

From last time

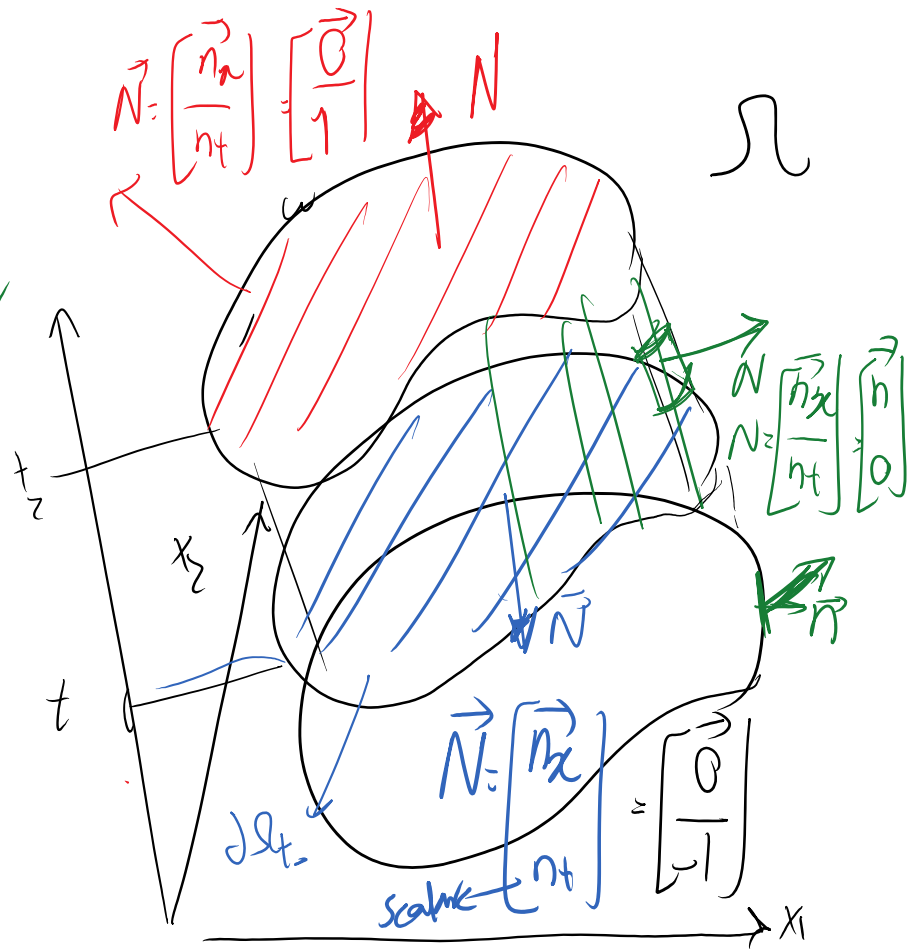
$$\int_{\partial S_V} (\rho \vec{f}_x \cdot \vec{n}) dS = \vec{N} \cdot \text{on } dS_V$$

$$\int_{\partial S_V} \begin{pmatrix} \rho \\ f_x \\ f_t \end{pmatrix} \cdot \begin{pmatrix} \vec{n} \\ 0 \end{pmatrix} dS =$$

$$\rho_x \cdot \vec{n} + \rho_t \cdot 0 = \rho_x \cdot \vec{n}$$

$$F = \begin{pmatrix} f_x \\ f_t \end{pmatrix}$$

space time flux



From last time the integral over vertical boundary is:

$$\int_{\partial S_V} \rho_x \cdot \vec{n} dS = \int_{\partial S_V} F \cdot N dS$$



$$-\int_{\partial\Omega^-} f_t dS = \int_{\Omega} F \cdot N dS \quad \text{iii}$$

