

From last time:

**Definition 112 (Noll, 1958)** Given an elastic body and a reference configuration that corresponds to the region  $\overset{0}{\mathcal{B}}$ , the material symmetry group at the material point identified by  $\mathbf{x}$  in the reference configuration is the set

$$\text{Msg}_{\mathbf{x}} = \{ \mathbf{H} \in \text{Unim } \mathcal{V}^+ : \mathbf{G}(\mathbf{FH}, \mathbf{x}) = \mathbf{G}(\mathbf{F}, \mathbf{x}) \ \forall \mathbf{F} \in \text{Lin } \mathcal{V}^+ \}.$$

Again, it should be emphasized that the material symmetry group is characterized by tensors  $\mathbf{H}$  that correspond to the gradients at  $\mathbf{x}$  of deformations — not the deformations themselves. This is because the mass density and the elastic response function in the second reference configuration depend only on the gradient of the connecting deformation. Also, note that  $\mathbf{H} \in \text{Msg}_{\mathbf{x}}$  is not a tensor field, but rather the value of a tensor field at  $\mathbf{x}$ .

The following theorem presents a property of all orthogonal elements of  $\text{Msg}_{\mathbf{x}}$  that derives from the Principle of Material Frame-Indifference.

**Theorem 174** Let  $\mathbf{Q} \in \text{Orth } \mathcal{V}^+$ . Then  $\mathbf{Q} \in \text{Msg}_{\mathbf{x}}$  iff

$$\mathbf{G}(\mathbf{QFQ}^t, \mathbf{x}) = \mathbf{Q} \mathbf{G}(\mathbf{F}, \mathbf{x}) \mathbf{Q}^t \ \forall \mathbf{F} \in \text{Lin } \mathcal{V}^+.$$

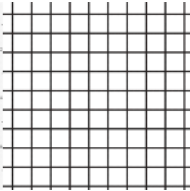
If  $\mathbf{Q}$  is a rotation, for it to belong to symmetry group of constitutive equation  $\mathbf{G}$ , we must have

$$\mathbf{G}(\mathbf{QFQ}^t, \mathbf{x}) = \mathbf{Q} \mathbf{G}(\mathbf{F}, \mathbf{x}) \mathbf{Q}^t \ \forall \mathbf{F} \in \text{Lin } \mathcal{V}^+ \ (\det \mathbf{F} > 0)$$


$$\mathbf{Q} \in \text{Msg}_{\mathbf{x}} \Rightarrow \begin{array}{l} \textcircled{1} \ \mathbf{G}(\mathbf{FQ}) = \mathbf{G}(\mathbf{F}) \quad \text{Noll's definition} \\ \text{objectivity} \quad \textcircled{2} \ \mathbf{G}(\mathbf{QF}) = \mathbf{Q} \mathbf{G}(\mathbf{F}) \mathbf{Q}^t \\ \text{objectivity} \end{array}$$

$$\begin{aligned} \mathbf{F}' = \mathbf{QFQ}^t & \xrightarrow{\textcircled{1}} \mathbf{G}(\underbrace{\mathbf{QFQ}^t}_{\mathbf{F}} \mathbf{Q}) = \mathbf{G}(\mathbf{QFQ}^t) \Rightarrow \\ \mathbf{G}(\mathbf{QFQ}^t) & = \mathbf{G}(\mathbf{QF}) \quad \text{use eqn (2)} \\ & = \mathbf{Q} \mathbf{G}(\mathbf{F}) \mathbf{Q}^t \end{aligned}$$

$G(Q F Q^T) = Q G(F) Q^T$  if  $Q \in \text{Msg}$



rotated by  $90^\circ$   
 $Q$



$Q = \text{Rot}(n60^\circ)$

I will comment on how this can be simplified for linear elasticity (relevant to HW9)

Linear Elasticity:

$\sigma = F \bar{G}(C) F^T$

$C = F^T F, F = \nabla y_x$

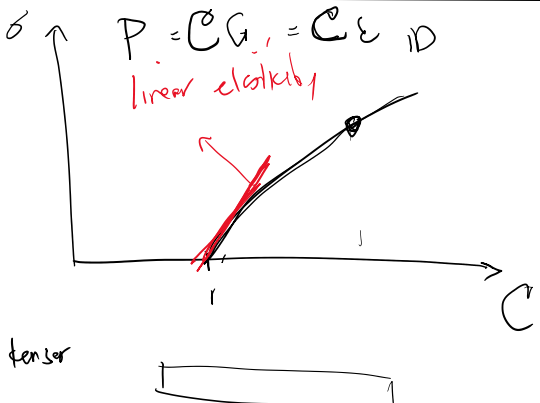
$\sigma = F \bar{G}(C) F^T$

$P = J \bar{\sigma} F^{-T}$

$\downarrow$   
PK-I

$P = J F \bar{G}(C)$  ①

we'll do a Taylor's series around  $C=I$  for  $\bar{G}(C)$



$P = \bar{C} G_{,i} = \bar{C} \epsilon_{iD}$   
 linear elasticity

4th order elasticity tensor

$$f'(x+1) = f(1) + x f'(1) + \frac{x^2}{2} f''(1) + \dots$$

$P = J F \bar{G}(C) = J F (\bar{G}(C-I + I)) = J F (\underbrace{\bar{G}(I)}_0 + (C-I) \frac{\partial \bar{G}(I)}{\partial C}) + O((C-I)^2)$

we assume that the reference is such that for

$F=I (C=I)$  we have zero stress

constitutive eqn

$P = J F \left[ \left( 2 \frac{\partial \bar{G}(I)}{\partial C} \right) \left( \frac{C-I}{2} \right) + O(\epsilon^2) \right] = J F \bar{C} \bar{G}$

$\underbrace{\left\{ \frac{\partial C}{\partial \epsilon} \right\}}_{\substack{\text{4th order} \\ \text{tensor}}} \underbrace{\left\{ 2 \right\}}_G + O(\epsilon^2) \rightarrow \epsilon = ||H|| \rightarrow \text{Green strain}$

$$C_{ijkl} = 2 \frac{\partial \bar{G}_{ij}}{\partial C_{kl}} (I)$$

$$P = \underbrace{\left( 1 + \frac{O(\epsilon)}{\text{trace}(E)} + O(\epsilon^2) \right)}_{\substack{J \\ \text{HW7}}} \underbrace{\left( I + \frac{H}{\alpha \epsilon} \right)}_F \left( \underbrace{C}_{\text{Green}} + O(\epsilon^2) \right)$$

$$= C G + O(\epsilon)$$

$P = C G + O(\epsilon)$

making  $G = \frac{\text{trace}(E)}{2} + O(\epsilon^2)$

$\delta, P, S$  the same within  $O(\epsilon^2)$ ?

linear elasticity  $C = 2 \frac{\partial \bar{G}}{\partial C} (I)$

$\frac{P}{S} = C \begin{matrix} \epsilon \\ G \end{matrix}$

$\delta = C \epsilon$  for linear elasticity

$\delta_{ij} = C_{ijkl} \epsilon_{kk}$

$$\sigma = \begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ & \sigma_{22} & \sigma_{23} \\ & & \sigma_{33} \end{pmatrix}$$

9 comp

same with  $\varepsilon$  in 3D  
3x3

What about  $C$

$$3 \times 3 \times 3 \times 3 = 81 \text{ components}$$

$$\delta_{ij} = \delta_{ji} \quad \rightarrow \quad C_{ijkl} = C_{jikl}$$

$$C_{ijkl} = 2 \frac{\partial \bar{G}_{ij}(C)}{\partial C_{kl}} = 2 \frac{\partial \bar{G}_{ji}(C)}{\partial C_{lk}} = C_{jilk}$$

because  $C_{kl} = C_{lk} \quad (C = C^T)$

minor symmetries of  $C$  tensor

$$C_{\tilde{ij}kl} = C_{\tilde{ji}kl} \quad (3)$$

$$C_{\tilde{ij}\tilde{kl}} = C_{\tilde{ij}\tilde{lk}}$$

Voir notation:

independent values

$$\begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{12} & \sigma_{22} & \sigma_{23} \\ \sigma_{13} & \sigma_{23} & \sigma_{33} \end{pmatrix}$$

