

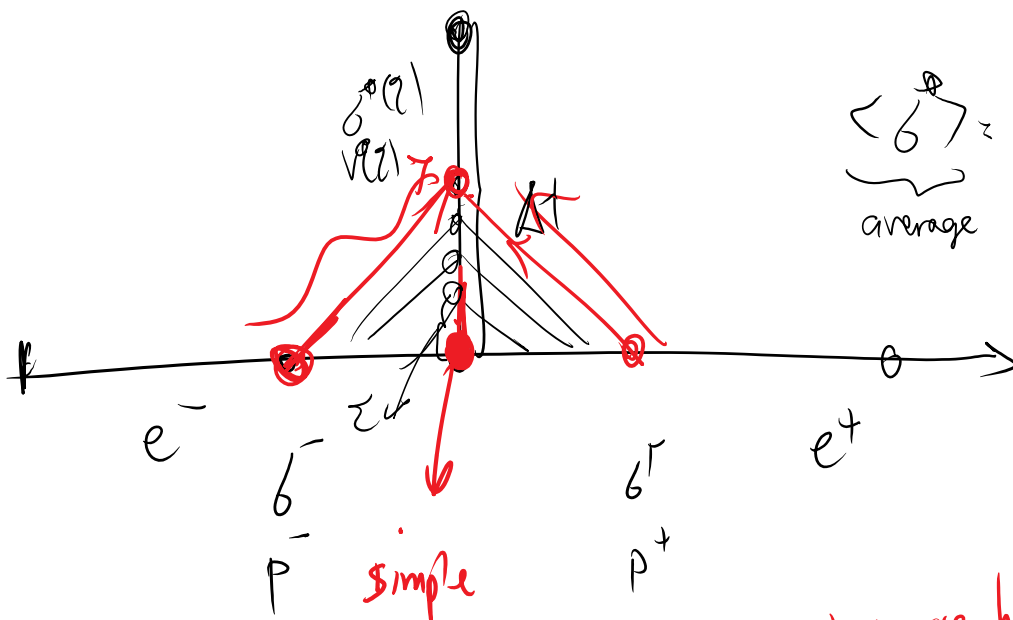
The difficulty in handling source terms when obtaining numerical fluxes (for example Riemann solution)

$$\dot{p} - b_x = \rho b$$

$$\dot{b} - \frac{E}{\rho} p_x = 0$$

$$S = \begin{pmatrix} \rho b \\ \alpha \end{pmatrix}$$

we assumed ρb to be zero



$$\langle b \rangle = \frac{1}{\Delta t} \int_0^{\Delta t} b(\tau) d\tau$$

average best

a age + jump term sins are had

next best option

$$\langle b^* \rangle \approx b^* \left(\tau = \frac{\Delta t}{2} \right)_+$$

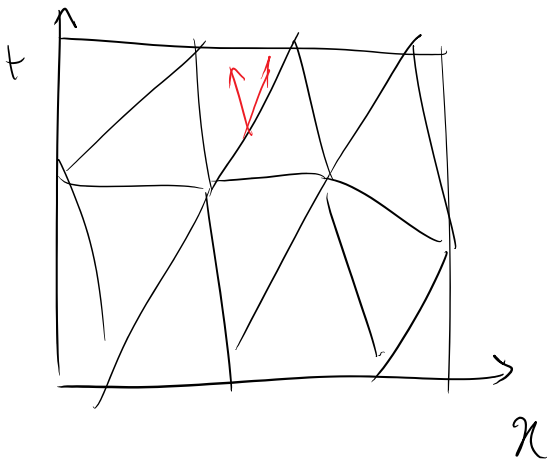
$$\langle \sigma^p \rangle \approx \sigma \left(\xi = \frac{\Delta t}{2} \right) + \mathcal{O}(\Delta t^2)$$

In either case, the Riemann solution at $\xi \neq 0$

requires the integration of source terms along characteristics.

What happens to Riemann solutions for spacetime DG methods and in particular aSDG method.

