

From the last time

Balance of linear momentum

$$\textcircled{*} \frac{D}{Dt} \int_{B(t)} \rho dV = \int_{B(t)} \frac{\partial \rho}{\partial t} dV + \int_{\partial B(t)} \rho \otimes \mathbf{v} \cdot \mathbf{n} dS = \int_{B(t)} \rho b dV + \int_{\partial B(t)} \sigma \cdot \mathbf{n} dS$$

$$\int_{B(t)} \frac{\partial \rho}{\partial t} dV + \int_{\partial B(t)} \underbrace{(-\delta + \rho \otimes \mathbf{v})}_{\text{total spatial flux den. for linear momentum}} \cdot \mathbf{n} dS = \int_{B(t)} \rho b dV$$

Apply Div theorem

$$\forall B(t) \int_{B(t)} \left(\frac{\partial \rho}{\partial t} + \nabla_{\mathbf{y}} \cdot (-\delta + \rho \otimes \mathbf{v}) - \rho b \right) dV = 0$$

Apply localization

$\frac{\partial \rho}{\partial t} + \nabla_{\mathbf{y}} \cdot \left(\overbrace{-\delta}^{\text{diffuse flux}} + \overbrace{\rho \otimes \mathbf{v}}^{\text{convective flux}} \right) - \rho b = 0$

Equation of Motion (EOM)

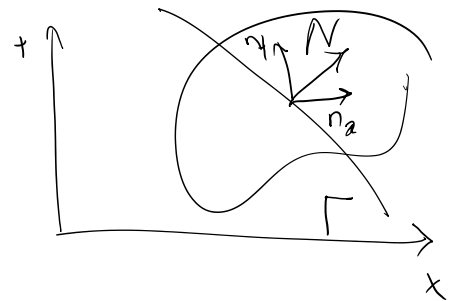
strong form of balance of linear momentum

$\mathbf{P} = \rho \mathbf{v}$ (also $\mathbf{m} = \rho \mathbf{v}$)

①

Next HW

$$M = \begin{bmatrix} -\delta + \rho \otimes \mathbf{v} \\ \mathbf{P} \end{bmatrix} \begin{matrix} \text{spatial} \\ \text{temporal flux} \end{matrix}$$



* solid mechanics infinitesimal theory

$$M = \begin{bmatrix} \mathbf{P} \\ -\delta \end{bmatrix} \quad \mathbf{P} \approx \delta$$

$$[M] \cdot \mathbf{N} = 0$$

$$M = \begin{bmatrix} -\sigma \\ P \end{bmatrix} \quad r \equiv 0$$

$$[M] \cdot \vec{N} = 0$$

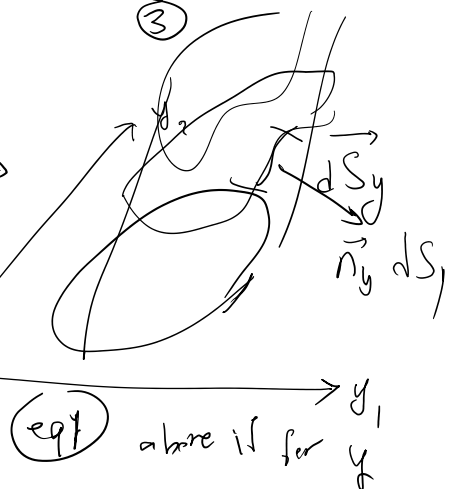
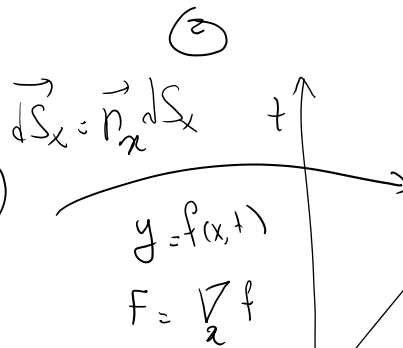
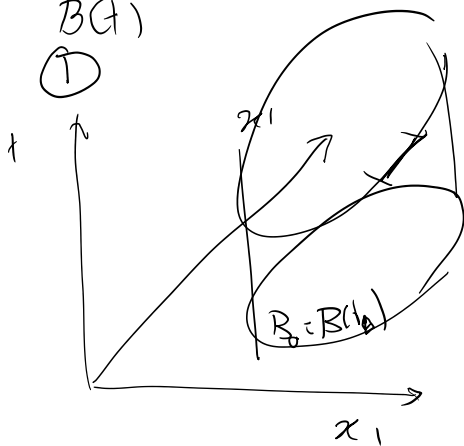
check if
this is correct

$$-\sigma \cdot n_x + [P] \cdot n_x = 0$$

for HW7 problem 2

Lagrangian expression of Balance of linear momentum

$$\textcircled{*} \frac{D}{DT} \int_{B(t)} P \, dV_y = \int_{\partial B(t)} -\sigma n_y \, dS_y + \int_{B(t)} p b \, dV_y$$



term (3)

$$\int_{B(t)} p b \, dV_y = \int_{B_0} p b \left(\frac{D}{DT} dV_x \right) = \int_{B_0} \underbrace{(p \mathcal{J})}_{\rho_0(x)} b \, dV_x$$

$$= \int \rho_0(x) b \, dV_x$$

(i)

domain of integration does not
change in time $\Rightarrow \frac{D}{DT}$ goes inside

term (1)

