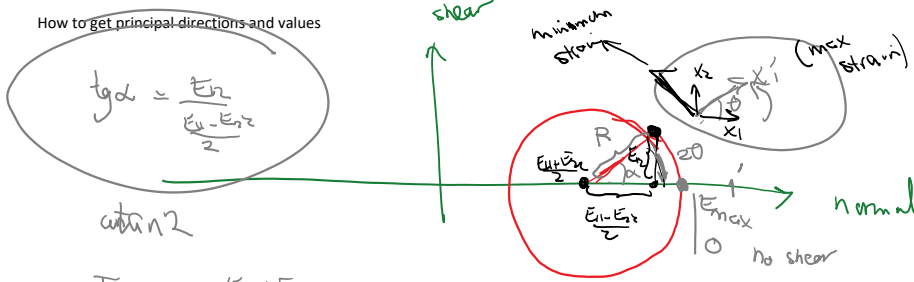


How to get principal directions and values



$$\tan 2\theta = \frac{E_{12}}{\frac{E_{11}-E_{22}}{2}}$$

where

$$E_{max} = \frac{E_{11}+E_{22}}{2} + R$$

$$-R = \sqrt{E_{12}^2 + \left(\frac{E_{11}-E_{22}}{2}\right)^2}$$

$$E_{min} = \frac{E_{11}+E_{22}}{2} - R$$

$$\alpha = -2\theta$$

Recall rotation from  $1 \rightarrow 1'$  being  $\theta$

in Mohr circle we had  $-2\theta$  rotation

You can always use eigen funcn to calculate these

$$\begin{bmatrix} E_{11}-\lambda & E_{12} \\ E_{12} & E_{22}-\lambda \end{bmatrix} \begin{bmatrix} \cos\theta \\ \sin\theta \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$\lambda^2 - (E_{11}+E_{22})\lambda + E_{11}E_{22}-E_{12}^2 = 0 \quad \leftarrow \text{eigen vector in direction } \theta$$

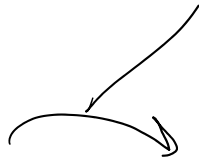
$$\lambda = \frac{E_{11}+E_{22}}{2} \pm \sqrt{\left(\frac{E_{11}-E_{22}}{2}\right)^2 + E_{12}^2}$$

they match  $E_{max}, E_{min}$  above

Please read theorem 139 (Cesaro line integral representation)

idea

$$\begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$



$$E = \begin{bmatrix} E_{11} & E_{12} \\ E_{12} & E_{22} \end{bmatrix}$$



$$E_{11} = u_{1,1}$$

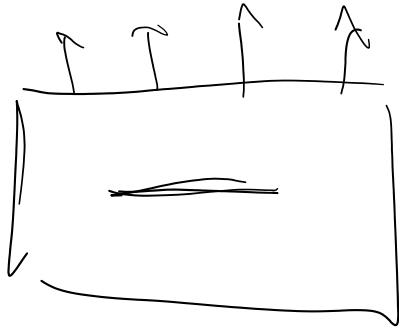
$$E_{22} = u_{2,2}$$

$$E_{12} = \frac{1}{2}(u_{1,2} + u_{2,1})$$

we cannot always go from strain to displacement

Why we may even want to go from strain to displacement?

We have these functions called Airy stress functions -> we get stress solutions that are very good for many different problems



$$\begin{matrix} \epsilon_{11} \\ \epsilon_{22} \\ \epsilon_{12} \end{matrix} \checkmark \rightarrow \begin{bmatrix} E_{11} \\ E_{22} \\ 2E_{12} \end{bmatrix} = C \begin{bmatrix} \epsilon_{11} \\ \epsilon_{22} \\ \epsilon_{12} \end{bmatrix}$$

next  $E_{11} = U_{1,1} \rightarrow U_i = \int E_{11} dx_1$

we cannot always Integrate strains to get displacements. We need Additional compatibility eqns.

