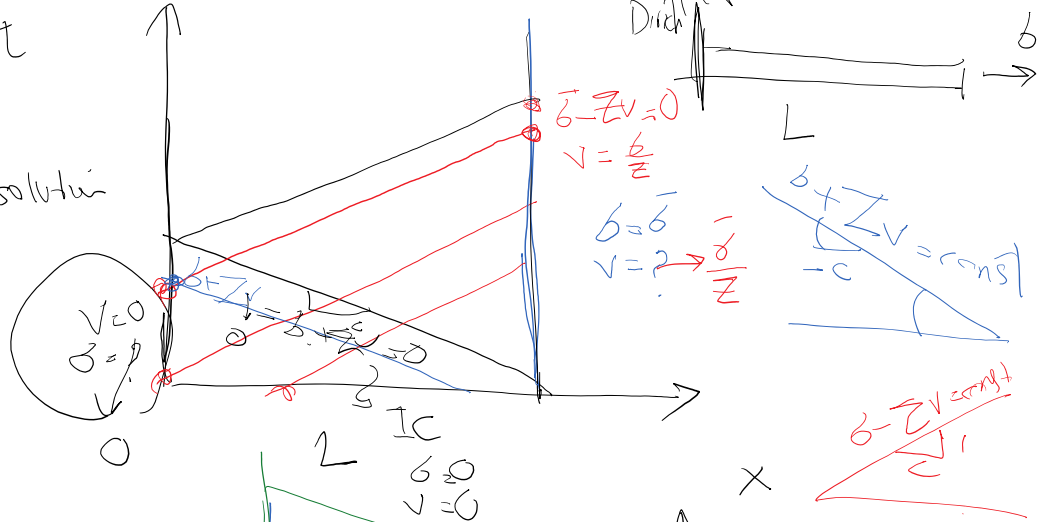
$$1 \rightarrow [pV] = 0$$

c) $n_x, n_t \neq 0$

the speed of these jump manifolds is not arbitrary



we want to find spacetime solution of δ & v



$$n_x = \frac{1}{\sqrt{1+c^2}}$$

$$n_t = \frac{c}{\sqrt{1+c^2}}$$

$$\begin{aligned} [G] &= \delta \\ [N] &= \frac{\delta}{c} \\ \rightarrow [P] &= \rho \frac{\delta}{z} \end{aligned}$$

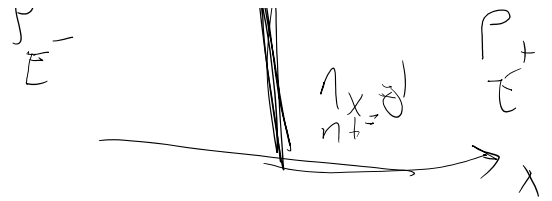
$$\begin{aligned} -[G] \cdot n_x + [P] n_t &= \\ -\delta \frac{1}{\sqrt{1+c^2}} + \frac{\rho \delta}{c} \frac{c}{\sqrt{1+c^2}} &= 0 \\ &= 0 \quad \checkmark \end{aligned}$$

Material interface



Maximal interface

only traces $-\llbracket \llbracket \cdot \rrbracket \cdot n_x = 0$
are continuous

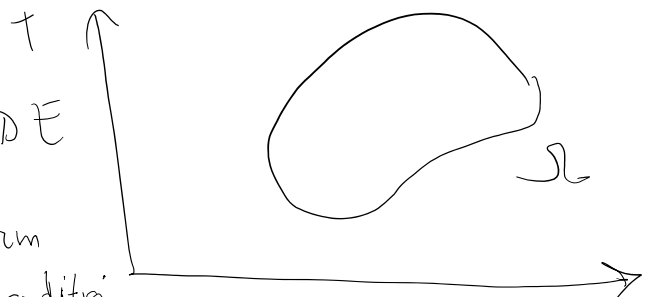


$\llbracket P \rrbracket$ can be nonzero ($\llbracket U \rrbracket = 0$ by continuity)
but if $\rho \neq \rho^+$ then $\llbracket P \rrbracket \neq 0$

