

2018/02/28

Wednesday, February 28, 2018

11:37 AM

(6)

$$\begin{array}{c} n^- = 1 \quad n^+ = -1 \\ \rightarrow \quad \leftarrow \\ \vec{v} \end{array}$$

$a_{4x1} \text{ does}$   
 $\text{of the interface}$

$$u^- = [1 \quad 1 \quad | \quad 0 \quad 0] a, \quad u^+ = [0 \quad 0 \quad | \quad 1 \quad 0] a$$

$$[[u]] = u^- \cdot n^- + u^+ \cdot n^+ - u^- \cdot v - u^+ \cdot v = [1 \quad 1 \quad | \quad -1 \quad 0] a$$

$$v^- = [1 \quad 1 \quad | \quad 0 \quad 0] \dot{a} \quad v^+ = [0 \quad 0 \quad | \quad 1 \quad 0] \dot{a}$$

$$\lambda^- \delta^- \cdot n^- = [0 \quad \frac{k^- \lambda^-}{h^-} \quad | \quad 0 \quad 0] \quad \lambda^+ \delta^+ \cdot n^+ = [0 \quad 0 \quad | \quad 0 \quad \frac{\lambda^+ k^+}{h^+}]$$

$$\lambda^- \delta^- \cdot n^- + \lambda^+ \delta^+ \cdot n^+ = [0 \quad \frac{k^- \lambda^-}{h^-} \quad | \quad 0 \quad -\frac{\lambda^+ k^+}{h^+}]$$

$$\delta^- = [0 \quad \frac{k^-}{h^-} \quad | \quad 0 \quad 0] a \quad \delta^+ = [0 \quad 0 \quad | \quad 0 \quad \frac{k^+}{h^+}] a$$

Terms from interior interface in 1D,  $\rho = 1$

$$\tilde{T}_u = -[[u]] \delta^+$$

$$\tilde{I}_U = -\tilde{I}_U \nabla \psi^0$$

$$= - \begin{bmatrix} 1 \\ 1 \\ -1 \\ 0 \end{bmatrix} \left( \sum_{\delta^-} \bar{\delta}^- + \sum_{\delta^+} \delta^+ + \sum_V \bar{V} + \sum_V V^+ \right)$$

$$= - \begin{bmatrix} 1 \\ 1 \\ -1 \\ 0 \end{bmatrix} \left( \sum_{\delta^-} \left[ \begin{smallmatrix} 0 & \frac{K}{h} & 0 & 0 \end{smallmatrix} \right] \dot{Q} + \sum_{\delta^+} \left[ \begin{smallmatrix} 0 & 0 & 0 & \frac{K^+}{h^+} \end{smallmatrix} \right] \dot{Q} \right. \\ \left. + \sum_V \left[ \begin{smallmatrix} 1 & 1 & 0 & 0 \end{smallmatrix} \right] \ddot{A} + \sum_V \left[ \begin{smallmatrix} 0 & 0 & 1 & 0 \end{smallmatrix} \right] \ddot{A} \right)$$

$\tilde{I}_U$  term  $\rightarrow$

$$- \begin{bmatrix} 1 \\ 1 \\ -1 \\ 0 \end{bmatrix} \left( \sum_{\delta^-} \left[ \begin{smallmatrix} 0 & \frac{K}{h} & 0 & 0 \end{smallmatrix} \right] + \sum_{\delta^+} \left[ \begin{smallmatrix} 0 & 0 & 0 & \frac{K^+}{h^+} \end{smallmatrix} \right] \right) Q$$

$K^I$  goes to  $K_{4 \times 4}^I$  Interface stiffness  $4 \times 4$

$$- \begin{bmatrix} 1 \\ 1 \\ -1 \\ 0 \end{bmatrix} \left( \left( \sum_V \left[ \begin{smallmatrix} 1 & 1 & 0 & 0 \end{smallmatrix} \right] + \left( \sum_V \left[ \begin{smallmatrix} 0 & 0 & 1 & 0 \end{smallmatrix} \right] \right) \right) \ddot{A} \right)$$