$\sigma$  is sym

independent values

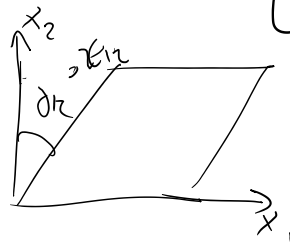
$$\begin{pmatrix} \varepsilon_{11} & \varepsilon_{12} & \varepsilon_{13} \\ \varepsilon_{12} & \varepsilon_{22} & \varepsilon_{23} \\ \varepsilon_{13} & \varepsilon_{23} & \varepsilon_{33} \end{pmatrix}$$

Voigt stress array

$$S = \begin{bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{33} \\ \sigma_{23} \\ \sigma_{13} \\ \sigma_{12} \end{bmatrix} \begin{matrix} \sigma_{12} \\ \sigma_{23} \\ \sigma_{31} = \sigma_{13} \end{matrix}$$

$$\gamma = \begin{bmatrix} \epsilon_{11} \\ \epsilon_{22} \\ \epsilon_{33} \\ 2\epsilon_{23} \\ 2\epsilon_{13} \\ 2\epsilon_{12} \end{bmatrix} = \begin{bmatrix} \epsilon_{11} \\ \epsilon_{22} \\ \epsilon_{33} \\ \gamma_{23} \\ \gamma_{13} \\ \gamma_{12} \end{bmatrix}$$

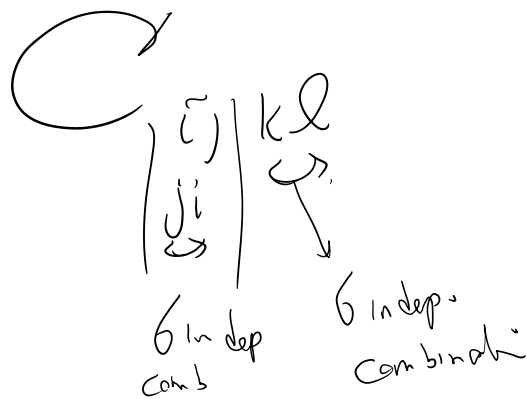
eng shear strains



$$S = \begin{bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{33} \\ \sigma_{23} \\ \sigma_{13} \\ \sigma_{12} \end{bmatrix} = S \gamma$$

$6 \times 6$        $6 \times 1$

Voigt stiffness



out of 81 values in  $C_{ijkl}$  only 36 are independent

$\begin{bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{33} \\ \sigma_{23} \\ \sigma_{13} \end{bmatrix}$	=	<table border="1" style="border-collapse: collapse; width: 100%;"> <tr> <td style="padding: 5px;"><math>E_n \rightarrow \sigma_n</math></td> <td style="padding: 5px;"><math>E_{\text{shear}} \rightarrow \sigma_n</math></td> </tr> <tr> <td style="text-align: center; padding: 5px;"><math>3 \times 3</math></td> <td style="text-align: center; padding: 5px;"><math>3 \times 2</math></td> </tr> <tr> <td style="padding: 5px;"><math>E_n \rightarrow \sigma_{\text{normal}}</math></td> <td style="padding: 5px;"><math>E_{\text{shear}} \rightarrow \sigma_{\text{shear}}</math></td> </tr> </table>	$E_n \rightarrow \sigma_n$	$E_{\text{shear}} \rightarrow \sigma_n$	$3 \times 3$	$3 \times 2$	$E_n \rightarrow \sigma_{\text{normal}}$	$E_{\text{shear}} \rightarrow \sigma_{\text{shear}}$	$\begin{bmatrix} \epsilon_{11} \\ \epsilon_{22} \\ \epsilon_{33} \\ 2\epsilon_{23} \\ 2\epsilon_{13} \end{bmatrix}$
$E_n \rightarrow \sigma_n$	$E_{\text{shear}} \rightarrow \sigma_n$								
$3 \times 3$	$3 \times 2$								
$E_n \rightarrow \sigma_{\text{normal}}$	$E_{\text{shear}} \rightarrow \sigma_{\text{shear}}$								

