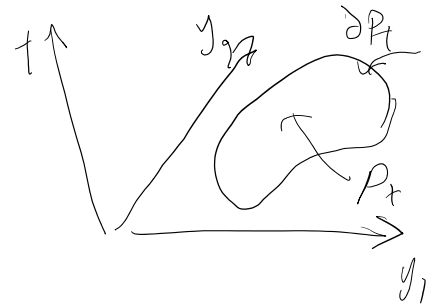


B) General expression of balance laws in spacetime

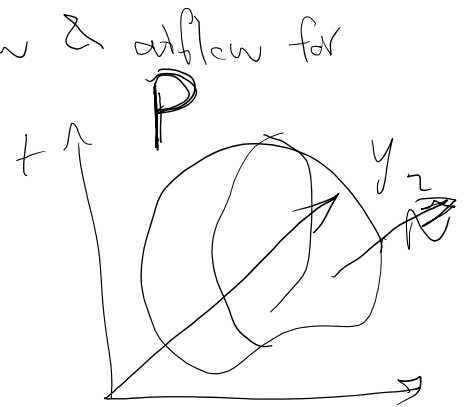
$$\frac{D}{Dt} \int_{P_t} s \, dV_y = \int_{P_t} r_s \, dV_y - \int_{\partial P_t} f_s^y \, ndA_y$$

$$\Rightarrow \int_{P_t} \frac{\partial s}{\partial t} + \int_{\partial P_t} F_s^y \, ndA_y = \int_{P_t} r_s \, dV_y$$



express it as temporal flux on time inflow & outflow for arbitrary shapes in space time

$$\int_{\partial P_t} F \cdot N \, dA_y = \int_{P_t} r_s \, dV_y$$



$F = \begin{bmatrix} F_s^y \\ s \end{bmatrix}$ → space flux density ($F_s^y = \underbrace{sv}_y + \underbrace{f_s^y}_{\text{diffusive part}}$)
 → temporal flux = density of balanced quantity

$N = \begin{bmatrix} \vec{n}_y \\ n_t \end{bmatrix}$ → vector
 → scalar in 2D $\begin{bmatrix} n_{y1} \\ n_{y2} \\ n_t \end{bmatrix}$

$$\int_{\partial P_t} F \cdot N \, dA_y = \int_{P_t} r_s \, dV_y \quad \text{Balance law}$$

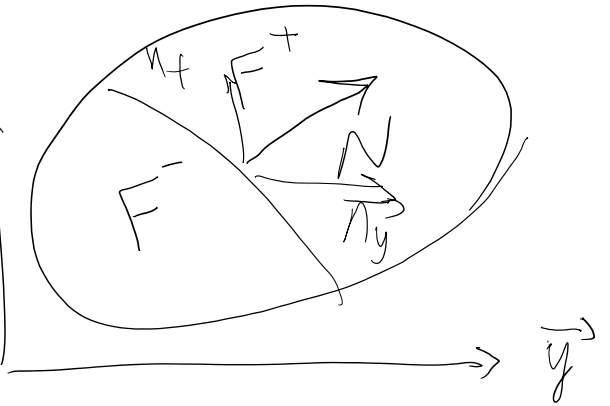
$$\Rightarrow \left\{ \begin{array}{l} \text{PDE} \\ \nabla_y \cdot F - r_s = 0 \\ \left[\nabla_y \quad \frac{\partial}{\partial t} \right] \begin{bmatrix} F_s^y \\ s \end{bmatrix} = r_s = \frac{\partial s}{\partial t} + \nabla_y \cdot F_s^y - r_s = 0 \end{array} \right.$$