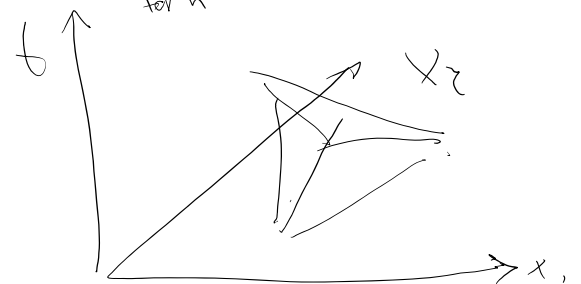
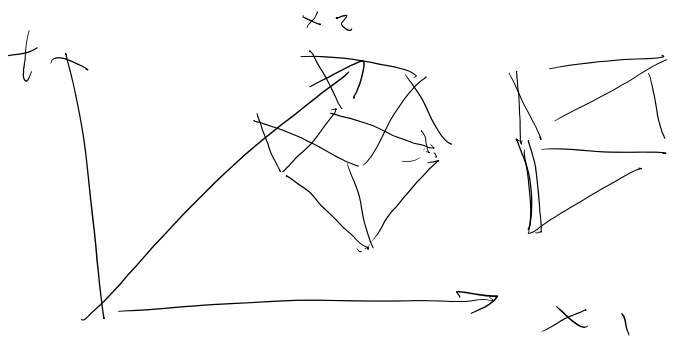
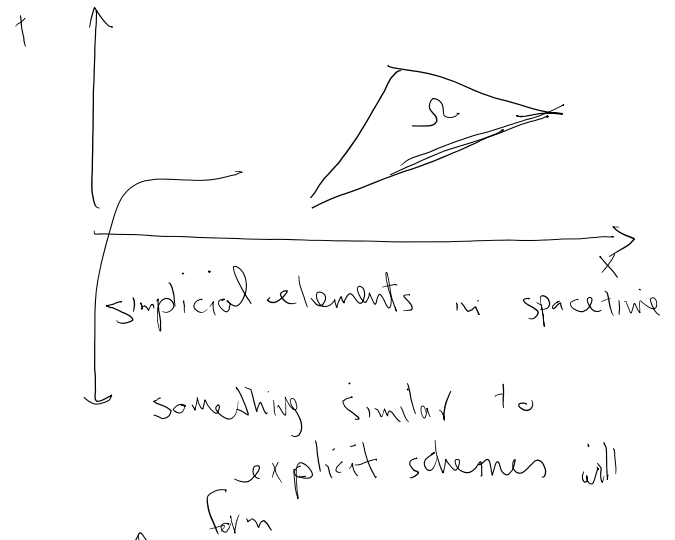
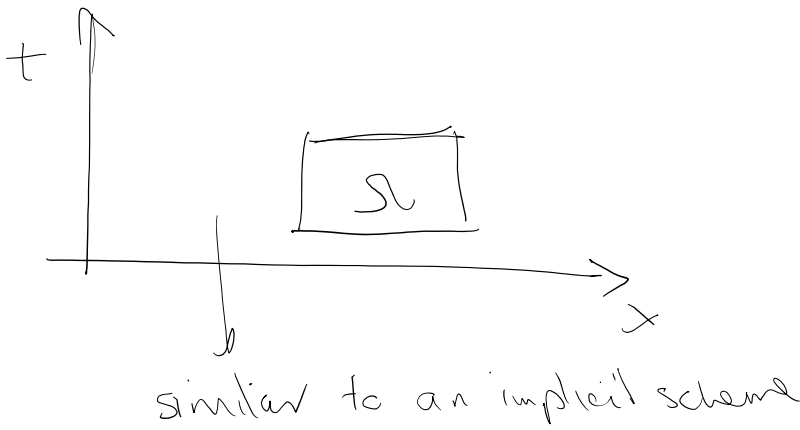
Formulating a spacetime discontinuous Galerkin method:

$\nabla_{st} \cdot F - r = 0$ strong form PDE

$\llbracket F \rrbracket \cdot N = \llbracket F_n \rrbracket \cdot n_x + \llbracket P \rrbracket \cdot A_t = 0$ jump condition