$C$  goes to  $D_{4 \times 4}^I$  interface damping

Other term

$$\tilde{f}_g = \lambda \tilde{\delta} \cdot \tilde{n}^- (-\tilde{v}^+ \tilde{v}^-) + \lambda \tilde{\delta}^T \cdot \tilde{n}^+ (-\tilde{v}^+ \tilde{v}^-)$$

$$v^* = \sqrt{\tilde{v}^-} \tilde{\delta}^- + \sqrt{\tilde{v}^+} \tilde{\delta}^+ + \sqrt{\tilde{v}^-} v^- + \sqrt{\tilde{v}^+} v^+$$

$$= (\lambda \tilde{\delta} \cdot \tilde{n}) (-v^*) + \lambda \tilde{\delta} \cdot \tilde{n}^- v^- + \lambda \tilde{\delta}^T \cdot \tilde{n}^+ v^+$$

$$(\lambda \tilde{\delta} \cdot \tilde{n}) = \tilde{\delta} \tilde{\delta}^- \cdot \lambda \tilde{\delta}^T \tilde{\delta}^+$$

$$= -(\lambda \tilde{\delta} \cdot \tilde{n}) \left( \underbrace{\sqrt{\tilde{v}^-} \tilde{\delta}^- + \sqrt{\tilde{v}^+} \tilde{\delta}^+}_{K_2} + \underbrace{\sqrt{\tilde{v}^-} v^- + \sqrt{\tilde{v}^+} v^+}_{C_2} \right) \\ + (\lambda \tilde{\delta} \cdot \tilde{n})^- v^- + (\lambda \tilde{\delta} \cdot \tilde{n})^T v^+ = C_2$$

$$= (K_2) \dot{a} + C_2 \ddot{a}$$

$$K_2 = -(\lambda \tilde{\delta} \cdot \tilde{n}) \left( \sqrt{\tilde{v}^-} \begin{bmatrix} 0 \\ \tilde{\delta}^- \\ 0 \\ 0 \end{bmatrix}^T + \sqrt{\tilde{v}^+} \begin{bmatrix} 0 \\ 0 \\ 0 \\ \tilde{\delta}^+ \end{bmatrix}^T \right)$$

$$① C_2 = -(\lambda \tilde{\delta} \cdot \tilde{n}) \left( \sqrt{\tilde{v}^-} \begin{bmatrix} 1 & 1 & 1 & 0 & 0 \end{bmatrix}^T + \sqrt{\tilde{v}^+} \begin{bmatrix} 0 & 0 & 1 & 0 & 0 \end{bmatrix}^T \right)$$

$$+ (\lambda \tilde{\delta} \cdot \tilde{n})^- \begin{bmatrix} 1 & 1 & 0 & 0 \end{bmatrix}^T + (\lambda \tilde{\delta} \cdot \tilde{n})^T \begin{bmatrix} 0 & 0 & 1 & 0 \end{bmatrix}^T$$

$$\lambda \tilde{\delta}^- = \begin{bmatrix} 0 \\ -\frac{1}{2} \tilde{\delta}^- \\ 0 \\ 0 \end{bmatrix}$$

$$\lambda \tilde{\delta}^+ = \begin{bmatrix} 0 \\ 0 \\ 0 \\ \frac{1}{2} \tilde{\delta}^+ \end{bmatrix}$$

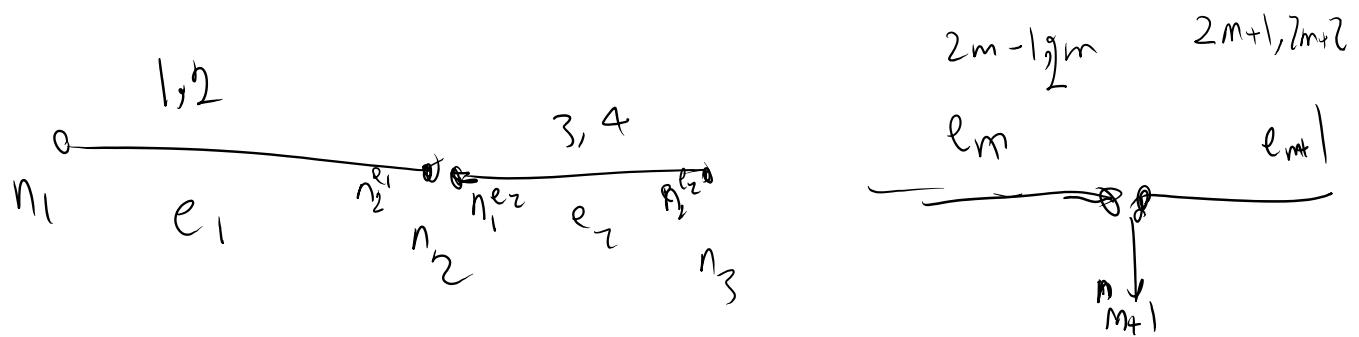
$$\lambda \tilde{\delta} = \begin{bmatrix} 0 \\ -\frac{1}{2} \tilde{\delta}^- \\ 0 \\ 0 \\ \frac{1}{2} \tilde{\delta}^+ \end{bmatrix}$$

