

Conservation of mass:

$$M_{t_1} = M_{t_2} \dots$$



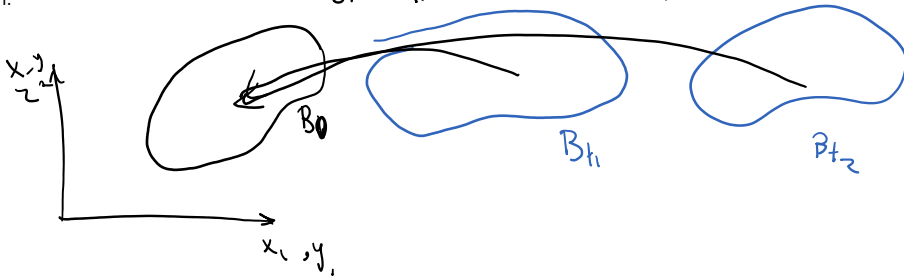
$$\frac{DM}{Dt} = 0 = \frac{D}{Dt} \int \rho dV_y = \int \rho \nabla \cdot \mathbf{v} dV_y + \int \mathbf{v} \cdot \nabla \rho dV_y = 0$$

mass density                      mass source                      mass sink flux

$$\frac{DM}{Dt} = 0 = \frac{D}{Dt} \int \rho dV_y \quad 1$$

Lagrangian Interpolation:

start from the same point



$$\frac{DM}{Dt} = 0 \rightarrow M(t) = M(0)$$

$$\int_{B_t} \hat{\rho}(y,t) dV_y = \int_{B_0} \rho_0(x) dV_x$$

change of variables  
 $dV_y = J dV_x$

$$\int_{B_0} \hat{\rho}(y,t) J dV_x = \int_{B_0} \rho_0(x) dV_x$$

$$\rightarrow \int_{B_0} [\hat{\rho}(y,t) J - \rho_0(x)] dV_x = 0$$

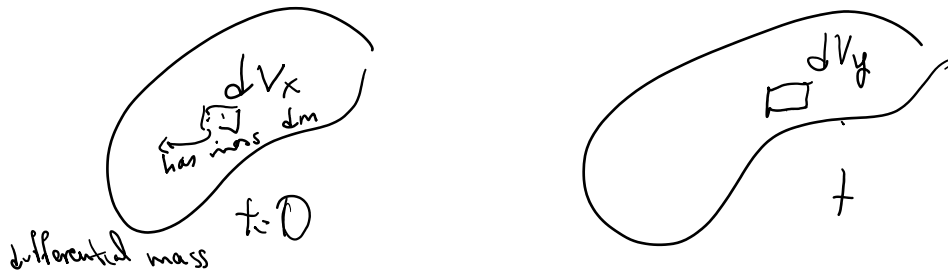
arbitrary  $\rightarrow$  localization theorem  $\rightarrow$

$$\hat{\rho}(y,t) J - \rho_0(x) = 0$$

Lagrangian  
 mass conserved:

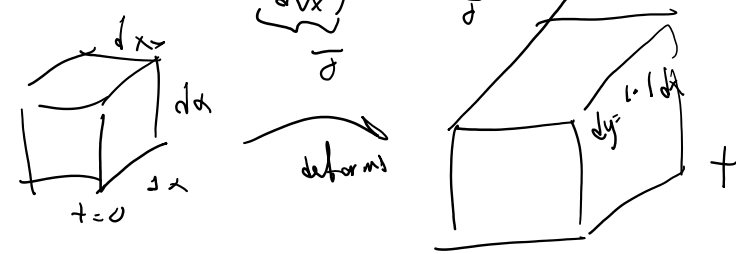
$$\rho J = \rho_0 \Rightarrow \rho(x,t) = \frac{\rho_0(x)}{J(x,t)}$$

intuitive way of looking at this



$$dm = \rho_0 dV_x = \rho dV_y$$

$$\rightarrow \rho = \rho_0 \left( \frac{dV_y}{dV_x} \right)^{-1} = \rho_0 \frac{1}{J}$$