L O ∇ J L S

② $[F] \cdot N = 0$

$$\underline{[F]_S} \cdot \vec{n}_y + [S] \cdot n_t = 0$$

t ↑



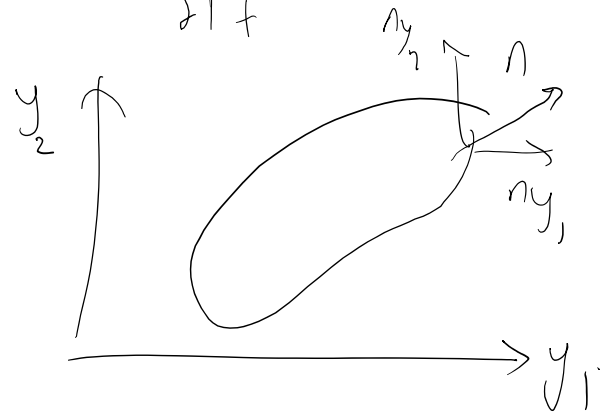
Steady state or static balance laws, $\frac{D}{Dt} = 0$

no rate in time

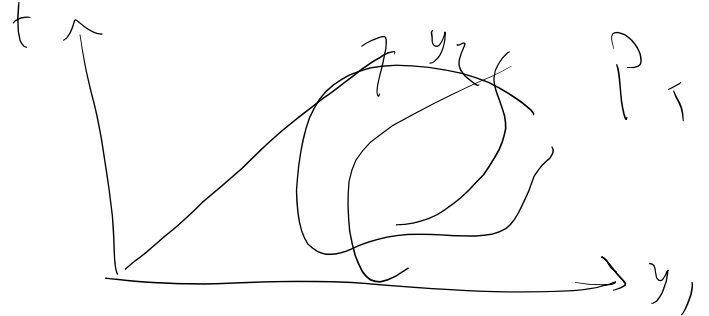
$$\frac{D S}{Dt} = 0 = \int_{P_t} \sigma_s dV - \int_{\partial P_t} f_s^y n dA_y$$

$$\int_{\partial P_t} f_s^y n dA_y = \int_{P_t} f_s dV$$

$\int_{\partial P_t} f_s^y n dA_y$ ← static flux → $\int_{P_t} f_s dV$ source



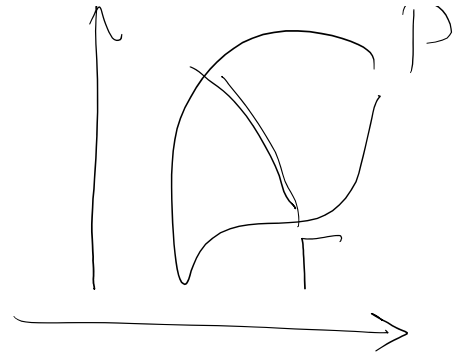
$$\int_{\partial P_t} F \cdot N dA_y = \int_{P_t} r_s dV$$



For any balance law we have



$$\int_{\partial P} F n dS = \int_P r dV$$



$$\Rightarrow \left\{ \begin{array}{l} \nabla \cdot F - r = 0 \quad \text{PDE} \\ [F] \cdot n = 0 \quad \text{Jump condition} \end{array} \right.$$

Dynamic case

$$F = \begin{bmatrix} F_s^y \\ S \end{bmatrix}$$

$$\left(\nabla_y \cdot F_s^y + \frac{\partial S}{\partial t} \right) - r_s = 0$$

$\nabla \cdot F$

$$[F_s^y] \cdot n_y + [S] \cdot n_z = 0$$

PDE

$$\nabla \cdot F - r = 0$$

Jump

$$[F] \cdot n = 0$$

Static

$$F = F_s^y$$

$$\nabla_y \cdot F_s^y - r = 0$$

$$[F_s^y] \cdot n_y = 0$$

C) Balance laws for arbitrary z coordinate

$$z = x$$

$$z = y$$

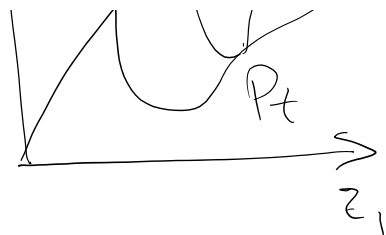
or something in between

(Arbitrary Lagrangian Eulerian)
ALE formulation



$$\int_{P_t} \nabla_{z_i} \cdot S = \int_{P_t} s dV_z$$

MS, ?