→ for spacetime methods we have two general classes of elements \mathcal{R}



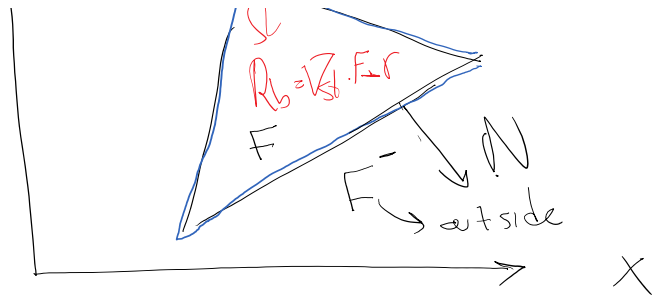
$R_b = \nabla_{st} \cdot F - r$

$R_b = \nabla_{st} \cdot F - r$

$$R_b = \int_{\Omega} \mathbf{V}_b \cdot \mathbf{F} - r$$

$$R_b = [\mathbf{F}] \cdot \mathbf{N}$$

$$[\mathbf{F}] = [\mathbf{F}^- - \mathbf{F}^+] \cdot \mathbf{N}$$

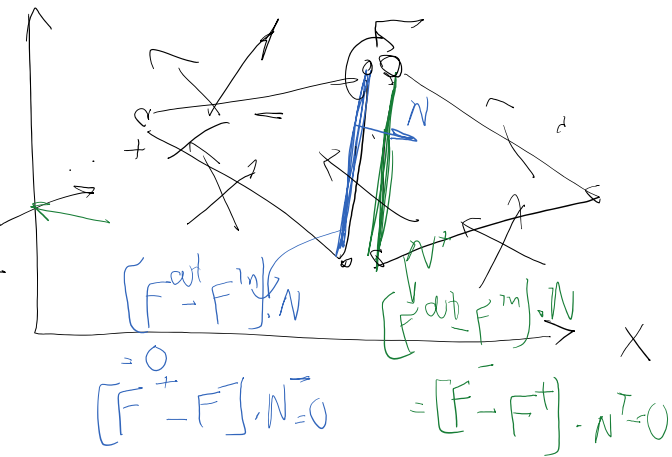


$$[\mathbf{F}^{ext} - \mathbf{F}^{int}] \cdot \mathbf{N} = 0$$

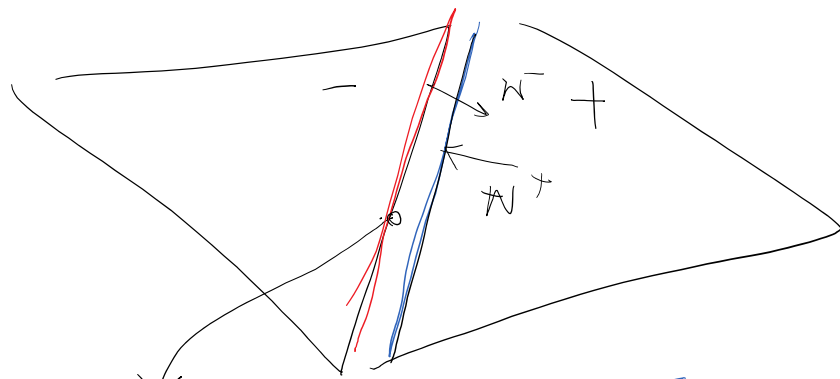
\mathbf{F}^{ext} → exterior trace of element
 \mathbf{F}^{int} → interior trace

$$[\mathbf{F}^{ext} - \mathbf{F}] \cdot \mathbf{N} = 0$$

1
 are coupled through Γ



$$[\mathbf{F}(\mathbf{F}^{int}, \mathbf{F}^{ext}) - \mathbf{F}] \cdot \mathbf{N} = 0$$



if $\mathbf{F}^{*-} = \mathbf{F}^{*+} = \mathbf{F}^*$
 almost always the case

$$[\mathbf{F}^{*+}(\mathbf{F}^-, \mathbf{F}^+) - \mathbf{F}^-] \cdot \mathbf{N}^- = 0 \quad (1)$$

$$[\mathbf{F}^{*-}(\mathbf{F}^-, \mathbf{F}^+) - \mathbf{F}^+] \cdot \mathbf{N}^+ = 0 \quad (2)$$

add them

$$[\mathbf{F}^+ - \mathbf{F}^-] \cdot \mathbf{N}^- = 0$$

F^* is a physically correct solution that is determined from the conditions of the interface on left & right.