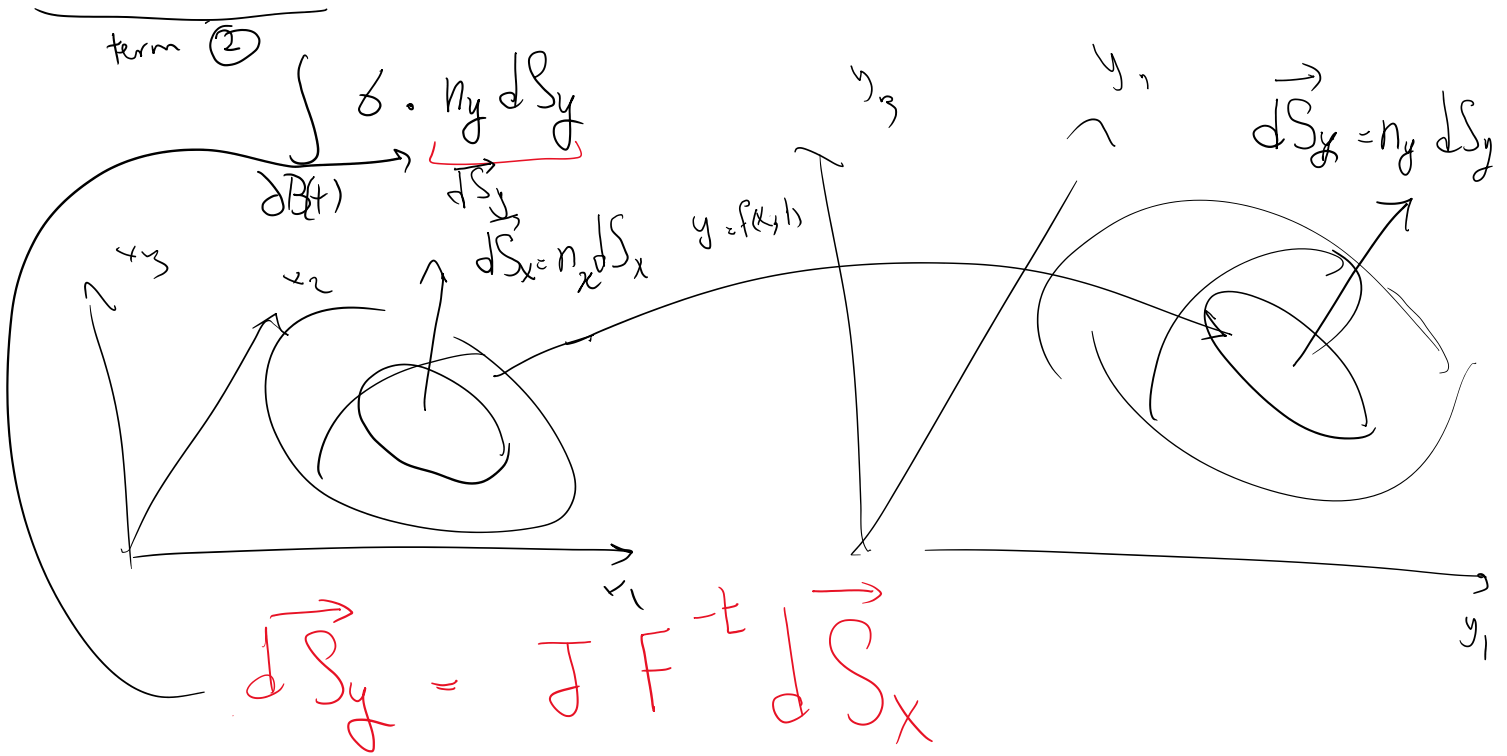
$$\begin{aligned} \frac{D}{DT} \int_{B(t)} P \, dV_y &= \frac{D}{DT} \int_{B_0} P \mathcal{J} \, dV_x = \int_{B_0} \frac{D}{DT} (P \mathcal{J}) \, dV_x \\ &= \int \frac{D}{DT} (P \vec{\mathcal{J}}) \, dV_x = \int \frac{D}{DT} \left(\underbrace{\rho_0 \vec{V}}_{\vec{P} = \rho \vec{V}} \right) \, dV_x = \int \frac{D}{DT} \rho_0 \, dV_x \end{aligned}$$