$$\left. \frac{DS}{Dt} \right|_{x\text{-fixed}} = ?$$

we follow a fixed volume of material

$$\frac{DS}{Dt} = \int_{P_t} \left. \frac{\partial S}{\partial t} \right|_{z\text{-fixed}} dV_y + \int_S \sqrt{V}(z,t) n_z dA_z$$

Eulerian $z=y \rightarrow V=\hat{V}$ ← $S \hat{V} \cdot n dA_y$

speed at which the boundary of P_t is moving when we follow a fixed material domain

Case 1 $z=y$ Eulerian

$$\underline{\bar{V}}(z,t) = \left. \frac{\partial y(x,t)}{\partial t} \right|_{x\text{-fixed}} = V(x,t) = \hat{V}(y,t)$$

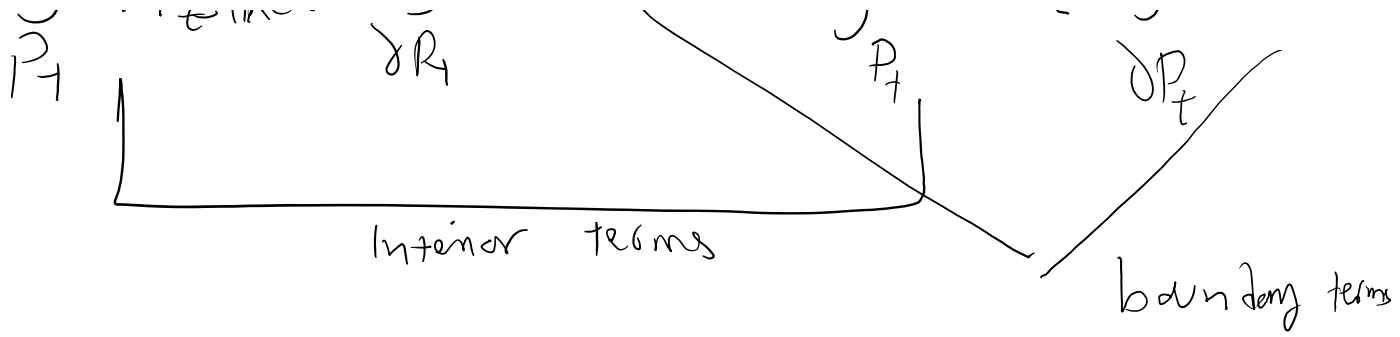
Case 2: $z=x$ Lagrangian

$$\underline{\bar{V}}(z,t) = \left. \frac{\partial x(x,t)}{\partial t} \right|_{x\text{-fixed}} = 0$$

$$z \neq x \ \& \ z \neq y \quad \bar{V}(z,t) \neq 0 \neq \hat{V}(y,t)$$

$$\left. \frac{DS}{Dt} \right|_{x\text{-fixed}} = \int_{P_t} \bar{r}_s^z dV_z - \int_S f_s^z(z,t) n_z dA_z$$

$$\int_{P_t} \left. \frac{DS}{Dt} \right|_{z\text{-fixed}} + \int_{\partial R} S \sqrt{V}(z,t) n_z dA_z = \int_{P_t} \bar{r}_s^z dV_z - \int_{\partial P_t} f_s^z(z,t) n_z dA_z$$



$$\int_{P_T} \left(\frac{\delta S}{\delta t} \Big|_{z\text{-fixed}} - f_s^z \right) dV_z + \int_{\delta R} \left(s \otimes V + f_s^z \right) \cdot n_z dA_z = 0$$

$$\checkmark \quad + \int_{\partial P_T} \left(s \otimes V + f_s^z \right) \cdot n_z dV_z = 0$$

$$\int_{P_T} \left[\frac{\delta S}{\delta t} - f_s^z + \nabla_z \cdot \left(s \otimes V + f_s^z \right) \right] dV_z = 0$$