$$\begin{bmatrix} 0 \\ 0 \end{bmatrix} \quad \text{and} \quad \begin{bmatrix} 0 \\ \lambda K_h^+ \end{bmatrix} \quad \text{and} \quad \begin{bmatrix} 0 \\ \lambda^T K^+ h^+ \end{bmatrix}$$

$$K^t = K_1 + K_2 \quad 4 \times 4 \quad \text{matrix}$$

$$C^S = C_1 + C_2 \quad 4 \times 4 \quad \text{matrix}$$

We assemble these to the global system



$$C^t = \begin{bmatrix} 2m-1 & 2m & 2m+1 & 2m+2 \\ 2m & 2m+1 & 2m+2 & 2m+3 \\ 2m+1 & 2m+2 & 2m+3 & 2m+4 \\ 2m+2 & 2m+3 & 2m+4 & 2m+5 \end{bmatrix}$$

for interface  
of node  
 $m+1$

assembled to the global  
damping matrix

Same process is repeated for  $K^t \rightarrow$  assembled to  $K$

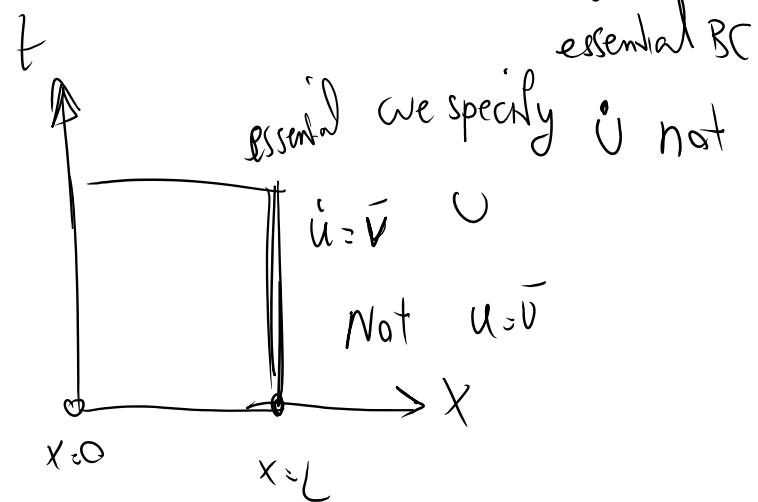
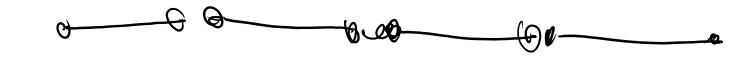
same process is repeated for  $K^I$  assembled to  $K$

Essential Boundary:

$$B(u, \tilde{v}) = - \int_{\partial e} \tilde{u} (\delta \cdot n) ds + \lambda \int_{\partial e} \delta \cdot n (-\tilde{v} + v) ds$$

$$\begin{aligned} V^* &= \bar{V} \\ \delta^* &= \delta \end{aligned}$$

$$\tilde{u}^* = \bar{u}$$



if we specifying  $u(x=L, t) = \bar{u}(t) \Rightarrow$   
 $v(x=L, t) = \bar{v}(t) = \bar{u}(t) - \bar{v}(t)$

$$B(u, \tilde{v}) = - \int_{\partial e_u} \tilde{u} (\delta \cdot n) ds + \lambda \int_{\partial e_u} \delta \cdot n (-\tilde{v} + v) ds$$