2D

$$\begin{aligned} E_{11} &= U_{1,1} \\ E_{22} &= U_{2,2} \\ E_{12} &= .5 (U_{1,2} + U_{2,1}) \end{aligned}$$

3 strains



$$U = \begin{bmatrix} U_1 \\ U_2 \end{bmatrix}$$

2 displacements

3 - 2 = 1 additional "compatibility" eqns needed to ensure we can integrate strain to get displacement.

$$\boxed{\epsilon_{11,22} + \epsilon_{22,11} - 2 \epsilon_{12,12} = 0} \quad (\star)$$

In 3D there are 3 compatibility equations (6 strains - 3 displacements = 3)

In 1, there is no compatibility equations. So, every reasonable strain can be integrated.

$$\frac{du}{dx} = E(x) = 0.005x + 1e-5x^2$$

$$u = \int \frac{du}{dx} \cdot dx = 0.01x^2 + \frac{1e-5x^3}{3} + C$$

Motion:

We have time dependency of deformation

**Definition 87** A motion of a body is a family of deformations ordered by a single real parameter called time, denoted  $t$ . We introduce a reference time  $t_0$  associated with the undeformed state of the body.<sup>16</sup> Then a motion is denoted by

$$\{f(\cdot, t), t \in [t_0, \infty),$$

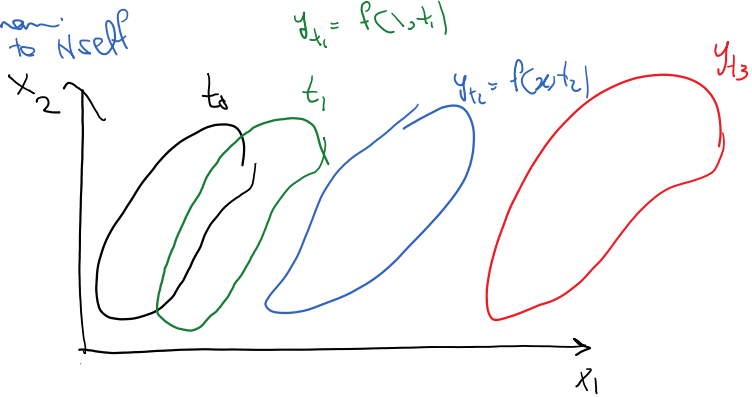
where

$$y = f(x, t)$$

is the position vector at time  $t$  of the material point identified by the position vector  $x$  in the undeformed state at time  $t_0$ . A motion inherits all the required properties of a deformation, except that the numbered properties in Definition 72 are superseded by the requirements

1.  $f(x, t_0) = x$ ;
  2.  $f \in C^2(\overset{0}{B} \times [t_0, \infty), V)$ .<sup>17</sup>
- Motion is a time-dependent deformation
- $y = x$  @  $t_0 \rightarrow F = I$   
 $\det F = 1$

@ time zero domain maps to itself



Basically for each time we want  $y_t$  to be a deformation

**Definition 72** Let  $\overset{0}{B}$  be an open, bounded, regular region of a Euclidean point space  $\mathcal{E}$ . A deformation  $f$  is a mapping (function) of points in  $\overset{0}{B}$  onto another open region of  $\mathcal{E}$  with the properties

1.  $f$  is one-to-one; i.e.,  $f(x) = f(y) \Rightarrow x = y \forall x, y \in \overset{0}{B}$ .
2.  $f \in C^2(\overset{0}{B}), f^{-1} \in C^2(f(\overset{0}{B}))$ ,
3.  $\det \nabla f(x) > 0 \forall x \in \overset{0}{B}$ .

The notation  $f(\overset{0}{B})$  refers to the mapped region, which is called the image of the set  $\overset{0}{B}$  under  $f$ .