P_T

arbitrary (Use localization to get)

$$\left. \frac{\partial s}{\partial t} \right|_{z\text{-fixed}} + \underbrace{\nabla_z \cdot \mathbf{F}_s^z}_{\text{spatial flux density}} = \underbrace{r_s^z}_{\text{source term}}$$

temporal flux density

$$\mathbf{F}_s^z = s \otimes \underbrace{\mathbf{V}_z}_{\substack{\text{velocity of boundary of } P_T \\ \text{"advective"} \quad \text{"diffusive"}}} + \mathbf{f}_s^z$$

$$\begin{aligned} V_z = \hat{V} & \quad z = y \\ V_z = 0 & \quad z = x \end{aligned}$$

Conservation of mass:

$$\frac{DS}{Dt} = \frac{D}{Dt} \int_{P_T} s \, dV_y = \underbrace{\int_{P_T} r_s \, dV_y}_{\text{source term}} - \underbrace{\int_{\partial P_T} \mathbf{f}_s^y \cdot \mathbf{n} \, dA_y}_{\text{spatial flux}}$$

$$S=M \quad \frac{DM}{Dt} = \frac{D}{Dt} \int_{P_T} \underbrace{\rho}_{\text{mass density}} \, dV_y = \bigcirc + \bigcirc$$

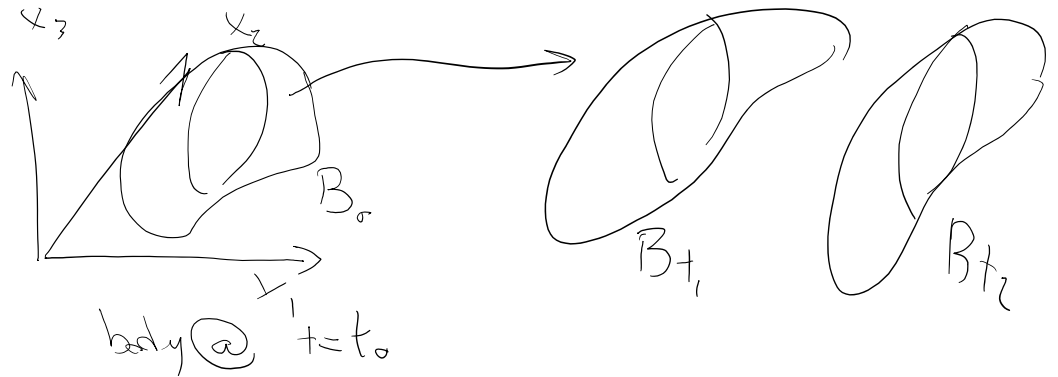
$$\frac{DM}{Dt} = 0 \quad M = \text{const} \quad (\text{conservation law})$$

Conservation of Mass

Conservation of Mass

$$\frac{DM}{Dt} = 0 = \frac{D}{Dt} \int \rho \, dV_y$$

Lagrangian interpretation



$$M(0) = \int_{B_0} \rho_0(x) \, dV_x$$

density @ $t=t_0$

$$M(t) = \int_{B_t} \hat{\rho}(y,t) \, dV_y$$

$$\frac{dM}{dt} = 0 \rightarrow M(t) = M(0)$$

$$\int_{B_t} \hat{\rho}(y,t) \, dV_y = \int_{B_0} \rho_0(x) \, dV_x$$

$$\int_{B_0} \rho(x,t) \, J \, dV_x = \int_{B_0} \rho_0(x) \, dV_x$$

$$dV_y = J \, dV_x$$

$$J = \det F$$

$$\int_{B_0} (\rho(x,t) J - \rho_0(x)) \, dV_x = 0$$

B_0 arbitrary \rightarrow use localization

arbitrary \longrightarrow use localization

Balance
of mass:
Lagrangian
interpretation

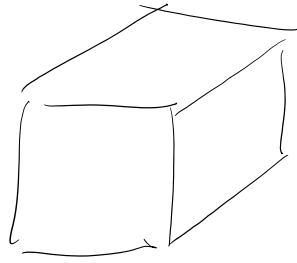
$$\rho J = \rho_0 \implies \rho(x,t) = \frac{\rho_0(x)}{J(x,t)}$$