→ 1D

$$-\tilde{u} \cdot (\delta \cdot n) + \lambda \int_{\partial e_u} \delta \cdot n (-\tilde{v} + v) ds \quad @ \text{essential BC}$$

$$-\hat{u} \cdot (\delta \cdot n) + \lambda \delta \cdot n (-V + V) \quad \text{at essential BC}$$

stress  
 RHS force  
 damping

$$\begin{aligned} n &= -1 & x &= 0 \\ u &= [1 \ 0]^T a & V &= [1 \ 1]^T a \\ \delta &= [0 \ \frac{K}{h}] a & \lambda &= [0 \ \frac{K}{h}] a \end{aligned}$$

$$\begin{array}{c} x=L \\ u=[1 \ 1]e \quad n=1 \\ V=[1 \ 1]a \\ \lambda=[0 \ \frac{K}{h}]a \end{array}$$

$$K_{\text{contribution}} = -\hat{u}(\delta \cdot n)$$

$$\begin{bmatrix} 1 \\ 0 \end{bmatrix} \begin{bmatrix} 0 & \frac{K}{h} \end{bmatrix} - \begin{bmatrix} 1 \\ 1 \end{bmatrix} \begin{bmatrix} 0 & \frac{K}{h} \end{bmatrix}$$

$$C_{\text{contribution}} = \lambda \delta \cdot n V$$

$$-\lambda \begin{bmatrix} 0 \\ K_h \end{bmatrix} \begin{bmatrix} 1 & 0 \end{bmatrix} + \lambda \begin{bmatrix} 0 \\ K_h \end{bmatrix} \begin{bmatrix} 1 & 1 \end{bmatrix}$$

$$F_{\text{contribution}} = \lambda \delta \cdot n V$$

$$-\lambda \begin{bmatrix} 0 \\ K_h \end{bmatrix} \bar{V} + \lambda \begin{bmatrix} 0 \\ K_h \end{bmatrix} \bar{V}$$

②

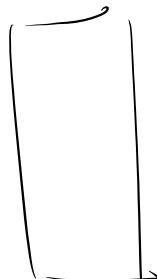
Natural boundary

$$B(\hat{u}, u) = \int_{\partial\Omega} \hat{u} (\delta^* \cdot n) ds + \lambda \int_{\partial\Omega} \delta \cdot n (-V^* + V) ds$$

def

$$\boxed{\begin{aligned} V^* &= V \\ \delta^* \cdot n &= \bar{\delta} \end{aligned}}$$

