## 2019/11/15

Friday, November 15, 2019 11:40 AM

Last time from objectivity we obtained:



Theorem 173 If the elastic constituitive equation

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$$\mathbf{T}(\mathbf{x},t) = \mathbf{G}(\mathbf{F}(\mathbf{x},t),\mathbf{x}) \tag{4.1}$$

is consistent with the Principle of Material Frame-Indifference, then it can be written in any of the following reduced forms:

$$\tilde{\mathbf{T}}(\mathbf{x},t) = \mathbf{R}(\mathbf{x},t)\mathbf{G}(\mathbf{U}(\mathbf{x},t),\mathbf{x})\mathbf{R}^{t}(\mathbf{x},t);$$
(4.2)

$$\mathbf{T}(\mathbf{x},t) = \mathbf{F}(\mathbf{x},t)\mathbf{\tilde{G}}(\mathbf{U}(\mathbf{x},t),\mathbf{x})\mathbf{F}^{t}(\mathbf{x},t);$$
(4.3)

$$\tilde{\mathbf{T}}(\mathbf{x},t) = \mathbf{F}(\mathbf{x},t)\bar{\mathbf{G}}(\mathbf{C}(\mathbf{x},t),\mathbf{x})\mathbf{F}^{t}(\mathbf{x},t);$$
(4.4)

where  $\hat{\mathbf{G}} : \operatorname{Psym} \times \stackrel{0}{\mathcal{B}} \to \operatorname{Sym}$  and  $\bar{\mathbf{G}} : \operatorname{Psym} \times \stackrel{0}{\mathcal{B}} \to \operatorname{Sym}$ .

## 4.4 Material symmetry; Isotropy

From geometric perspective, any multiple of 90 degree rotation, results in the same material.

A transformation of an object that leaves some properties of the object invariant is called a symmetry transformation.



How about a constitutive equation?

We will show that under infinitesimal deformation for linear material:









Last time we obtained the relation between G's starting from two different "initial configurations":

$$f^{(n)}(x) = g(x^{(n)})$$

$$f^{(n)}(x) = g(x$$

divide the two relations to get

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the two relations to get  

$$\frac{f_{x}(x^{(2)})}{P_{y}(x^{(1)})} = \frac{det}{det} \frac{F^{(1)}}{F^{(1)}} \left\{ \begin{array}{c} 2^{2} = g(x^{(1)}) = 3 \\ \hline 1 = g($$

$$\frac{J_{*}(N)}{\mathcal{P}_{*}(X^{(1)})} = \frac{\partial u}{\partial t} F^{(1)}$$

$$\frac{J_{*}(N)}{\left[\frac{F^{(1)}}{F^{(2)}} + \frac{F^{(2)}}{\sqrt{2}}\right]} = \frac{\partial v}{\partial t} \frac{F^{(2)}}{\sqrt{2}}$$

$$\frac{J_{*}(N)}{\left[\frac{F^{(1)}}{F^{(2)}} + \frac{F^{(2)}}{\sqrt{2}}\right]} = \frac{\partial v}{\partial t} \frac{V_{*}}{\sqrt{2}}$$

$$\frac{J_{*}(N)}{\int_{\mathcal{P}_{*}(X^{(1)})}} = \frac{\partial v}{\partial t} \frac{V_{*}}{\sqrt{2}}$$



As the minimum requirement going through different initial configurations, we want the initial density to not change. From (D) we require Z (I zu or der tempson H for which called unimodular &+ H = | is is Examples:  $\nabla g = \begin{bmatrix} 2 & 0 \\ 0 & k \end{bmatrix}$  $dt \nabla g = 1$ 2906 Ŝ Uq (Vangl Unindular AIL\_\_\_X  $\square$ ζx RID [2 2 ( du P3-4 + ) 2D

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Basically, if we only restric ourselves to g's for which initial density does not change (very reasonable restriction), we are left with grad g's in the space of unimodular tensors (which obviously include rotations):

Vg E Unim Dt = 2 HELIND / ddH=1/

How about constitutive equation for Cauchy stress tensor T 👸 )

$$T = G_{1}^{(1)} \left(F_{1}^{(1)}, \chi^{(1)}\right)$$

$$T = G_{1}^{(2)} \left(F_{1}^{(2)}, \chi^{(1)}\right)$$

$$T = G_{1}^{(2)} \left(F_{1}^{(2)}, \chi^{(2)}\right)$$

$$F_{1}^{(2)} = \overline{y}_{g(1)} = \overline{y}_{g(1)} \overline{y}_{g(1)} = F_{1}^{(2)} \overline{y}_{g(1)}$$

$$F_{1}^{(2)} = \overline{y}_{g(1)} = \overline{y}_{g(1)} \left(F_{1}^{(2)}, \chi^{(2)}\right)$$

$$F_{1}^{(2)} = \overline{y}_$$

if 
$$\nabla g$$
 is in symmetry group of conditivitive equals: what should are  
have?  $\int G'(F, X)$  these should be equal  
 $G^{e_1}(F, X) = G^{i_2}(FZ_g, X^{u})$  Alwaystone  
 $G^{e_1}(F, X^{u}) = G''(F, X^{u'})$  take if  $\nabla g$  belongs  
 $G^{e_2}(F, X^{u'}) = G''(F, X^{u'})$  take if  $\nabla g$  belongs  
to symmetry group for  
const. Eqn. (Room B, 'R B'  
same const eqn. is charatorial)  
 $G^{e_1}(F, X') = G''(FTg, X'')$ 

Basically, map g belongs to symmetry group for cons. Eqn. If

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Definition 112 (Noll, 1958) Given an elastic body and a reference configuration that corresponds to the region  $\stackrel{0}{\mathcal{B}}$ , the material symmetry group at the material point identified by x in the reference configuration is the set

$$\underset{\mathbf{x}}{\operatorname{Msg}} = \left\{ \mathbf{H} \in \operatorname{Unim} \ \mathcal{V}^{+} : \mathbf{G}(\mathbf{F}\mathbf{H}, \mathbf{x}) = \mathbf{G}(\mathbf{F}, \mathbf{x}) \ \forall \ \mathbf{F} \in \operatorname{Lin} \ \mathcal{V}^{+} \right\}.$$

Again, it should be emphasized that the material symmetry group is characterized by tensors **H** that correspond to the gradients at **x** of deformations — not the deformations themselves. This is because the mass density and the elastic response function in the second reference configuration depend only on the gradient of the connecting deformation. Also, note that  $\mathbf{H} \in \mathrm{Msg}_{\mathbf{x}}$  is not a tensor field, but rather the value of a tensor field at  $\mathbf{x}$ .

The following theorem presents a property of all orthogonal elements of  $\rm Msg_x$  that derives from the Principle of Material Frame-Indifference.

## For isotropic solid material, what should be symmetry group of constitutive equation?

All rotations belong to symmetry group.

What is the material that ALL unimodal tensors belong to its symmetry group?



"Elastic fluids," would have all unimodal tensors in their const. eqn. symmetry group:



TAM551: using this equation, it can be shown that for linear isotropic solid, there are only two independent material parameters (E, nu OR Lame's parameters)

 $G_{ij} = G_{ikl} \in kl$   $G_{ij} = G_{ikl} \in kl$   $G_{ij} = \int S_{ij} S_{kl} + M \left[ S_{ik} S_{jl} + \frac{1}{2} S_{jk} \right]$ 

Cijke - J St, Ske + M (Sik Sik + J.G Sik) Shear modulus Shear modulus Shear modulus Shear modulus