4

$$\left( \begin{array}{c} \sigma_{23} \\ \sigma_{13} \\ \sigma_{12} \end{array} \right) \left[ \begin{array}{c} \sigma_n \rightarrow \sigma_{shear} \\ \sigma_{13} \\ \sigma_{23} \end{array} \right] \left[ \begin{array}{c} \epsilon_{shear} \rightarrow \sigma_{shear} \\ \epsilon_{13} \\ \epsilon_{23} \end{array} \right] \left( \begin{array}{c} 2\epsilon_{23} \\ 2\epsilon_{13} \\ 2\epsilon_{12} \end{array} \right) \quad (4)$$

Voigt notation

Hyperelastic materials

General elastic material  $\sigma = G(F) \stackrel{\text{objectivity}}{=} F \bar{G}(C) F^t$

Hyperelastic material is more specialized  $e = \bar{e}(F) \stackrel{\text{objectivity}}{=} \bar{e}(C)$   
specific energy

$\Rightarrow \bar{G}(C) = \frac{2p_0}{\sqrt{\det C}} \frac{\partial \bar{e}(C)}{\partial C}$

for the proof see Hyperelastic.pdf

(5)

What's the formula for elasticity tensor  $\mathcal{C}$  for a hyperelastic material

$$\mathcal{C} = 2 \frac{\partial \bar{G}}{\partial C} (I)$$

we derived this above for any elastic material  $\Rightarrow$

hyper elastic  $\bar{G}(C) = \frac{2p_0}{\sqrt{\det C}} \frac{\partial \bar{e}(C)}{\partial C}$

$$\mathcal{C} = 2 \frac{\partial \left( \frac{2p_0}{\sqrt{\det C}} \frac{\partial \bar{e}(C)}{\partial C} \right)}{\partial C} =$$

$$C^0 = 2 \frac{\partial \left( \frac{1}{\sqrt{\det C}} \right)}{\partial C} \Big|_{C=I} =$$

$$4\rho_0 \left( \frac{\partial \frac{1}{\sqrt{\det C}}}{\partial C} \frac{\partial \bar{e}(C)}{\partial C} + \frac{1}{\sqrt{\det C}} \frac{\partial^2 \bar{e}(C)}{\partial C \partial C} \right) \Big|_{C=I}$$

(ab)' = a'b + ab'

$$= 4\rho_0 \left[ \frac{\partial \frac{1}{\sqrt{\det C}}}{\partial C} \Big|_{C=I} \frac{\partial \bar{e}}{\partial C}(I) + \frac{1}{\sqrt{\det I}} \frac{\partial^2 \bar{e}}{\partial C \partial C}(I) \right]$$

Recall  $\partial_c F \bar{G}(C) F^t = F \frac{2\rho_0}{\sqrt{\det C}} \frac{\partial \bar{e}}{\partial C}(C) F^t$

if  $C=I$   $\partial(C=I) = F \frac{2\rho_0}{\sqrt{\det I}} \left( \frac{\partial \bar{e}}{\partial C}(I) \right) F^t = 0$

For hyperelastic materials we have

$$C = 4\rho_0 \frac{\partial^2 \bar{e}}{\partial C \partial C} (C=I)$$

$$C_{ijkl} = 4\rho_0 \frac{\partial^2 \bar{e}}{C_{ij} \partial C_{kl}} (C=I)$$

$$= 4\rho_0 \frac{\partial^2 \bar{e}}{\partial C_{kl} \partial C_{ij}} (C=I) = C_{kl ij}$$

$$\frac{\partial^2 f}{\partial a \partial b} = \frac{\partial^2 f}{\partial b \partial a}$$

$$\frac{\partial^2 T}{\partial a \partial b} = \frac{\partial^2 T}{\partial b \partial a}$$