$\vec{D} = \rho \vec{V}$

$$\int_{\partial B} \dots$$

$$\int_{\partial B} \dots = \int_{\partial B} \dots$$

$\vec{P}_0 = \rho_0 \vec{V}$ Lagrangian (x, t)
 $\vec{P} = \rho \vec{V}$ Eulerian (y, t)



term ② :

$$\int_{\partial B_0} (J \sigma F^{-t}) \vec{dS}_x = \int_{\partial B} \sigma (J F^{-t} \vec{dS}_x) =$$

$$P(x, t) = J(x, t) \sigma(y(x, t), t) F^{-t}(x, t)$$

Piola-Kirchhoff stress tensor

②

Balance of linear momentum in Lagrangian coordinate

$$\begin{aligned}
 \frac{D}{Dt} \int_{B(t)} \rho \, dV_y &= \int_{B(t)} \rho \, b \, dV_y + \int_{\partial B(t)} \sigma \cdot d\vec{S}_y \\
 \downarrow & \quad \downarrow \quad \quad \downarrow \\
 \frac{D}{Dt} \int_{B_0} \rho_0 \, dV_x &= \int_{B_0} \rho_0 \, b \, dV_x + \int_{\partial B_0} \mathbf{P} \cdot d\vec{S}_x \\
 \int_{B_0} \frac{D}{Dt} \rho_0 \, dV_x & \\
 \vec{P}_0 = \rho_0 \vec{v} & \text{ referential linear momentum density}
 \end{aligned}$$

$$\mathbf{P} = \mathbf{J} \boldsymbol{\sigma} \mathbf{F}^{-t}$$

\downarrow \downarrow \downarrow
 PK-I stress Cauchy stress

③

Derive the PDE from ③:

$$\begin{aligned}
 \int_{B_0} \frac{D}{Dt} \rho_0 \, dV_x &= \int_{B_0} \rho_0 \, b \, dV_x + \int_{\partial B_0} \mathbf{P} \cdot d\vec{S}_x \\
 \downarrow & \quad \downarrow \quad \quad \downarrow \\
 \int_{B_0} \nabla_x \cdot \mathbf{P} \, dV_x &
 \end{aligned}$$

$$\forall B_0: \int_{B_0} \left(\frac{D}{Dt} \rho_0 - \rho_0 \, b - \nabla_x \cdot \mathbf{P} \right) dV_x = 0$$

→ localization ⇒ PDE shown below

B_0
 \Rightarrow localization \Rightarrow PDE shown below

Eulerian

$$\frac{\partial}{\partial t} P + \nabla_y \cdot (-\delta + P \otimes v) - \rho b = 0$$

Lagrangian

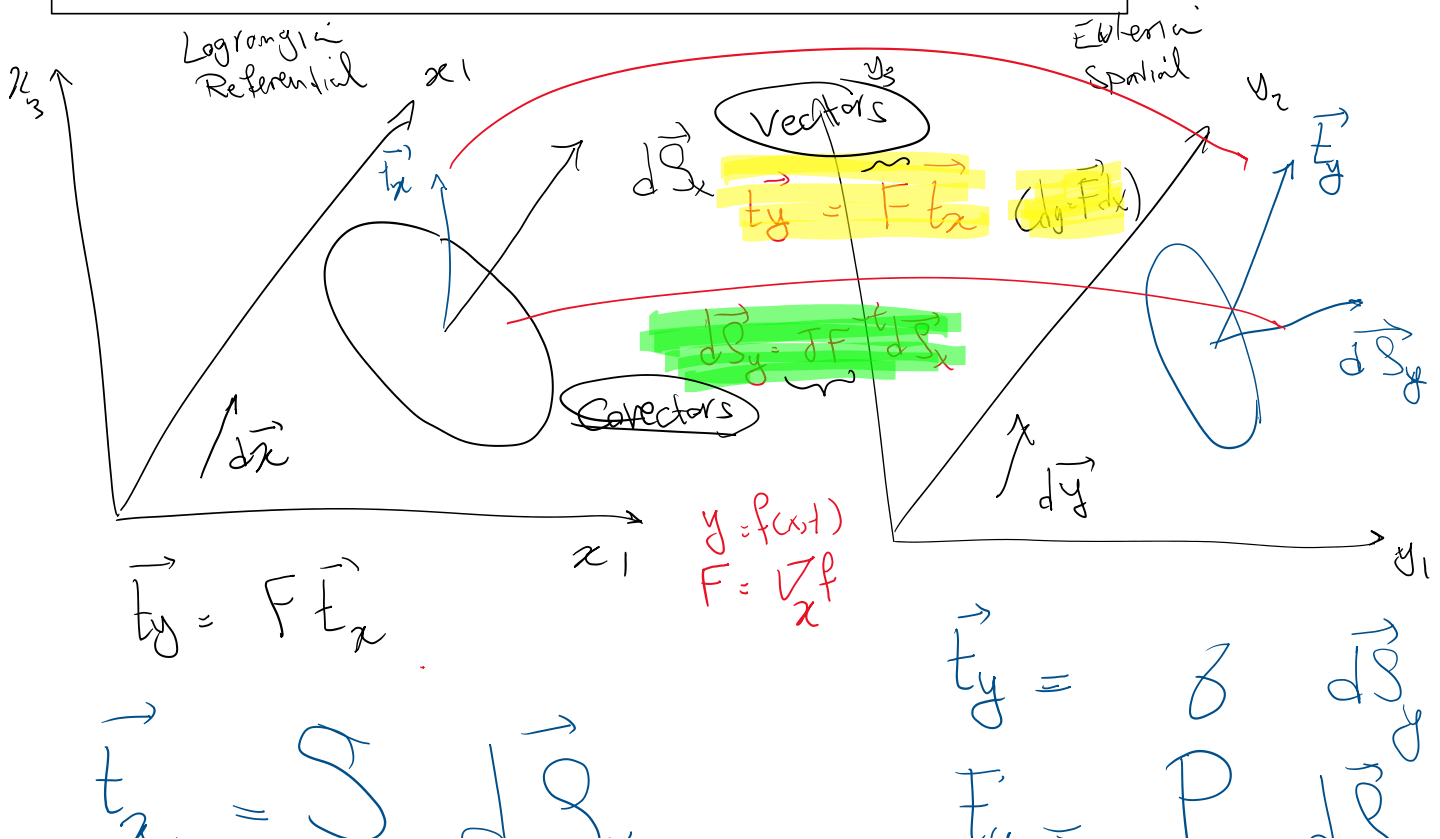
$$\frac{D}{Dt} P_0 - \nabla_x \cdot P - \rho_0 b = 0$$