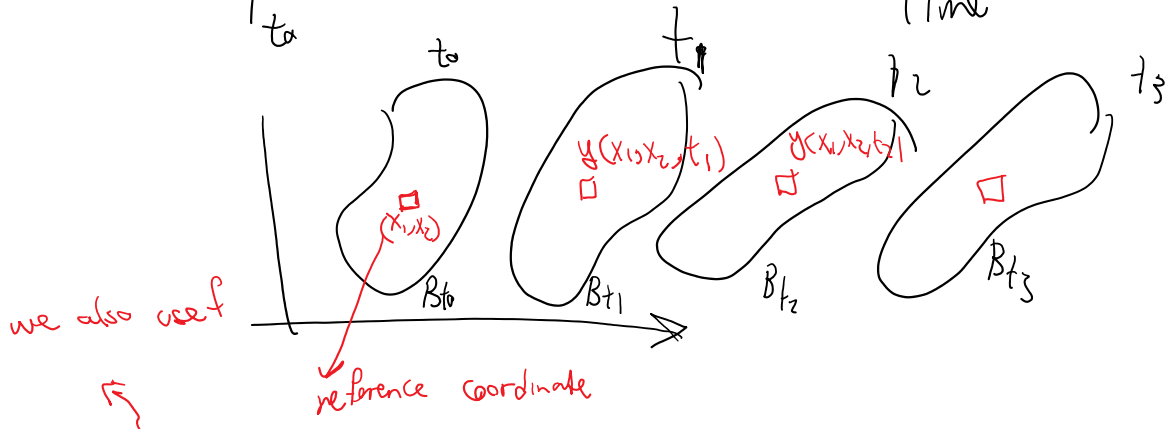
fy

see theorem 143 if  $\det F \neq 0 \rightarrow \det F > 0$

$\det F = 1$  @  $t_0$  &  $\det F \neq 0$  continuous  $\rightarrow$  it always stays  $> 0$



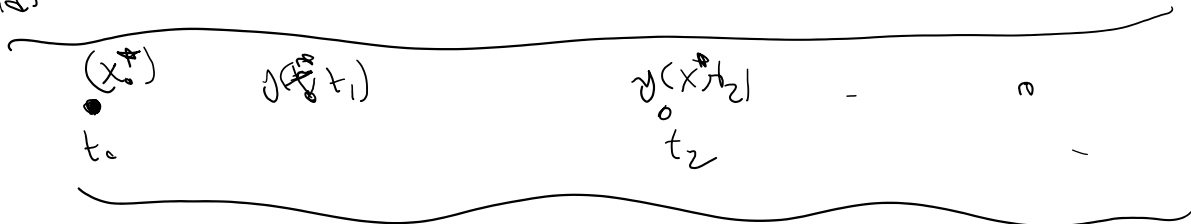
Velocity



reference coordinate

$$V(x, t) = \frac{Dy(x, t)}{Dt} \quad | \quad x \text{ is fixed}$$

fluids



$$V(x^*, t) = \frac{dy(x^*, t)}{dt} \quad | \quad x^* = \text{const}$$

particle is fixed



taking @ a fixed location  
we measure things in  $y$  (current configuration)  
appropriate for fluid mechanics

Eulerian

$$\hat{v}(y, t)$$

Lagrangian, we track particles from reference coordinate  $x$

$$\underline{V(x, t)}$$

mostly used for solid materials

Many physical laws & equations are

Many physical laws & equations are for a fixed body in reference coordinate or fixed particle

$$V(x, t) = \frac{\partial \psi(x, t)}{\partial t} \quad | \text{fixed } x$$

~~$$V(y, t) = \frac{\partial \psi(y, t)}{\partial t} \quad | \text{fixed } y$$~~

for fluids

$$x = f(x, t) \rightarrow x = f^{-1}(y, t) \left. \begin{array}{l} \\ V(x, t) \end{array} \right\} \rightarrow$$

$$\hat{V}(y, t) = V(f^{-1}(y, t), t)$$

Summary

$$v(x,t) = \frac{D y(x,t)}{Dt} \Big|_{x\text{-fixed}} = \frac{D u(x,t)}{Dt} \text{ velocity}$$

$$a(x,t) = \frac{D v(x,t)}{Dt} \Big|_{x\text{-fixed}} = \frac{D^2 y(x,t)}{Dt^2} \Big|_{x\text{-fixed}} = \frac{D^2 u(x,t)}{Dt^2}$$

$$\frac{D}{Dt}$$

called material time derivative  
x is fixed

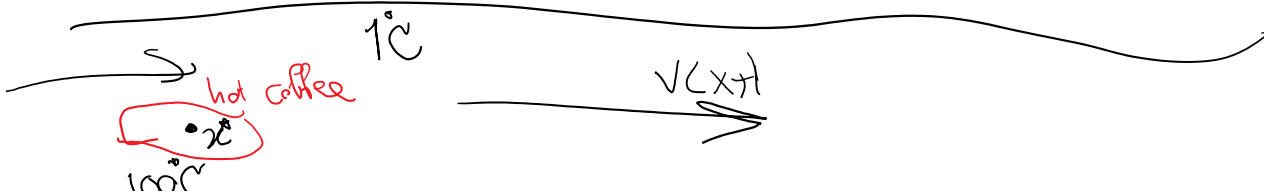
$\frac{\partial}{\partial t}$  often is spatial time derivative  
where y is fixed