$$dm = \rho dV$$

$$\begin{array}{l} \text{at } t=t_0 \\ \text{at } t \end{array} \quad \begin{array}{l} \rho_0 dV_x \\ \hat{\rho} dV_y \end{array} \quad \parallel \quad \implies \quad \rho(x,t) J dV_x$$

$$\rho_0 = \rho J$$

$$\rho = \frac{\rho_0}{J}$$

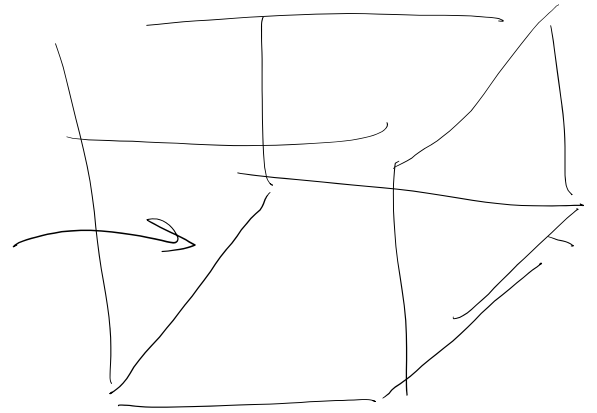


dx

$$dV_x = dx^3$$

$$dm = dV_x \rho_0$$

$$= \rho_0 dx^3$$



$1.1 dx$

$$dV_y = \underbrace{(1.1)^3}_J dx^3$$

$$dm = \rho dV_y$$

$$= \rho \frac{(1.1)^3}{J} dx^3$$

$$\rho = \frac{\rho_0}{(1.1)^3} = \frac{\rho_0}{J}$$

Volume \uparrow $\rho \downarrow$

Uses of dm being constant in time

Theorem 151 (Reduced Transport Theorem) Let $g \in C^1(\mathfrak{B}, \mathfrak{R})$. Then

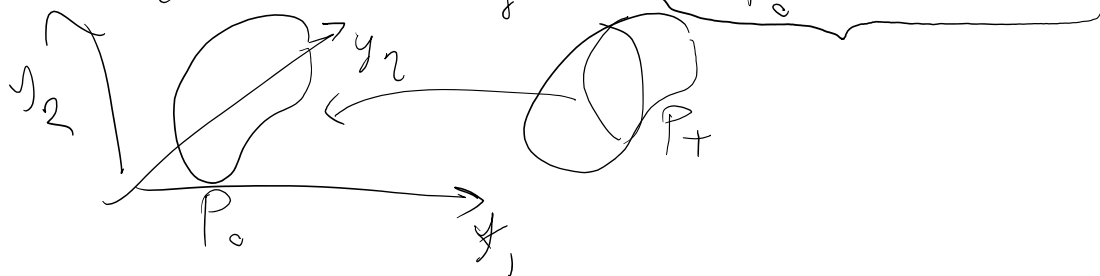
$$\frac{d}{dt} \int_{P_t} g(\mathbf{y}, t) \rho(\mathbf{y}, t) dV_{\mathbf{y}} = \int_{P_t} \left[\frac{\partial g}{\partial t}(\mathbf{y}, t) + g_{,i}(\mathbf{y}, t) \hat{v}_i(\mathbf{y}, t) \right] \rho(\mathbf{y}, t) dV_{\mathbf{y}}$$

$$= \int_{P_t} \left[\frac{\partial g}{\partial t}(\mathbf{y}, t) + \nabla g(\mathbf{y}, t) \cdot \hat{\mathbf{v}}(\mathbf{y}, t) \right] \rho(\mathbf{y}, t) dV_{\mathbf{y}}$$

added
to transport equation

Compare
Transport
 $\frac{D}{Dt} \int g dV_{\mathbf{y}} = \dots$

$$\frac{D}{Dt} \int_{P_t} \hat{g}(\mathbf{y}, t) \underbrace{\rho(\mathbf{y}, t) dV_{\mathbf{y}}}_{dm_{\mathbf{y}}} = \frac{D}{Dt} \int_{P_0} g(\mathbf{x}, t) dm =$$