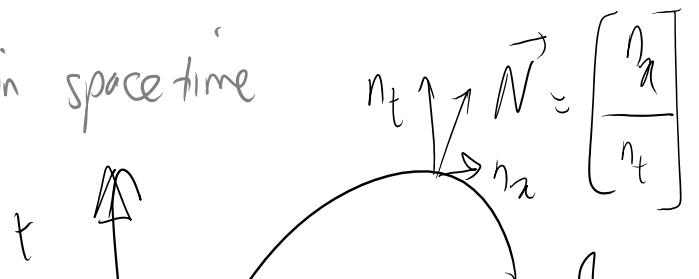
$$\int_{\partial\Omega} f_t \cdot n dS + \int_{\partial\Omega^+} f_t dS - \int_{\partial\Omega^-} f_t dS = \int_{\Omega} r dV$$

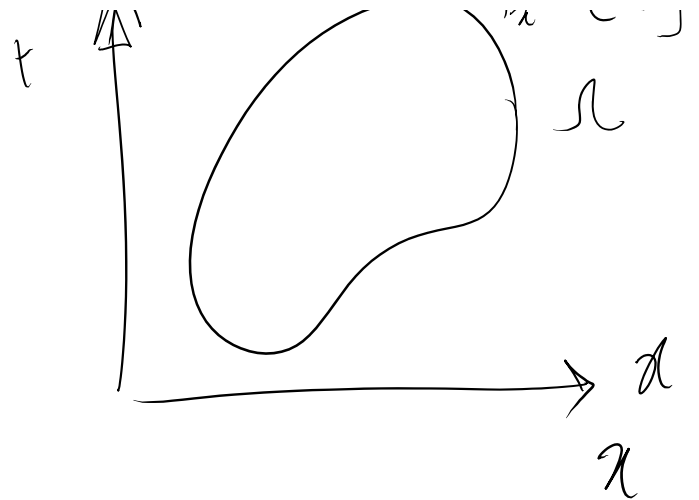
i ↓

$$\int_{\partial\Omega} F \cdot N dS + \int_{\partial\Omega^+} F \cdot N dS + \int_{\partial\Omega^-} F \cdot N dS = \int_{\Omega} r dV$$

$$\textcircled{1} \quad \int_{\partial\Omega} F \cdot N dS = \int_{\Omega} r dV$$

Expression of balance law in spacetime



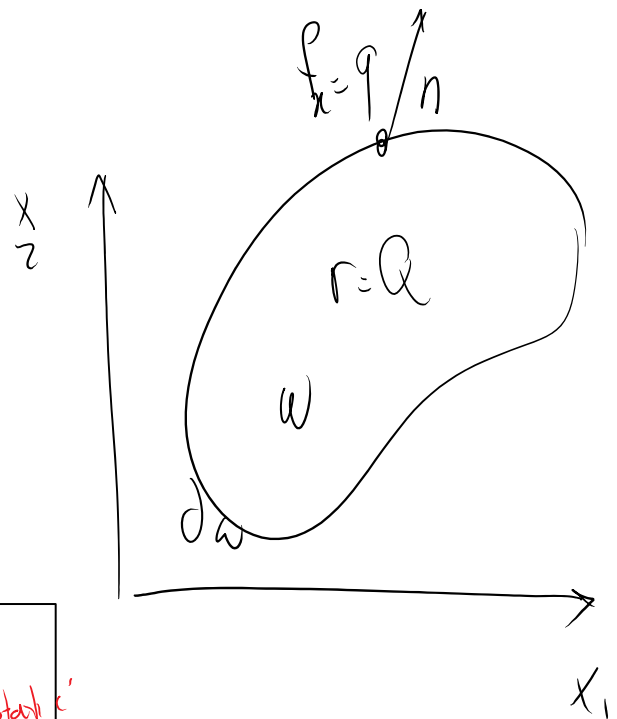


While we can "justify" the form of balance law in space time (eqn (1)) for an arbitrary shaped Ω , the actual form of balance law in spacetime is eqn (1).