For hyperelastic

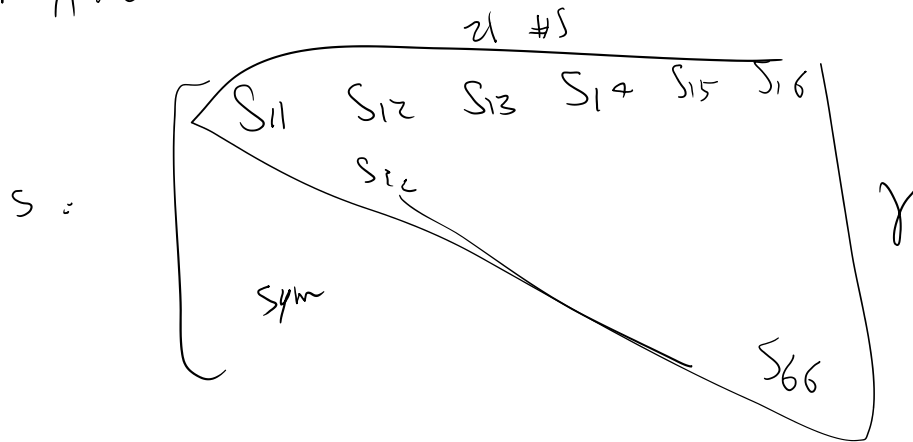
$$\mathbb{C} = 4g_0 \frac{\partial^2 \bar{e}}{\partial C \partial C} (I)$$

$$\mathbb{C}_{ijkl} = \mathbb{C}_{klij} \quad \text{major symmetry}$$

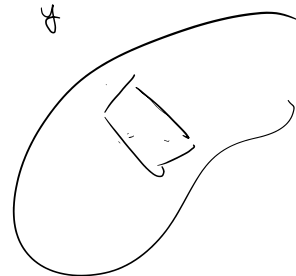
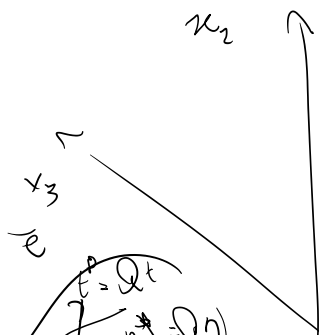
& it still has minor symmetries that any elastic material has

$$\mathbb{C}_{ijkl} = \mathbb{C}_{jilk} \quad , \quad \mathbb{C}_{ijkl} = \mathbb{C}_{ijlk}$$

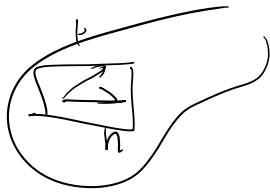
$S = S^T$  in this case  $S$  is symmetric for hyperelastic material



$$y^* (x, t) = c(t) + Q(t) y(x, t)$$







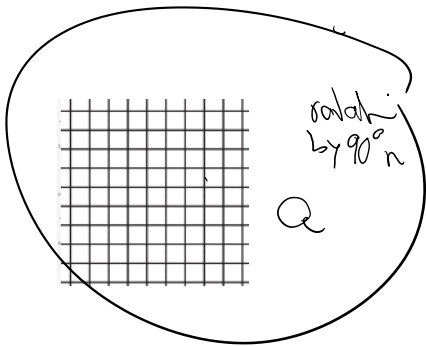
$$\sigma^* = Q \sigma Q^T$$

$$\sigma_{ij}^* = Q_{im} Q_{jn} \sigma_{mn}$$

$$C = ?$$

$$C_{ijkl} = Q_{im} Q_{jn} Q_{kp} Q_{lq} C_{mnpq}$$

What if  $Q$  is in symmetry group for constitutive equation of stress ( $C$ )



$$Q = Rot(60^\circ)$$

$Q$  is in symmetry group iff

$$C_{ijkl} = Q_{im} Q_{jn} Q_{kp} Q_{lq} C_{mnpq}$$

$$C_{ijkl} = C_{ijkl}$$

For an isotropic elastic material, we only have 2 independent parameters

$$E, \nu$$

$E, \nu$

$\lambda, \mu$ : Lamé's parameters

$$C_{ijkl} = \lambda \delta_{ij} \delta_{kl} + \mu (\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk})$$

[https://en.wikipedia.org/wiki/Lam%C3%A9\\_parameters](https://en.wikipedia.org/wiki/Lam%C3%A9_parameters)