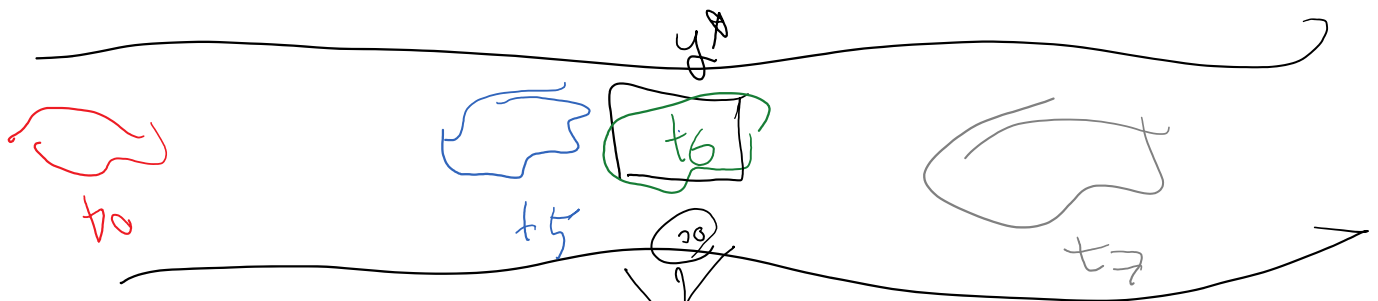
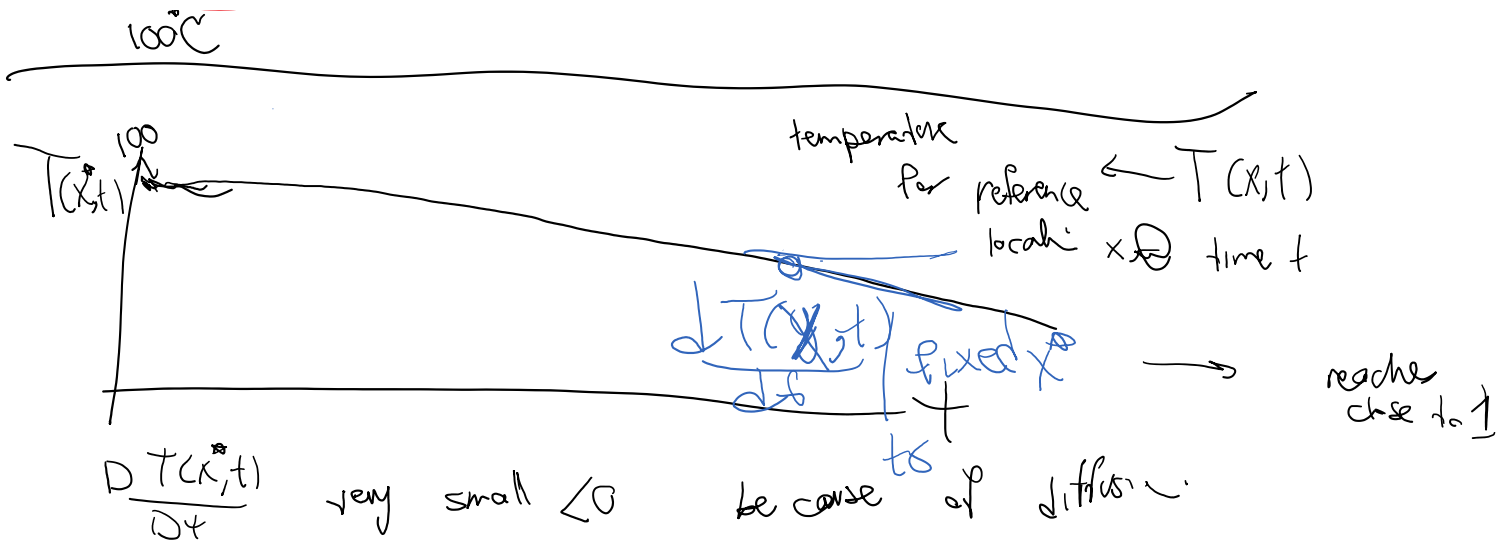
Since  $y(x,t) = zc + u(x,t)$

$$v(x,t) = \frac{D y(x,t)}{Dt} \Big|_{x\text{-fixed}} = \frac{D (zc + u(x,t))}{Dt} \Big|_{x\text{-fixed}} = \frac{D u(x,t)}{Dt} \Big|_{x\text{-fixed}}$$

How material and spatial time rates are related?

$$\frac{D}{Dt} \Big|_{x\text{-fixed}} \text{ vs } \frac{\partial}{\partial t} \Big|_{y\text{-fixed}}$$





measuring  $T$  at fixed  $y$  (Eulerian)