What I did has many problems! There is no metric in space time; we cannot define normal vectors, etc. and to do all these rigorously we need to use differential forms notation (not discussed here)

Comparison with steady state or static balance laws

$$-\int_{\partial\omega} f_{\alpha} \cdot \vec{n} \, ds + \int_{\omega} r \, dV = 0$$



2.6

$$\int_{\partial\omega} f_{\alpha} \cdot n_{\alpha} \, ds = \int_{\omega} r \, dV$$

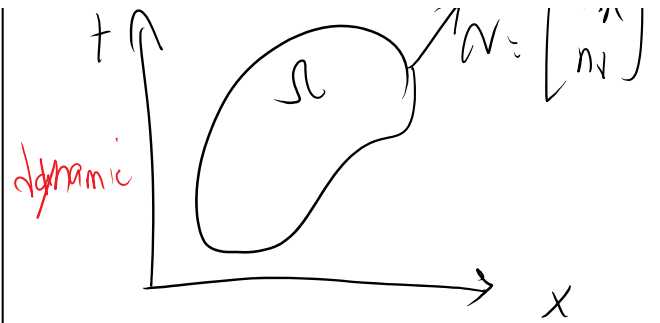
Static

Space time balance law

t ↑

$\vec{n} = \begin{bmatrix} n \\ n_t \end{bmatrix}$

$$2b \quad \int_{\Omega} \mathbf{F} \cdot \mathbf{N} dS = \int_{\Omega} \sigma dV$$



$$\mathbf{F} = \begin{pmatrix} F_n \\ F_t \end{pmatrix}$$

For any balance law the contribution of fluxes on the boundary balances the source term contribution from inside.

Compare this with more complex form of dynamic balance laws are used to:

we often write 2b as

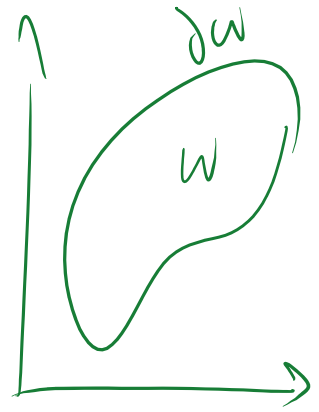
$$\frac{d}{dt} \int_{\omega} f_t dv = - \int_{\partial\omega} f_n \cdot n ds + \int_{\omega} r dv$$

not only Ω implied by this ($\omega \times [t_1, t_2]$) is more restrictive than general Ω in spacetime, the form looks different from a static balance law.

Summary:

Any balance law can be written as:

$$\textcircled{3} \int_{\partial W} f \cdot n \, ds = \int_W r \, dv$$



in spacetime f includes (spatial flux density + balance quantity density) & in space f is only the spatial flux.

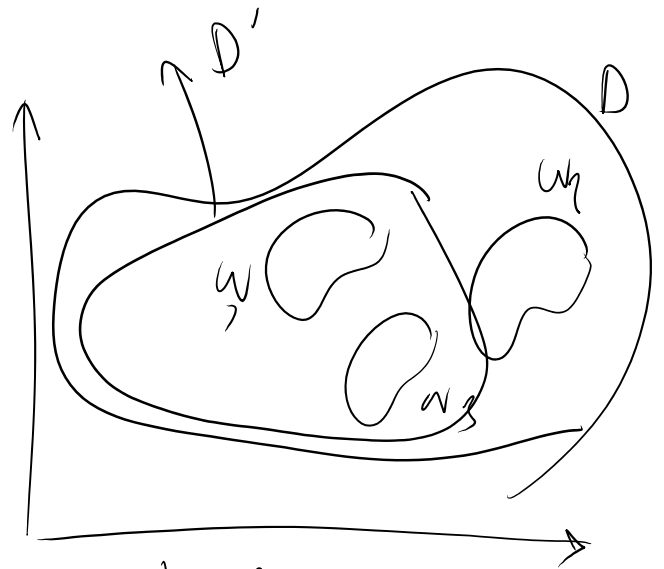
Strong form and jump conditions derived from a balance law:

$\forall W$

$$\int_{\partial W} f \cdot n \, ds = \int_W r \, dv$$

in D' $f \in C^1$

& ∂W is continuous



$$\int (\nabla \cdot f - r) \, dv = 0$$

$\omega \subset D'$ is arbitrary

$$\int_{\omega} (\nabla \cdot f - r) dv = 0$$

$\omega \subseteq D'$ is arbitrary

Localization theorem \rightarrow

strong form
(PDE)

(4a)