$$= \int_{P_0} \frac{D}{Dt} (g(\mathbf{x}, t) dm) = \int_{P_0} \frac{D}{Dt} g(\mathbf{x}, t) \underbrace{dm}_{\text{doesn't depend on time}}$$

$$= \int_{P_t} \frac{D}{Dt} \hat{g}(\mathbf{y}, t) dm$$

$$\int_{P_t} \left(\frac{\partial g}{\partial t} + \nabla_{\mathbf{y}} g \cdot \hat{\mathbf{v}} \right) dm$$

$$= \int \left(\frac{\partial g}{\partial t} + \nabla_y g \cdot \hat{v} \right) \rho^g dV_y$$

$$\frac{Dg}{Dt}$$

~~Transport eqn~~

$$\begin{aligned} \frac{d}{dt} \int_{P_t} g(\mathbf{y}, t) dV_y &= \int_{P_t} \left[\frac{\partial g}{\partial t}(\mathbf{y}, t) + g_{,i}(\mathbf{y}, t) \hat{v}_i(\mathbf{y}, t) + g(\mathbf{y}, t) \hat{v}_{i,i}(\mathbf{y}, t) \right] dV_y \\ &= \int_{P_t} \left\{ \frac{\partial g}{\partial t}(\mathbf{y}, t) + [g \hat{v}_i]_{,i}(\mathbf{y}, t) \right\} dV_y \\ &= \int_{P_t} \frac{\partial g}{\partial t}(\mathbf{y}, t) dV_y + \int_{\partial P_t} g(\mathbf{y}, t) [\hat{v}(\mathbf{y}, t) \cdot \mathbf{n}(\mathbf{y}, t)] dA_y, \end{aligned}$$

we don't have this term that came from

$$\frac{D}{Dt} = \text{div}_y \vec{v} \int$$

can prove reduced transport eqn by letting $\tilde{g} = \rho^g g$ in transport eqn

$$\frac{D}{Dt} \int \underbrace{g}_{\text{is volumetric density}} dV_y = \text{Transport eqn}$$

$$\frac{D}{Dt} \int \underbrace{g \rho}_{\text{is mass density of } G} dV_y = \frac{D}{Dt} \int g dm = \text{Reduced eqn Transport}$$

Conservation of Mass in Eulerian framework:

$$\frac{D}{Dt} \int_{P_t} \rho dV_y = \int_{P_t} \frac{\partial \rho}{\partial t} dV_y + \int_{\partial P_t} \rho \hat{v} \cdot \mathbf{n} dA_y$$

$$\frac{D}{Dt} \int_{P_t} s \rho dV_y = \int_{P_t} \frac{\partial s}{\partial t} \rho dV_y + \int_{\partial P_t} s \rho \hat{v} \cdot \mathbf{n} dA_y$$

$$\frac{D}{Dt} \int_{\mathcal{R}} \rho \, dV_y = \int_{\mathcal{R}_t} \frac{\partial \rho}{\partial t} \, dV_y + \int_{\partial \mathcal{R}_t} \rho \hat{\mathbf{v}} \cdot \mathbf{n} \, dA_y$$

$$\frac{D}{Dt} \int_{\mathcal{R}} \rho \, dV_y = \frac{D}{Dt} M = \int_{\mathcal{R}_t} \frac{\partial \rho}{\partial t} \, dV_y + \int_{\partial \mathcal{R}_t} \rho \hat{\mathbf{v}} \cdot \mathbf{n} \, dA_y$$

$$\boxed{\frac{DM}{Dt} \int_{\mathcal{R}_t} \rho \, dV_y = \int_{\mathcal{R}_t} \frac{\partial \rho}{\partial t} + \int_{\partial \mathcal{R}_t} \rho \hat{\mathbf{v}} \cdot \mathbf{n} \, dA_y = 0}$$