① Spacetime DG methods:
FEM



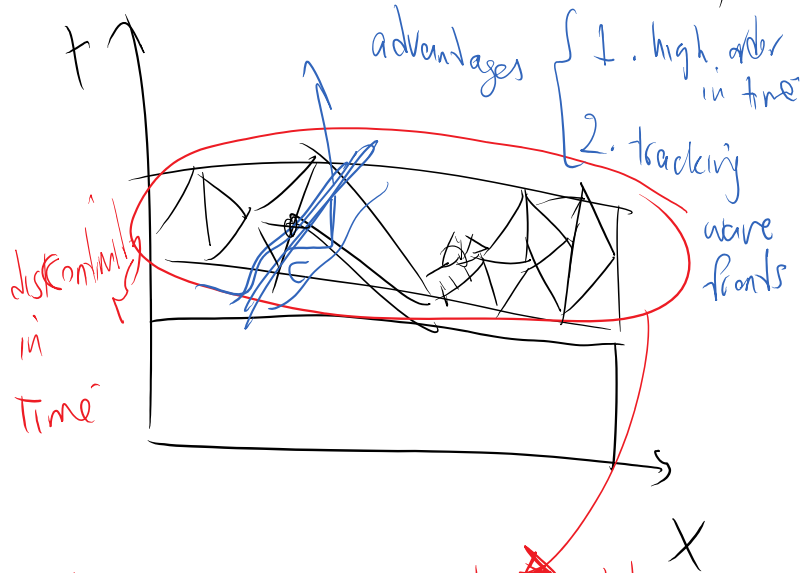
we solve a globally coupled problem in
space dim $\rightarrow \mathbb{E}^d \times \mathbb{R}^+$ time

- The form of shape functions in spacetime for CFEM makes the whole domain globally coupled even if all

Next was

② TDG

Time discontinuous Galerkin method
(Tom Hughes & Hubert)



discontinuity between time slabs
enables solution of 1 time

makes the whole domain globally coupled even if all faces are causal.

-> DG formulation

Can employ causality of the mesh to solve one of a few elements at a time.

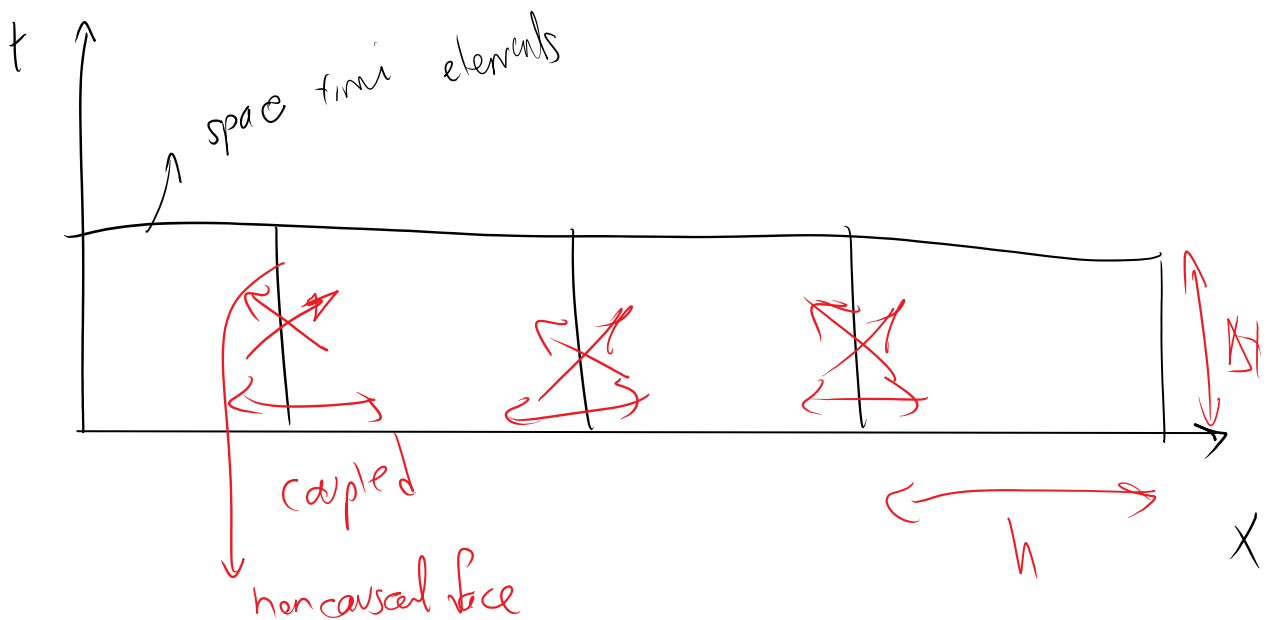
enables solution of 1 time slab rather than whole domain at a time

First SPACETIME methods used CFEM and solved a globally coupled problem.