$\nabla \cdot f - r = 0$

$\forall x \in D \setminus \Gamma$

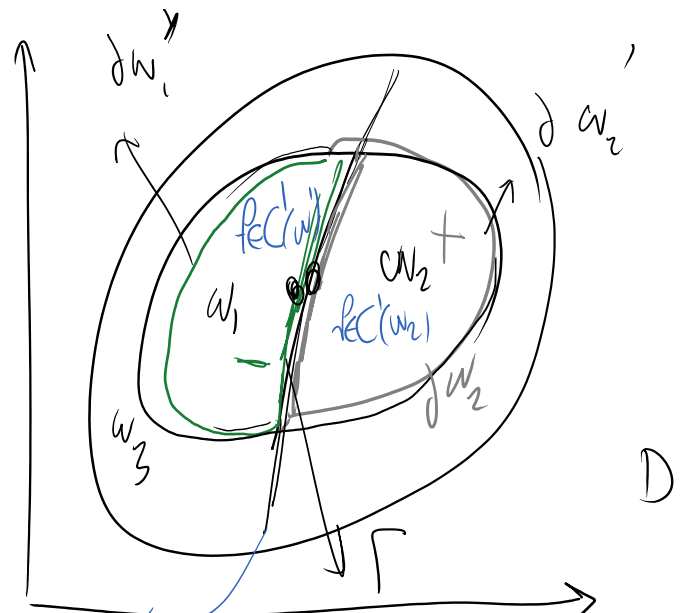
↓
Jump manifolds

where ever
 $f \in C^1$

Jump conditions

$$\int_{\partial \omega_1} f \cdot n ds = \int_{\omega_1} r ds \quad (\omega_1)$$

$$\int_{\partial \omega_2} f \cdot n ds = \int_{\omega_2} r ds \quad (\omega_2)$$



add them

a manifold on which f may not be C^1

$$\int_{\partial \omega_1'} f \cdot n ds + \int_{\Gamma} f \cdot n ds + \int_{\partial \omega_2'} f \cdot n ds = \int_{\omega_1} r dv + \int_{\omega_2} r dv$$

$$\int_{\partial \omega_2} f \cdot n \, ds + \int_{\Gamma} f \cdot n^+ \, ds = \int_{\omega_1} r \, dV + \int_{\omega_2} r \, dV$$

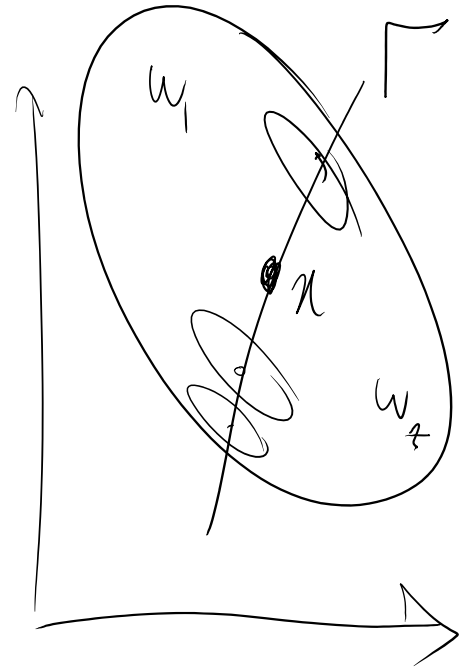
$$\int_{\partial \omega_3} f \cdot n \, ds + \int_{\Gamma} (f \cdot n^- + f \cdot n^+) \, ds = \int_{\omega_3} r \, dV$$

$$\int_{\partial \omega_3} f \cdot n \, ds - \int_{\omega_3} r \, dV = 0 \quad \text{balance law for } \omega_3$$