— (*) option can be used to define many interesting target values

fracture $\leftarrow \rightarrow$ always
 ED: $F_{in} \cdot [v]$ \parallel $[G] \cdot n_x = 0$
 $[v] \neq 0$ For example if we have crack opening or frictional slide

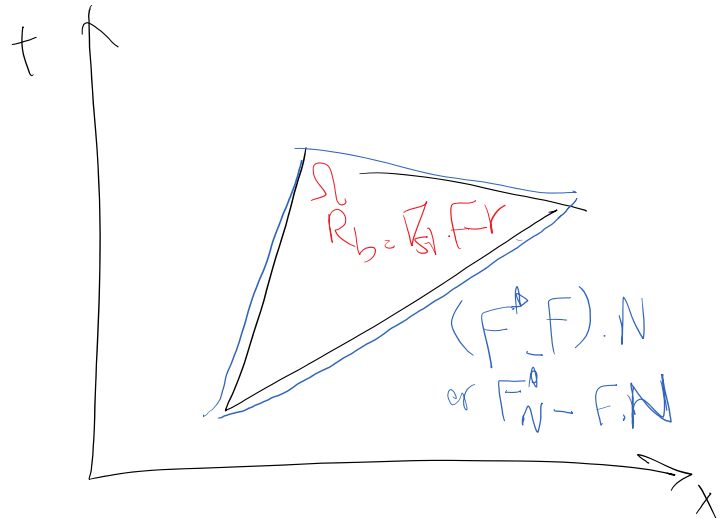
the equations are

$$R_b = V_{ST} \cdot F - r$$

$$R_f = (F^* - F) \cdot N$$

or $F_N^* - F \cdot N$

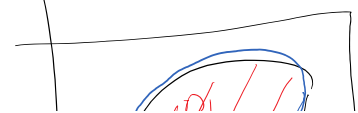
F is interior face
 F^* ($F_0, F_{outside}$)



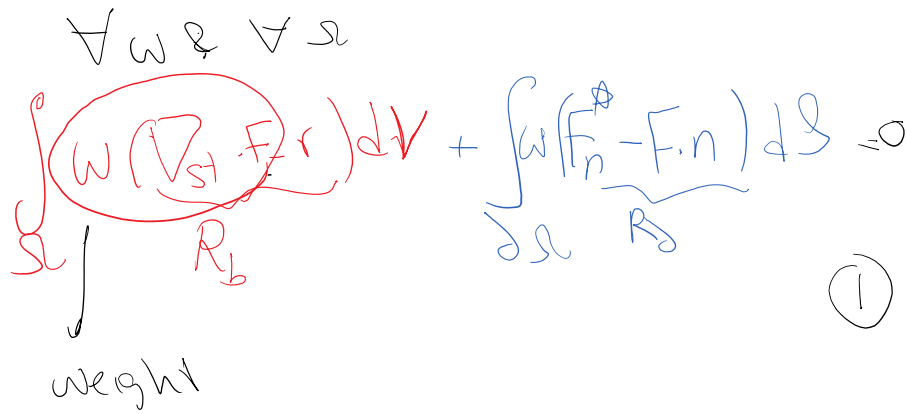
So, the use of star values in the context of FV and DG methods is more flexible than simply writing $(F^+ - F^-) \cdot N = 0$. It provides many options for the definition of numerical flux (for example average, Riemann and various forms of approximate Riemann fluxes) and physical conditions at an interface (contact, friction, resistive sheet, ...)