$$\rho(x,t) = \frac{\rho_0(x)}{1.1^3} = \frac{\rho_0}{J}$$

Interesting outcome of Lagrangian balance of mass:  
Recall

**Theorem 145 (Transport Theorem)** Let  $g \in C^1(\mathbb{Z}, \mathbb{R})$  be a spatial scalar field. Then

$$\begin{aligned} \frac{D}{Dt} \int_{P_t} g(y,t) dV_y &= \int_{P_t} \left[ \frac{\partial g}{\partial t}(y,t) + g_{,i}(y,t) \hat{v}_i(y,t) + g(y,t) \hat{v}_{i,i}(y,t) \right] dV_y \\ &= \int_{P_t} \left\{ \frac{\partial g}{\partial t}(y,t) + \nabla \cdot (g \hat{v})(y,t) \right\} dV_y \\ &= \int_{P_t} \frac{\partial g}{\partial t}(y,t) dV_y + \int_{\partial P_t} g(y,t) [\hat{v}(y,t) \cdot \mathbf{n}(y,t)] dA_y \end{aligned}$$

reduced transport  
 $\int g$

I liked this :)

**Theorem 151 (Reduced Transport Theorem)** Let  $g \in C^1(\mathbb{Z}, \mathbb{R})$ . Then

$$\begin{aligned} \frac{d}{dt} \int_{P_t} g(y,t) \rho(y,t) dV_y &= \int_{P_t} \left[ \frac{\partial g}{\partial t}(y,t) + g_{,i}(y,t) \hat{v}_i(y,t) \right] \rho(y,t) dV_y \\ &= \int_{P_t} \left[ \frac{\partial g}{\partial t}(y,t) + \nabla g(y,t) \cdot \hat{v}(y,t) \right] \rho(y,t) dV_y \end{aligned}$$

not very nice

Proof:  
Smart proof

$$\begin{aligned} \frac{D}{Dt} \int_{P_t} g \rho dV_y &= \frac{D}{Dt} \int_{P_t} g dm_y = \frac{D}{Dt} \int_{P_0} g dm \\ &= \int_{P_0} \left( \frac{D}{Dt} g \right) dm \end{aligned}$$

$dm_x = \rho_0 dV_x$   
constant @ time 0  
go back to  $P_0$

$$\int_{P_0} \left( \frac{D}{Dt} g \right) dm \stackrel{\text{go back to } P_0}{=} \dots$$

constant ...

$$= \int \left( \frac{D}{Dt} g \right) \rho dV_y$$

$$\frac{D}{Dt} \int_{P_t} \rho g dV_y = \int_{P_t} \left[ \frac{D}{Dt} (\rho g) \right] dV_y$$

$$= \int_{P_t} \left( \frac{\partial \rho}{\partial t} g + \nabla \rho \cdot \hat{v} g \right) dV_y$$

It's not a full D.C. ) not good

Balance of linear momentum

$$\frac{D}{Dt} \int_{P_t} \rho \hat{v} dV_y$$

extra  $\int_{\partial P_t}$

Balance of mass in Eulerian framework

$$\frac{DM_{P_t}}{Dt} = \int_{P_t} \frac{D}{Dt} \rho dV_y + \int_{\partial P_t} \rho \hat{v} \cdot \mathbf{n} dS_y = 0$$

$$\frac{DM}{Dt} = \frac{D}{Dt} \int_{P_t} \rho dV_y = \int_{P_t} \frac{\partial \rho}{\partial t} dV_y + \int_{\partial P_t} \rho \hat{v} \cdot \mathbf{n} dS_y = 0$$

$$\int_{P_t} \frac{\partial \rho}{\partial t} dV_y + \int_{\partial P_t} (\rho \hat{v}) \cdot \mathbf{n}_y dS_y = 0$$

$$\int_{P_t} \frac{\partial \rho}{\partial t} dV_y + \int_{P_0} \rho \hat{v} \cdot \mathbf{n} dV_y = 0$$

$r_t$

$\downarrow \frac{y}{\rho}$

$$\int \left[ \frac{\partial \rho}{\partial t} + \underbrace{\nabla_y \cdot (\rho \hat{V})}_{\text{div}} \right] dV_y = 0$$

→ Localized

Balance of mass in Eulerian framework

$$\frac{\partial \rho}{\partial t} + \underbrace{\nabla_y \cdot (\rho \hat{V})}_{\substack{\text{spatial flux} \\ \downarrow \frac{y}{\rho}}} = 0$$

(4)

$$\begin{aligned} S &= \rho \\ f_y &= 0 \\ r_y &= 0 \end{aligned}$$

Note: last time we had

$$\frac{\partial S}{\partial t} + \nabla_y \cdot F_s = r_s$$

$\frac{\partial S}{\partial t}$  → temporal flux density       $\nabla_y \cdot F_s$  → OUTWARD spatial flux density       $r_s$  → source term

$$\frac{\partial \rho}{\partial t} + \nabla_y \cdot \rho \hat{V} = 0$$

$$F_s = \rho \hat{V}$$

non-convective

+  $\rho \hat{V}$  (with a circled X)