$$\textcircled{4} \quad \int_{\Gamma} (f \cdot n^- + f \cdot n^+) \, ds = 0$$

$$\Rightarrow f \cdot n^- + f \cdot n^+ = 0$$

$\forall x \in \Gamma$ by localization



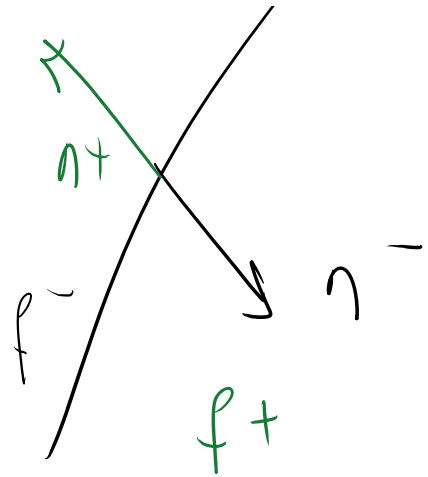
$$f \cdot n^- + f \cdot n^+ = \llbracket f \rrbracket$$



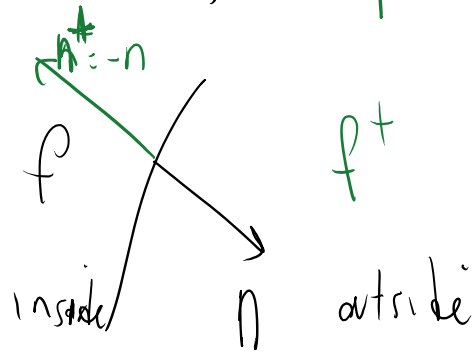
$$f \cdot n + f^T \cdot n = 0$$

symmetric view point

Jump def. by Arnold 2000
2001
papers



Another view point



$$f^- \cdot n + f^+ \cdot n^+ =$$

$$\downarrow$$

$$f^- \cdot n + f^+ \cdot (-n) =$$

$$-(f^+ - f^-) \cdot n = 0$$

$$[f] = f^{\text{outside}} - f^{\text{inside}}$$

$$f^- \cdot n + f^+ \cdot n^+ = 0 \rightarrow [f] \cdot n = 0$$

Summary

$$\int_{\partial \omega} f \cdot ds = \int_{\omega} r \, dv \implies$$

1. PDE / Strong form

$$\nabla \cdot f - r = 0$$

$D \setminus J$

↓
Jump set

2. Jump condition

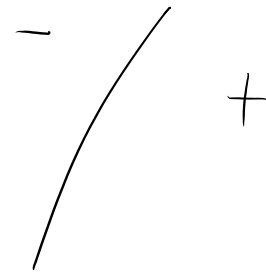
$$f^- \cdot n^- + f^+ \cdot n^+ = 0$$

or $[[P]] = 0$

Arnold's notation

$[[f]] \cdot n = 0$

$$[[f]] = f^{\text{out}} - f^{\text{in}}$$



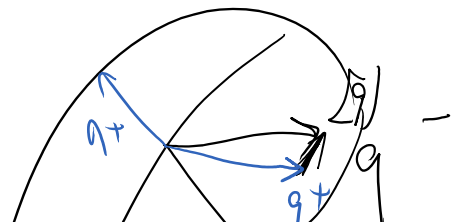
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We must start from the balance law. Many times the PDEs are written in a non-conservative way. For example Navier-Stokes equations may be written by dividing certain equations by ρ . In that case, we cannot even "guess" what the jump conditions corresponding to the original balance laws would have looked like.

Examples:

Heat conduction

static version



static version

$$(q^+ - q^-) \cdot n = 0$$

$$[q] \cdot n = 0 \quad [q] \perp n$$

$$q^+ \cdot n^+ = -q^- \cdot n^- \quad \text{balance of net fluxes}$$

PDE $r = Q \quad f = q \quad \nabla \cdot q - Q = 0$

Solid Mechanics

$$f = -b \quad r = pb$$

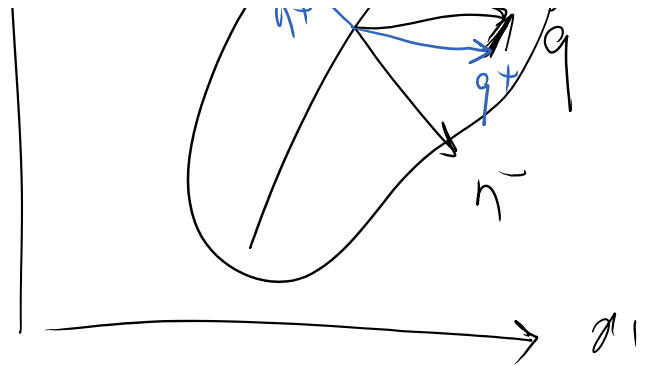
PDE $\nabla \cdot (-b) - pb = 0 \quad \nabla \cdot b + pb = 0$