- Clearly no star value for CFEMs.

③ Space time DG method Implicit

van der Vegt etc



the whole domain is coupled even if a hyperbolic problem

Δt_{max}

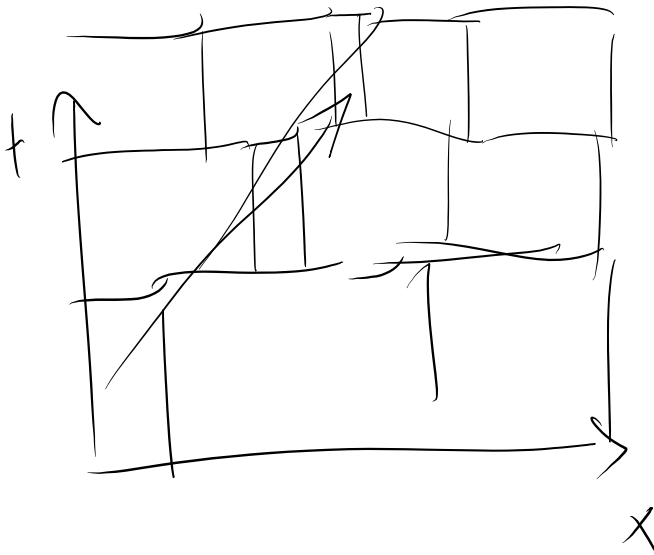
h

for hyperbolic PDE

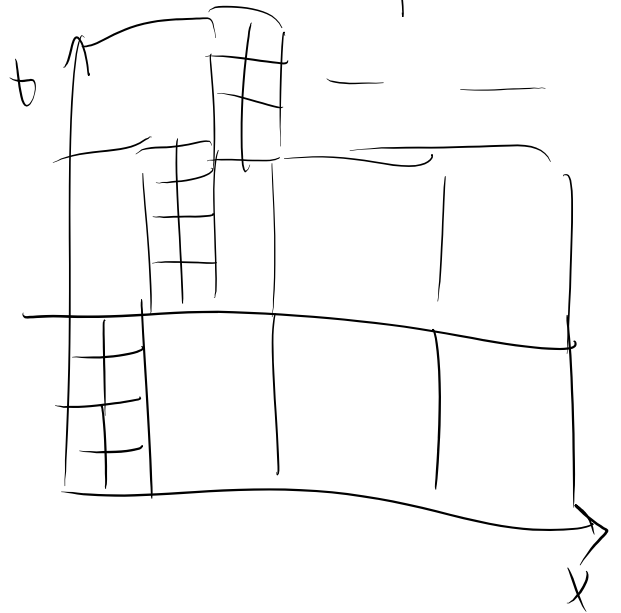
no time step limit

More refined versions of SDGs

h - Adaptivity in space