apply divergence theorem

$$\int_{\mathcal{R}_t} \frac{\partial \rho}{\partial t} + \int_{\mathcal{R}_t} \underbrace{\text{div}}_{\nabla_y \cdot} (\rho \hat{\mathbf{v}}) \, dV_y = 0$$

$$\int_{\mathcal{R}_t} \left[\frac{\partial \rho}{\partial t} + \text{div}(\rho \hat{\mathbf{v}}) \right] \, dV_y = 0$$

localization

Balance
of mass
in Eulerian
framework

$$\frac{\partial \rho}{\partial t} + \underbrace{\text{div}}_{\nabla_y \cdot} (\rho \hat{\mathbf{v}}) = 0$$

$\nabla_y \cdot$

spatial flux

Having a full divergence is good because:

1. We have a definition of spatial flux density (what div acts on)
2. Numerical formulation of many methods such as Discontinuous Galerkin method becomes much simpler

$$\frac{Ds}{Dt} = \frac{\partial s}{\partial t} + \nabla_y \cdot s \cdot \hat{v}$$

Another way to write conservation of mass

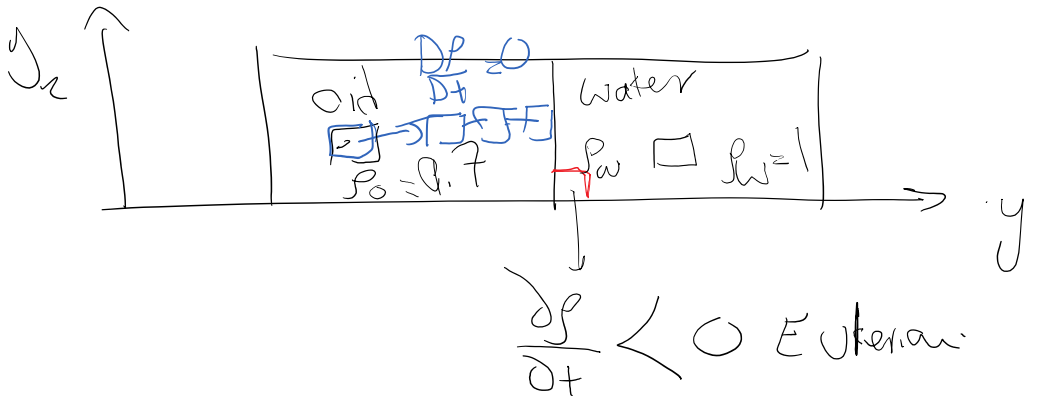
$$\frac{\partial \rho}{\partial t} + \text{div}(\rho \hat{v}) = \frac{\partial \rho}{\partial t} + \frac{\partial \rho \hat{v}_i}{\partial y_i} =$$

$$\underbrace{\frac{\partial \rho}{\partial t} + \frac{\partial \rho}{\partial y_i} \hat{v}_i}_{\text{Material rate}} + \rho \frac{\partial \hat{v}_i}{\partial y_i} = \left(\frac{\partial \rho}{\partial t} + \nabla_y \cdot \rho \cdot \hat{v} \right) + \rho (\text{div} \hat{v}) =$$

$$\frac{\partial \rho}{\partial t} + \text{div}(\rho \hat{v}) = \frac{D\rho}{Dt} + \rho (\text{div} \hat{v}) = 0$$

not a complete div term ρ

For incompressible fluid $\frac{D\rho}{Dt} = 0$ ($\rho = \text{const}$)



Incompressible fluid

$$\cancel{\frac{D\rho}{Dt}} + \rho \text{div} v = 0$$

$$\text{div} \hat{v} = 0$$

$$\frac{DJ}{Dt} = (\text{div} \hat{v}) \cdot J$$

$$D.J = 0$$

$$\frac{dV}{dt} = 0$$

Volume doesn't
change

$$dV_y = dV_x$$

In solid mechanics we assume incompressibility for plastic deformation
(Poisson ratio = 0.5)