$$(\sigma^+ - \sigma^-) \cdot n = 0$$

$$\sigma^+ \cdot n - \sigma^- \cdot n = 0$$

$$\boxed{\sigma^+ \cdot n = \sigma^- \cdot n}$$

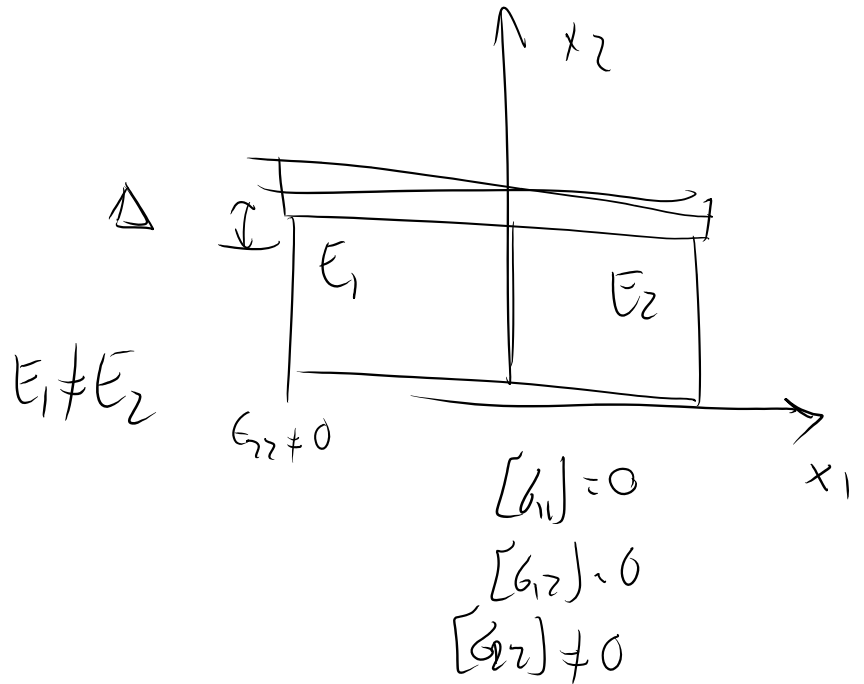
action-reaction law



$$\delta^T \cdot \vec{n}^+ = -\delta \cdot \vec{n}^-$$

Tractions are equal, but do we need to have

$$[\delta] = 0$$



How about a dynamic balance law:

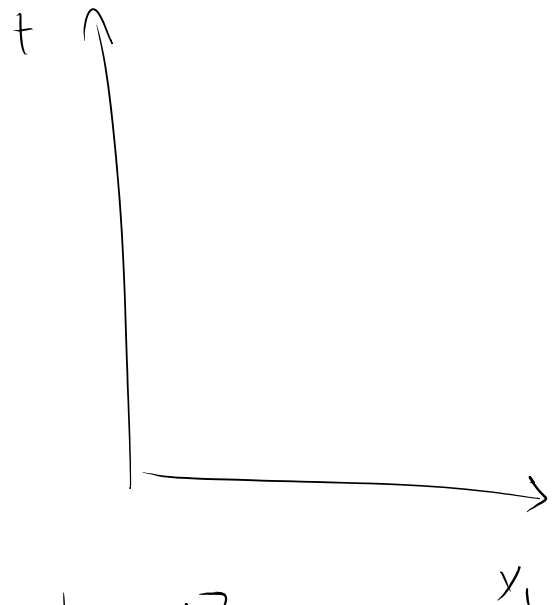
$$F = \begin{bmatrix} f_x \\ f_t \end{bmatrix}$$