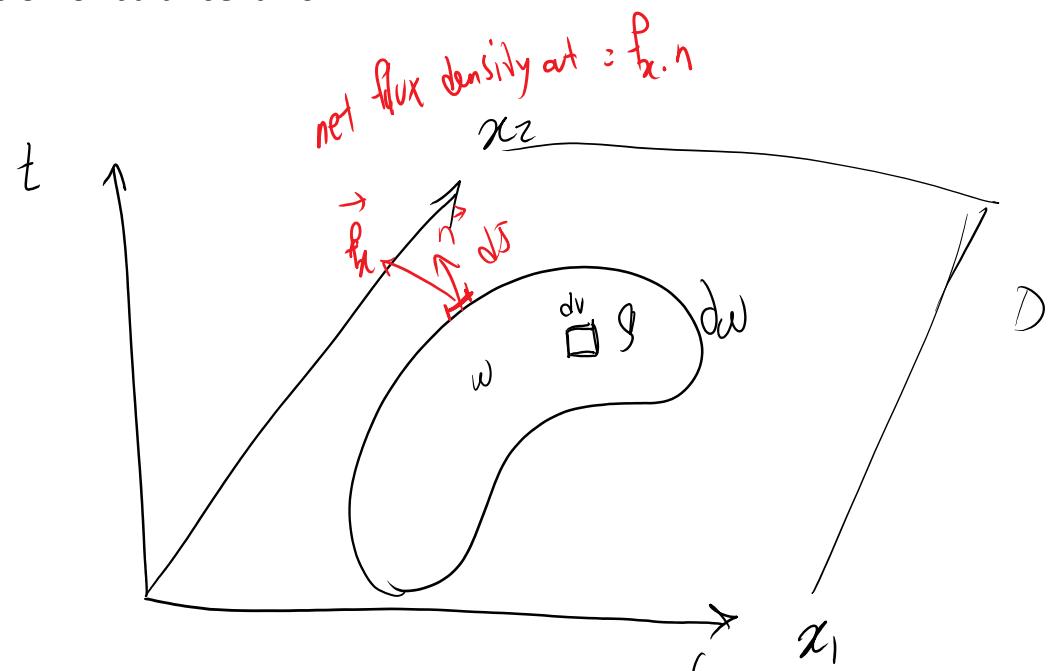
1D



$$B(\vec{u}, \vec{u}) = -\vec{u} \cdot \vec{\delta}$$

only contributes to the force  
vector

Spacetime expression of balance laws



For a static problem

$$-\int_{\partial\omega} f_x \cdot n \, ds + \int_{\omega} S \, dv = 0$$

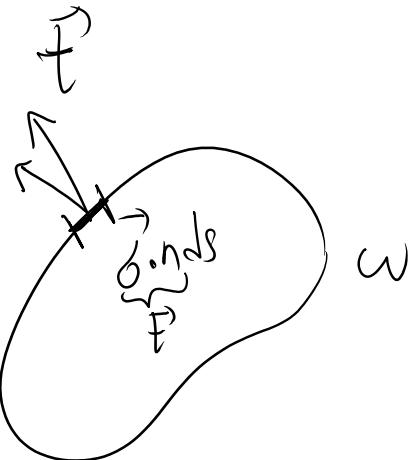
$\downarrow$   
 $f_x \cdot n = 0$  on the boundary

$\frac{\partial w}{\partial \omega}$   
 net gain of a quantity  
 from  $\partial \omega$  source term or  
interior contr.

Example:

Solid Mechanics

force (linear momentum)  
static version



because:  
fraction ADDS  
Not subtract forces  
to  $w$

$$-\int_{\partial \omega} (\mathbf{f} \cdot \mathbf{n}) ds + \int_{\omega} (\rho b) \cdot d\mathbf{v} = 0$$

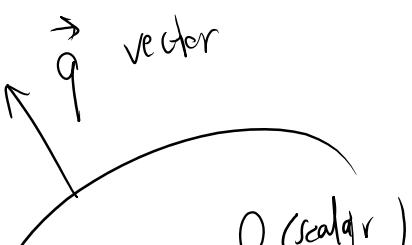
$$\int_{\partial \omega} \mathbf{f} \cdot \mathbf{n} ds + \int_{\omega} \rho b d\mathbf{v} = 0$$

Gauss theorem

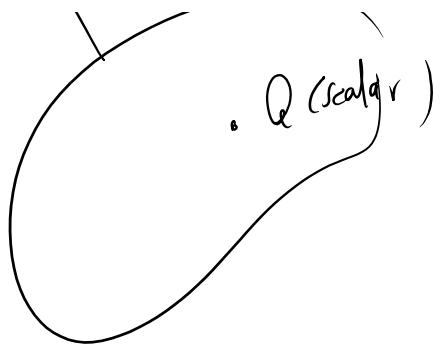
$$\begin{cases} (\mathbf{f} \cdot \mathbf{n} + \rho b) d\mathbf{v} = 0 & \text{P.D.} \\ \text{on } \omega \setminus \Gamma \rightarrow \text{jump set} \\ [\mathbf{f}] \cdot \mathbf{n} = 0 & \text{Jump condn.} \end{cases}$$

Another example

$$-\int \vec{q} \cdot \mathbf{n} ds + \int Q d\mathbf{v} = 0$$



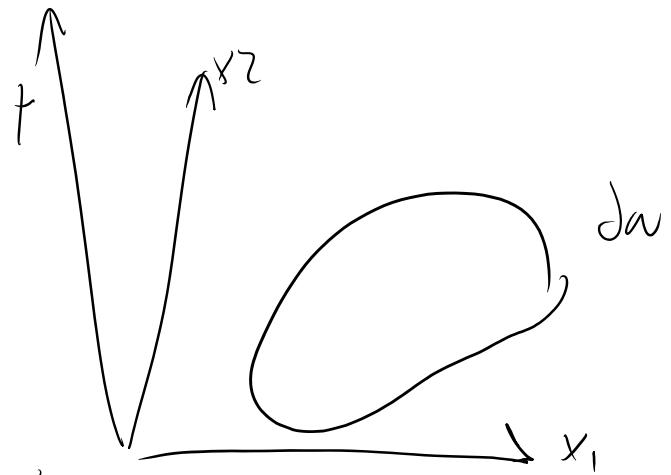
$$-\int_{\partial W} \vec{q} \cdot \vec{n} ds + \int_W Q dv = 0$$



$$\begin{cases} -\nabla \cdot \vec{q} + Q = 0 & \text{PDE} \\ [\vec{q}] \cdot \vec{n} = 0 & \text{Jump conditions} \end{cases}$$

What if the problem is dynamic?