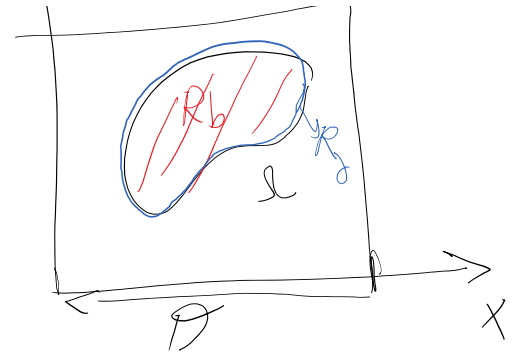
^{WR} Continuum weak statement.

F is the weak solution if for any $S_b \subseteq \mathbb{R}^d \times [0, T]$
 $\forall \omega \in \mathcal{V} \quad \forall \Omega$



$\forall \omega \in \forall \Omega$

$$\int_{\Omega} \underbrace{\omega (\nabla_{st} \cdot F - r)}_{\text{weight}} dV + \int_{\partial \Omega} \omega (F_n - F \cdot n) dS = 0 \quad (1)$$




We use the Gauss theorem to get to the weak statement.

$$\omega \nabla_{st} \cdot F = \nabla_{st} \cdot \omega F - \nabla_{st} \omega \cdot F$$

$$\int_{\Omega} \omega \nabla_{st} \cdot F dV = \int_{\Omega} \nabla_{st} \cdot \omega F dV - \int_{\Omega} \nabla_{st} \omega \cdot F dV =$$

$$\int_{\partial \Omega} \omega F \cdot N dS - \int_{\Omega} \nabla_{st} \omega \cdot F dV$$

plug this into (1)

$$\left(\int_{\partial \Omega} \omega F \cdot N dS - \int_{\Omega} \nabla_{st} \omega \cdot F dV \right) - \int_{\Omega} \omega r dV + \int_{\partial \Omega} \omega F_n dS - \int_{\partial \Omega} \omega F \cdot n dS = 0$$

$\int_{\Omega} \omega \nabla_{st} \cdot F$

continuous weak statement is

$$\forall \Omega, \forall \omega \in V$$

$$\int_{\Omega} (-\nabla_{st} \omega \cdot F - \omega r) dV + \int_{\partial \Omega} \omega (F_n - F \cdot n) dS = 0$$



(a) $\int_{\partial \Omega} (F \cdot N) dS = \int_{\Omega} r dV$ balance law



$$\omega = 1 \quad \nabla_{\mathcal{S}} \omega = 0 \quad \rightarrow \quad -\int r \, dV + \int F_n \, dS = 0$$

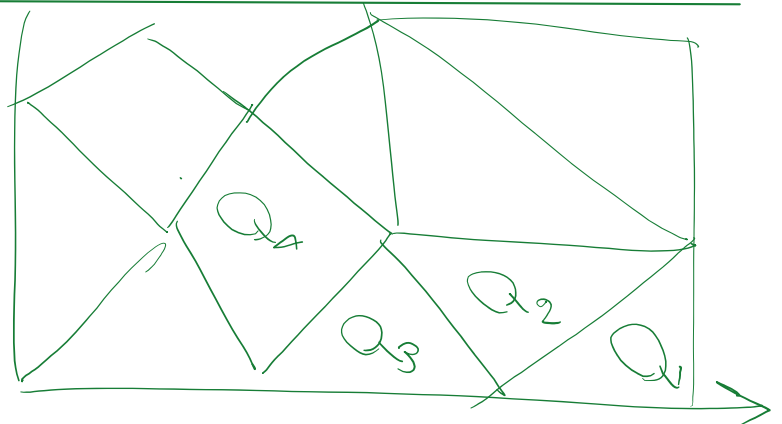
$$\textcircled{b} \quad \int_{\partial \Omega} F_n \, dS = \int_{\Omega} r \, dV$$

We satisfy the balance law w.r.t. target values

Now we want to go to discrete setting

$$V \Omega \rightarrow$$

spacetime mesh



$\Delta \rightarrow$
spacetime elements