balance
of linear
momentum

$$f_x = -\sigma$$

$$f_t = \frac{\text{Linear momentum}}{\text{volume}}$$

$$P = \text{Linear momentum} = \dot{M} \vec{v}$$



volume

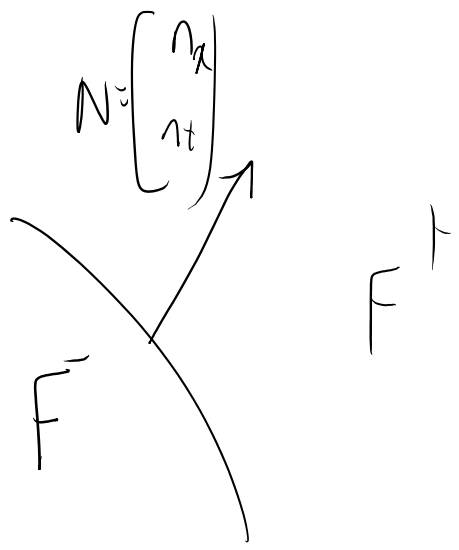
mass ↓ velocity ↓

$$= \frac{\text{mass} \cdot \vec{v}}{\text{Volume}} = \rho \vec{v}$$

$$f_t = p := \rho \vec{v}$$

$$F = \begin{bmatrix} -\delta \\ \rho \vec{v} \end{bmatrix}$$

⑥ for balance of linear momentum



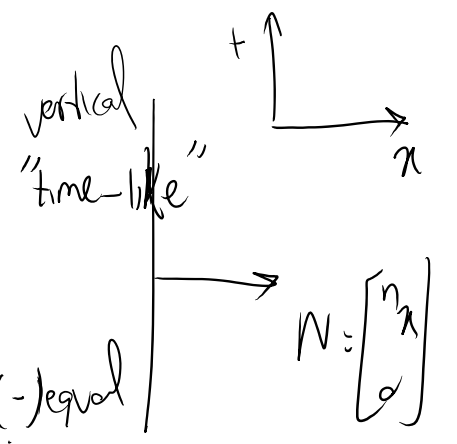
$$[F] \cdot N = 0$$

$$\begin{bmatrix} -\delta \\ \rho v \end{bmatrix} \cdot \begin{bmatrix} n_x \\ n_t \end{bmatrix} = 0 \rightarrow -[\delta]n_x + [\rho]n_t = 0$$

$$-[\delta]n_x + [\rho]n_t = 0$$

a) $n_t = 0 \quad -[\delta]n_x = 0$

action-reaction
traction are (-) equal
static equilibrium

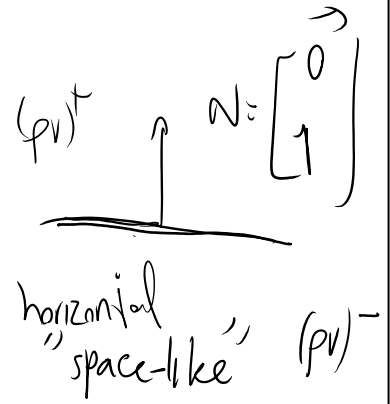


"static equation"

b) $n_x = 0$

$$[P] \cdot t = [P]_z = 0$$

$$(p_v)^- - (p_v)^+ = 0$$

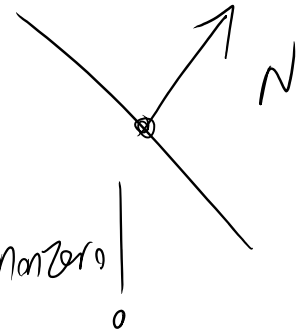


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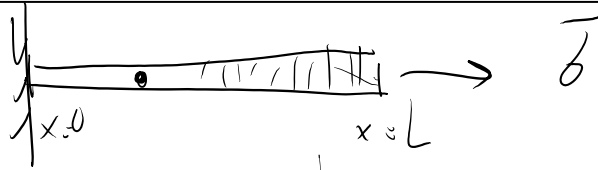
c)

$$-[G] \cdot n_x + [P] n_t = 0$$

$[G] \cdot n_x$ & $[P] n_t$ both can be nonzero!