Example: Heat Conduction



$$-\int_{\partial W} q_n ds + \int_W Q dv \cancel{=} \frac{d}{dt} \text{Energy in } W$$

$\underbrace{\quad}_{\text{Input energy/time}}$

= Input power

$$= \frac{d}{dt} \int_W (e) dv$$

energy density  
per unit volume

$$e = e_{el}(\varepsilon) + \underbrace{e_M}_{+} + \frac{1}{2}PV^2 + \dots$$

+  ~~$e(T)$~~   $\rightarrow$  thermal part

If  $e(T)$  is linear

$$C_v T$$

Volumetric heat capacity

$$-\int_{\partial\omega} q \cdot n ds + \int_{\omega} Q dv = \frac{d}{dt} \int_{\omega} (C_v T) dv \quad (3)$$

→

$$\frac{d}{dt} \int_{\omega} (C_v T) dv + \int_{\partial\omega} q \cdot n ds = \int_{\omega} Q dv$$

vol. energy density

exit energy

spatial flux

source law

quantity balanced

Volumetric density of that

# Solid Mechanics

$\frac{\text{mass} \times \text{velocity}}{\text{volume}}$

$$\frac{D}{Dt} \vec{P} = \sum \text{Forces}$$

$P = \text{mass} \times \text{velocity}$

$\left( \frac{\text{mass}}{\text{volume}} \right) \times \text{velocity}$

$$\vec{p} = \rho \vec{V}$$

(linear momentum density)

$$\frac{d}{dt} P = \frac{d}{dt} \int_{\Omega} p dV = \sum \text{forces} = - \oint_{\partial\Omega} (-p) n dS + \int_{\Omega} p_b dV$$

volumetric flux  
of balanced quantity

outward  
spatial flux source term

Balance of Mass in Eulerian Framework

$$\frac{d}{dt} \int_{\Omega} p dV = - \int_{\partial\Omega} p \vec{v} \cdot \vec{n} dS + 0$$

# General form of a balance law:

$$\frac{d}{dt} \int_{\mathcal{V}} F = \frac{d}{dt} \int_{\mathcal{W}} \underbrace{\rho_t f_t dV}_{\text{volumetric density } f_t F} = - \int_{\partial \mathcal{W}} f_{x.h} ds + \int_{\mathcal{W}} S dV$$

(4)