3D formulae	$K =$	$E =$	$\lambda =$	$G =$	$\nu =$	$M =$	Notes
$(K, E)$			$\frac{3K(3K-E)}{9K-E}$	$\frac{3KE}{9K-E}$	$\frac{3K-E}{6K}$	$\frac{3K(3K+E)}{9K-E}$	
$(K, \lambda)$		$\frac{9K(K-\lambda)}{3K-\lambda}$		$\frac{3(K-\lambda)}{2}$	$\frac{\lambda}{3K-\lambda}$	$3K - 2\lambda$	
$(K, G)$		$\frac{9KG}{3K+G}$	$K - \frac{2G}{3}$		$\frac{3K-2G}{2(3K+G)}$	$K + \frac{4G}{3}$	
$(K, \nu)$		$3K(1-2\nu)$	$\frac{3K\nu}{1+\nu}$	$\frac{3K(1-2\nu)}{2(1+\nu)}$		$\frac{3K(1-\nu)}{1+\nu}$	
$(K, M)$		$\frac{9K(M-K)}{3K+M}$	$\frac{3K-M}{2}$	$\frac{3(M-K)}{4}$	$\frac{3K-M}{3K+M}$		
$(E, \lambda)$	$\frac{E+3\lambda+R}{6}$			$\frac{E-3\lambda+R}{4}$	$\frac{2\lambda}{E+\lambda+R}$	$\frac{E-\lambda+R}{2}$	$R = \sqrt{E^2 + 9\lambda^2 + 2E\lambda}$
$(E, G)$	$\frac{EG}{3(3G-E)}$		$\frac{G(E-2G)}{3G-E}$		$\frac{E}{2G} - 1$	$\frac{G(4G-E)}{3G-E}$	
$(E, \nu)$	$\frac{E}{3(1-2\nu)}$		$\frac{E\nu}{(1+\nu)(1-2\nu)}$	$\frac{E}{2(1+\nu)}$		$\frac{E(1-\nu)}{(1+\nu)(1-2\nu)}$	
$(E, M)$	$\frac{3M-E+S}{6}$		$\frac{M-E+S}{4}$	$\frac{3M+E-S}{8}$	$\frac{E-M+S}{4M}$		$S = \pm \sqrt{E^2 + 9M^2 - 10EM}$ There are two valid solutions. The plus sign leads to $\nu \geq 0$ . The minus sign leads to $\nu \leq 0$ .
$(\lambda, G)$	$\lambda + \frac{2G}{3}$	$\frac{G(3\lambda+2G)}{\lambda+G}$			$\frac{\lambda}{2(\lambda+G)}$	$\lambda + 2G$	
$(\lambda, \nu)$	$\frac{\lambda(1+\nu)}{3\nu}$	$\frac{\lambda(1+\nu)(1-2\nu)}{\nu}$		$\frac{\lambda(1-2\nu)}{2\nu}$		$\frac{\lambda(1-\nu)}{\nu}$	Cannot be used when $\nu = 0 \Leftrightarrow \lambda = 0$
$(\lambda, M)$	$\frac{M+2\lambda}{3}$	$\frac{(M-\lambda)(M+2\lambda)}{M+\lambda}$		$\frac{M-\lambda}{2}$	$\frac{\lambda}{M+\lambda}$		
$(G, \nu)$	$\frac{2G(1+\nu)}{3(1-2\nu)}$	$2G(1+\nu)$	$\frac{2G\nu}{1-2\nu}$			$\frac{2G(1-\nu)}{1-2\nu}$	
$(G, M)$	$M - \frac{4G}{3}$	$\frac{G(3M-4G)}{M-G}$	$M - 2G$			$\frac{M-2G}{2M-2G}$	
$(\nu, M)$	$\frac{M(1+\nu)}{3(1-\nu)}$	$\frac{M(1+\nu)(1-2\nu)}{1-\nu}$	$\frac{M\nu}{1-\nu}$	$\frac{M(1-2\nu)}{2(1-\nu)}$			
2D formulae	$K_{2D} =$	$E_{2D} =$	$\lambda_{2D} =$	$G_{2D} =$	$\nu_{2D} =$	$M_{2D} =$	Notes

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