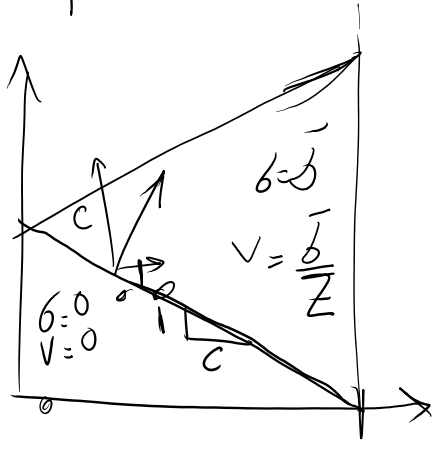
Example of N being slant



$$c = \sqrt{\frac{E}{\rho}}$$

$$\eta_x = \frac{1}{\sqrt{1+c^2}}$$

$$\eta_t = \frac{c}{\sqrt{1+c^2}}$$



$$Z = c\rho = \sqrt{E\rho}$$

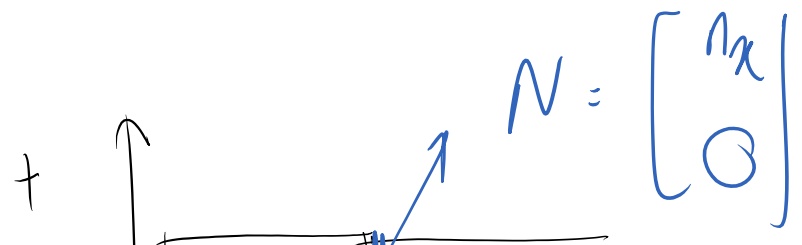
$$p = \rho v$$

$$[\delta] \cdot n$$

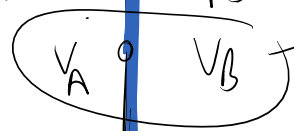
$$[\delta] \cdot n_x \neq 0 \quad ?$$

$$[-\delta] \cdot n_x + [p] \cdot n_t = 0 \quad ? \quad \text{check it}$$

where (what direction) can these jumps happen?

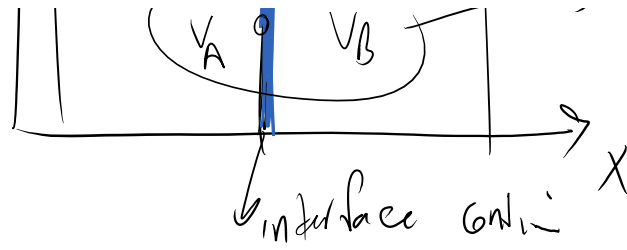


on vertical manifolds we can have nontrivial



simple core bounded interface

can have nontrivial jumps



bounded interface

$$[v] = 0$$

$$[p] \neq 0 \quad (p_A \neq p_B)$$

$$p = pV$$

$$[-b] \cdot n_x + [p] \cdot 0 = 0$$

$$-[b] \cdot n_x = 0$$

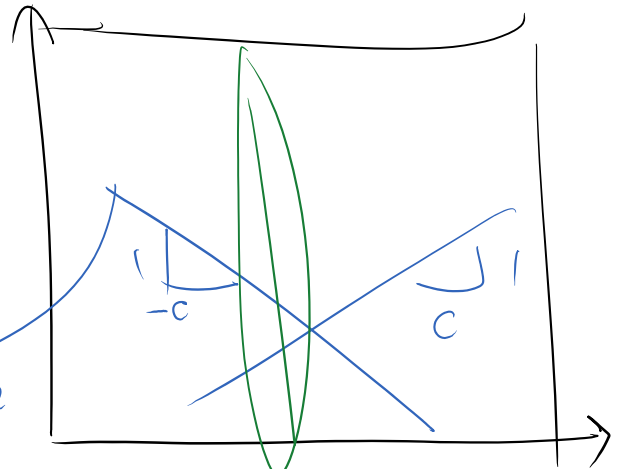
→ tractors are continuous

$[p] \neq 0$ is it possible

Other nontrivial jumps

$$c = \sqrt{\frac{E}{\rho}}$$

see dynamic example above



M_0 (no nontrivial jumps)