**balanced quantity**  
(energy, mass, linear momentum)

**volumetric density**  $f_t F$

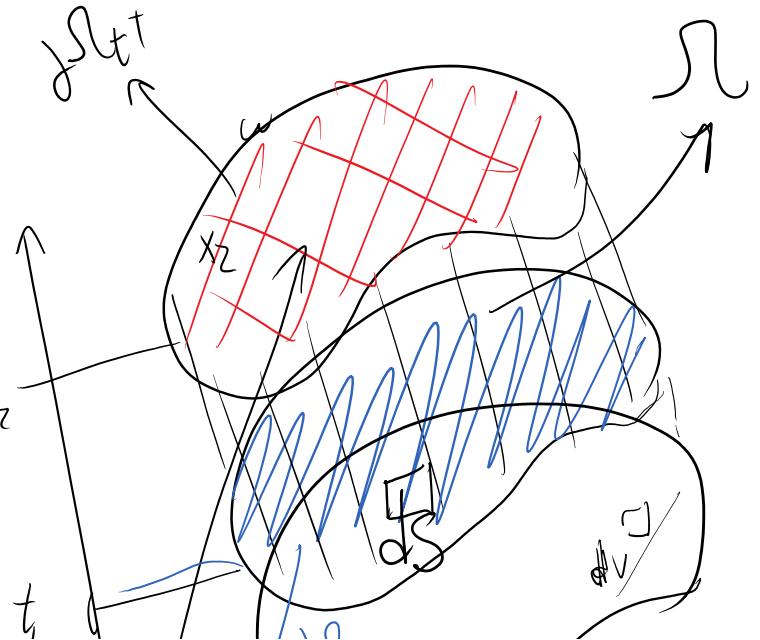
**outward spatial flux**

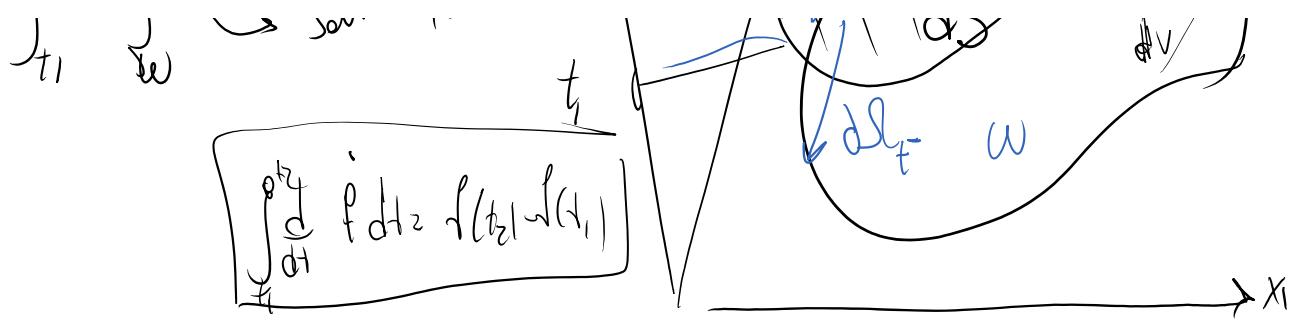
**source term**

$$(4) \rightarrow \frac{d}{dt} \int_{\mathcal{V}} \rho_t f_t dV + \int_{\partial \mathcal{W}} f_{x.h} ds \int_{\mathcal{V}} f dV \xrightarrow{\text{source term}}$$

Integrate this over time

$$\begin{aligned} & \int_{t_1}^{t_2} \left( \int_{\mathcal{V}} \rho_t f_t dV \right) dt + \int_{t_1}^{t_2} \int_{\partial \mathcal{W}} f_{x.h} ds \\ &= \int_{t_1}^{t_2} dt \int_{\mathcal{V}} f dV \xrightarrow{\text{source term}}$$





$$\int_{t_1}^{t_2} \left( \frac{1}{\rho} \int_{\omega} f_t d\nu \right) dt = \left[ f_t d\nu \right]_{t=t_2} - \left[ f_t d\nu \right]_{t=t_1}$$

5.ii

$$= \frac{\int f_t dS}{\partial S_{f,t}} - \frac{\int f_t dS}{\partial S_{f,t}}$$

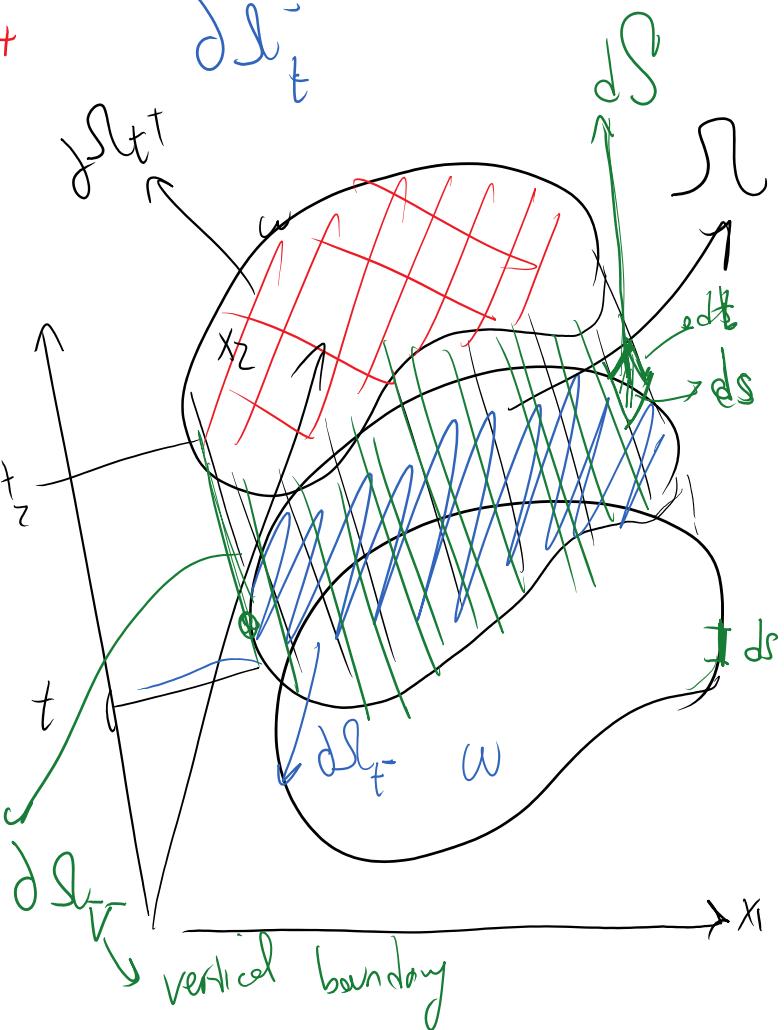
$$\int_{t_1}^{t_2} \left( \int_{\omega} f_{x,n} ds \right) dt$$