expanded form

$$P_0 = \rho_0(x) \vec{v}(x,t) \quad \frac{D}{Dt} P_0 = \rho_0 \frac{Dv}{Dt} = \rho_0 \frac{D^2 u}{Dt^2}$$

$$\begin{cases} \rho_0 \ddot{u}_1 - (P_{11,1} + P_{12,2} + P_{13,3}) = \rho_0 b_1 \\ \rho_0 \ddot{u}_2 - (P_{21,1} + P_{22,2} + P_{23,3}) = \rho_0 b_2 \\ \rho_0 \ddot{u}_3 - (P_{31,1} + P_{32,2} + P_{33,3}) = \rho_0 b_3 \end{cases}$$

(4)



$$t_x = \int dS_x$$

$$F_y = P d\vec{S}_x$$

$$\left. \begin{aligned} t_y^{\vec{}} &= P d\vec{S}_x \\ F_y^{\vec{}} &= F t_x^{\vec{}} \end{aligned} \right\} \rightarrow F t_x^{\vec{}} = P d\vec{S}_x$$

$$d\vec{S}_y = J F^t d\vec{S}_x$$

$$\rightarrow t_x^{\vec{}} = F^{-1} P d\vec{S}_x$$

$$P = J \delta F^t$$

Recall

$$d\vec{y} = \underbrace{\nabla_{y/m}}_{\text{F}} d\vec{x}$$

$$t_x^{\vec{}} = \int d\vec{S}_x$$

$$S = J F^{-1} \delta F^t$$

PK-II stress tensor

$$S^t = J (F^{-t})^t \delta^t (F^{-1})^t = J F^{-1} \delta F^t = S$$

$\delta = \delta^t$ balance of angular momentum (TAM 551 note)

S is symmetric and can be advantageous from numerical point of view

EOM: ρ

$$\rho_0 \frac{Dv}{Dt} - \nabla_x \cdot \underbrace{(F/S)}_P - \rho_0 b = 0$$

(5)

as a side note

-1 -1

as a side note

$$\vec{q}_x = \left(\vec{\sigma} \vec{F}^t \right) \vec{q}_y$$

$$d\vec{A}_y = \vec{\sigma} \vec{F}^t d\vec{A}_x$$

Balance of energy:

$$E = K + U + E_{EM}$$

temporal flux of energy

diffuse-spatial flux density

source term

$$\frac{dE}{dt} = -\sigma \cdot v + \rho + \vec{E} \times \vec{H}$$

heat flux density

heat source

Poynting vector

current density

Joule's heating

$$K = \frac{1}{2} \rho v^2$$

kinetic energy density

$$U = \rho \epsilon$$

internal energy density

$\epsilon =$ specific

(Energy per volume)

(Energy per mass)

$$E_{EM} = \frac{1}{2} (\vec{E} \cdot \vec{D} + \vec{B} \cdot \vec{H})$$