Equation (4) can be written in a variety of forms

$$\frac{\partial \rho}{\partial t} + \nabla_y \cdot (\rho \hat{V}) = 0$$

$$\nabla_y \cdot \rho \hat{V} = \frac{\partial}{\partial y_i} (\rho \hat{V}_i) = \underbrace{\frac{\partial \rho}{\partial y_i} V_i}_{\nabla_y \cdot \rho \hat{V}} + \underbrace{\rho \frac{\partial V_i}{\partial y_i}}_{\rho \text{ div } \hat{V}}$$

$$\frac{\partial \rho}{\partial t} + \underbrace{(\nabla_y \cdot \rho \hat{V} + \rho \text{ div } \hat{V})}_{\nabla_y \cdot \rho \hat{V}} = 0$$

$$\left( \frac{\partial \rho}{\partial t} + \nabla_y \cdot \rho \hat{V} \right) + \rho \text{ div } \hat{V} = 0$$

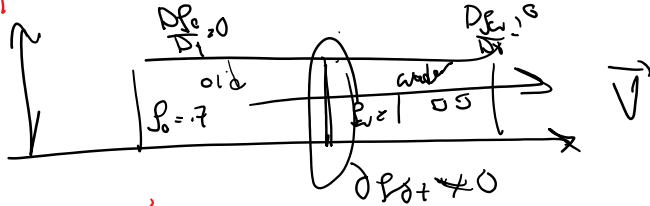
$$\frac{D\rho}{Dt} + \rho \text{ div } \hat{V} = 0$$

$$\frac{\partial \rho}{\partial t} + \nabla_y \cdot \rho \hat{V} = \frac{D\rho}{Dt} + \rho \text{ div } \hat{V} = 0$$

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \mathbf{v} = \frac{D\rho}{Dt} + \rho \operatorname{div} \mathbf{v} = 0$$

air . Compressible  $\rho$  changes in time  
 water or many fluids are nearly incompressible . Means that  
 their density can be considered constant in time.

$$\frac{D\rho}{Dt} = 0 \quad \text{for incompressible fluid}$$



$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \mathbf{v} = \frac{D\rho}{Dt} + \rho \operatorname{div} \mathbf{v} = 0$$

incompressible  $\rightarrow \operatorname{div} \hat{\mathbf{v}} = 0$

$$\frac{\partial \hat{v}_1}{\partial y_1} + \frac{\partial \hat{v}_2}{\partial y_2} + \frac{\partial \hat{v}_3}{\partial y_3} = 0$$

Summary: Conservation of mass

Lagrangian  $\rho(\mathbf{x}, t) = \frac{\rho_0(\mathbf{x})}{J(\mathbf{x}, t)}$

Eulerian  $\frac{\partial \hat{\rho}(\mathbf{y}, t)}{\partial t} + \operatorname{div}(\rho \hat{\mathbf{v}}(\mathbf{y}, t)) = \frac{D\hat{\rho}(\mathbf{y}, t)}{Dt} + \rho \operatorname{div} \hat{\mathbf{v}} = 0$

Incompressibility  $\rho = \rho_0 \Leftrightarrow J(\mathbf{x}, t) = 1$

$\frac{D\hat{\rho}}{Dt} = 0 \Rightarrow \operatorname{div} \hat{\mathbf{v}} = \frac{\partial \hat{v}_i}{\partial y_i} = 0$

Balance of linear momentum:



$$\mathbf{P} = \int_{P_t} (dm) \hat{\mathbf{v}} = \int_{P_t} \rho \hat{\mathbf{v}} dV_y$$

$\rho$  (or  $m$  in fluid mechanics)  
 linear momentum density

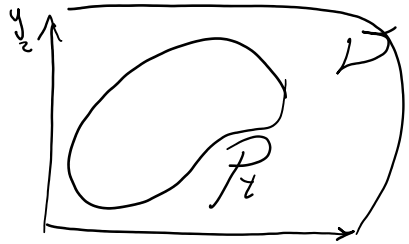
$$\mathbf{P} = \int \rho dV_y \quad \text{NP}$$