$$= \iint_{\omega} \int_{t_1}^{t_2} \left( f_{x,n} \right) \left( \frac{ds}{dt} \right) dt$$

$$= \int \left( f_{x,n} \right) dS$$

5.iii

$$\frac{\partial S_{f,t}}{\partial t} \rightarrow \text{vertical}$$



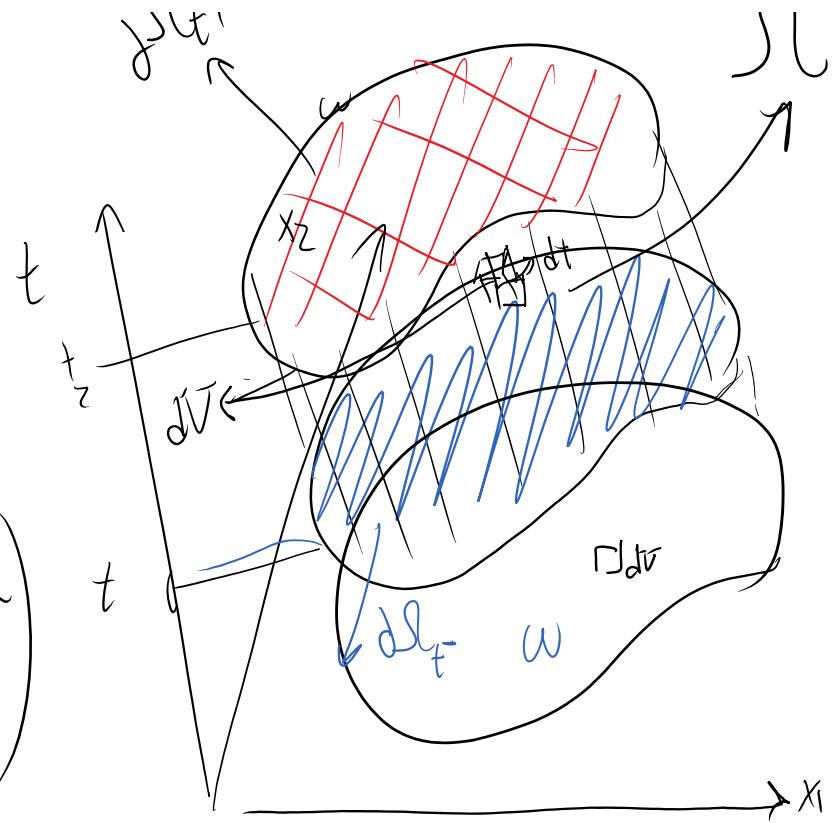
Source term



Source term

$$\int_{t_1}^{t_2} \int_V r dV$$

$$= \int_S r dV \quad (\text{inside } S)$$



$$\int (f_x \cdot \vec{n}) dS =$$

$$\int f_x \frac{\vec{n}_x}{\vec{n}_t} dS = N_{\text{ond}} dS$$

$$\vec{f}_x \cdot \vec{n} + \vec{f}_t \cdot \vec{0} = \vec{f}_x \cdot \vec{n}$$

$$F_z \left[ \frac{f_n}{f_t} \right]$$

space time flux