$$P = \int_{P_0} p dV_y \quad \vec{P} = \rho \vec{V}$$

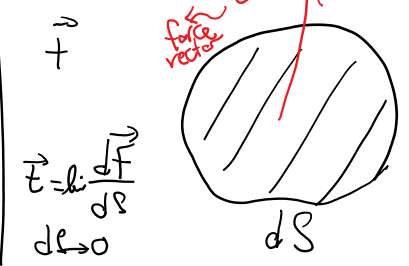
$$\frac{DP}{Dt} = \Sigma \text{ Forces acting in } P$$

$$\frac{DP}{Dt} = \Sigma \text{ Forces} = F_{\text{volumetric}} + F_{\text{surface}}$$

$$= \int_{P_0} \vec{b} \frac{dm}{\rho dV_y} + \int_{\partial P_t} \vec{t} dA_y$$



$\vec{b}$ : body force = force per unit mass  
 e.g. for gravity  $\vec{b} = \begin{bmatrix} 0 \\ 0 \\ -g \end{bmatrix}$   
 $\vec{b}$  has unit of acceleration



$\vec{t} = \lim_{dS \rightarrow 0} \frac{d\vec{F}}{dS}$   
 force on surface is extensive  
 $\Rightarrow$  density of  $\vec{t}$  = traction

$$\frac{DP}{Dt} = \frac{D}{Dt} \int_{P_t} p dV_y = \int_{P_t} \rho \vec{b} dV_y + \int_{\partial P_t} \vec{t} dS_y$$

$\vec{t} = T \cdot \vec{n}_y$  (vector)  
 Cauchy stress tensor  
 2nd order tensor

for now take it as it is

$$\vec{t} = \frac{D}{Dt} \int_{P_t} \rho \vec{b} dV_y - \int_{\partial P_t} \left( \frac{\partial T}{\partial z} \right) \cdot \vec{n}_y dS_y$$

e.g. for  $\vec{g}$   $\frac{DP_g}{Dt} = \frac{D}{Dt} \int_{P_t} \rho \vec{g} dV_y = \int_{P_t} \rho \vec{g} dV_y - \int_{\partial P_t} \frac{\partial p}{\partial y} \cdot \vec{n}_y dS_y$   
 source term for  $\vec{g}$  "diffuse" spatial flux

recall

$$\frac{DP_g}{Dt} = \int_{P_t} \frac{\partial \rho}{\partial t} dV_y + \int_{\partial P_t} \rho \vec{v} \cdot \vec{n}_y dS_y$$

so for  $\vec{g} = \vec{P}$  we'll have

$$\int_{P_t} p b \, dV_y + \int_{\partial P_t} T \cdot n_y \, dS_y = \int_{P_t} \frac{\partial p}{\partial t} \, dV_y + \int_{P_t} p \vec{v} \cdot \vec{n}_y \, dS_y$$

equal

$$\begin{aligned} p \vec{v} \cdot \vec{n} &= (p_i e_i) (v_j n_j) = (p_i v_j n_j) e_i \\ (p \otimes \vec{v}) \cdot \vec{n} &= ((p \otimes v)_k j e_i \otimes e_j) (n_k e_k) = (p_i v_j e_i \otimes e_j) (n_k e_k) \\ &= p_i v_j n_k e_i (e_j \cdot e_k) = \underbrace{\delta_{jk}}_{\delta_{jk}} (p_i v_j n_j) e_i \end{aligned}$$

$$\int_{P_t} \left( \frac{\partial p}{\partial t} - p b \right) \, dV_y + \int_{\partial P_t} (p \otimes v - T) \cdot n_y \, dS_y = 0$$

$$\int_{P_t} \left\{ \frac{\partial p}{\partial t} - p b + \operatorname{div} (p \otimes v - T) \right\} \, dV_y = 0$$

Localized in

Balance of linear momentum / equation of motion (EOM)

$$\frac{\partial p}{\partial t} - p b + \operatorname{div} (p \otimes \vec{v} - \vec{T}) = 0$$

vectors  
 $p = \rho \vec{v}$

$p = \rho \vec{v}$  linear momentum density  
 $T =$  Cauchy stress ( $\sigma$  is often used)  
 2nd order tensor  
 $\vec{m}$  is also used

⑤

Eulerian framework

This equation is the balance of linear momentum in **current configuration**:

- We need to use the current configuration to express balance of linear momentum (forces) because forces are applied in the current configuration.

conservation of mass

$$\frac{\partial \rho}{\partial t} + \operatorname{div} (\rho \vec{v}) = 0$$

scalar      vector

$$\frac{\partial g}{\partial t} + \nabla_y \cdot \vec{F}_g^{\text{total}} = \rho g$$

1 tensorial order higher than  $g$