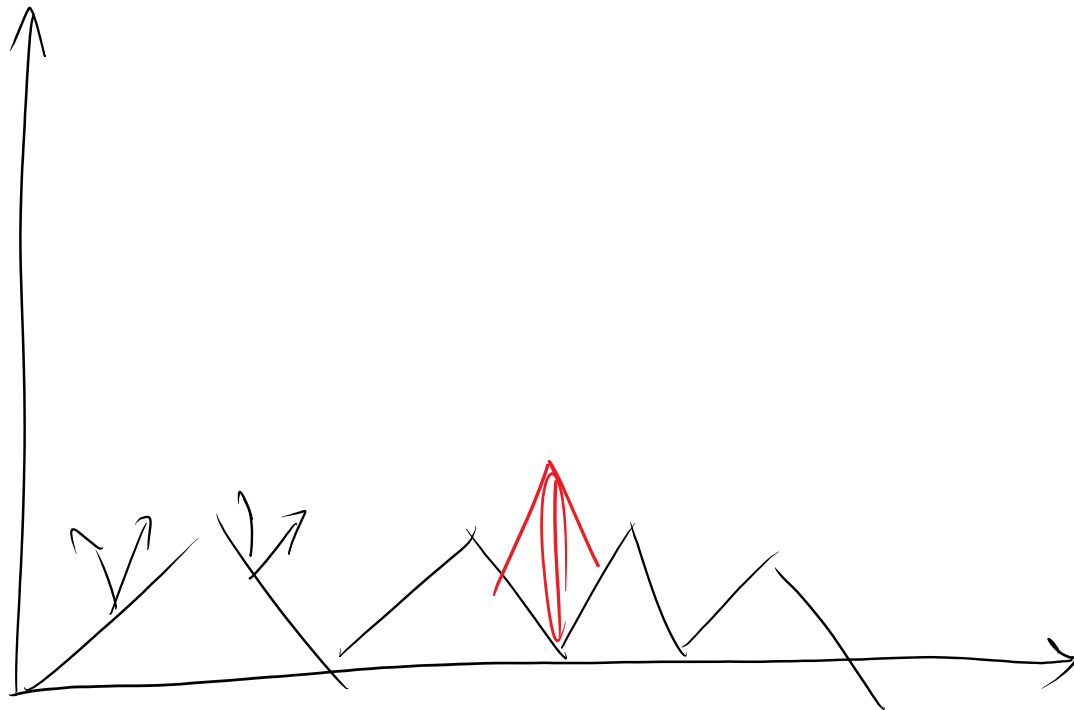


h - Adaptivity in spacetime



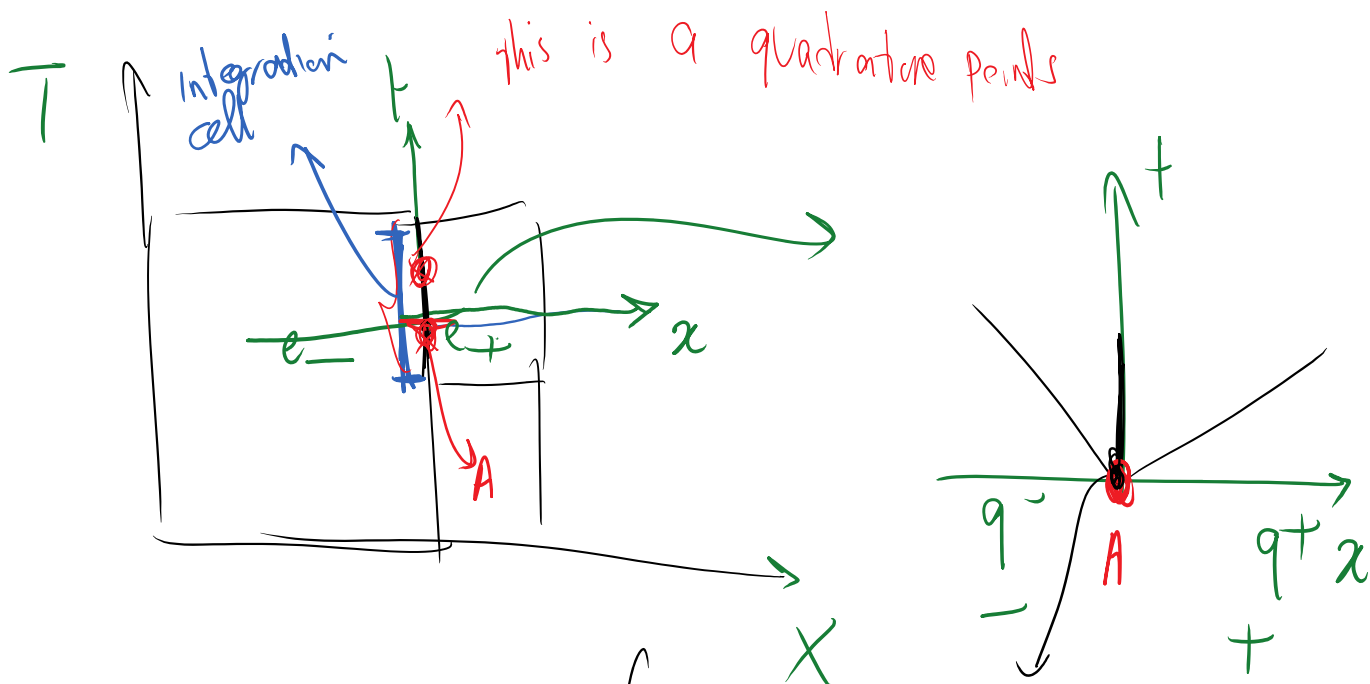
④ a SDG method

Richter 1990



Discussion on Riemann solutions for (3) and (4)

1. For both having source term does not complicate things!



For any spacetime DG methods source terms do not influence the Riemann Solution!

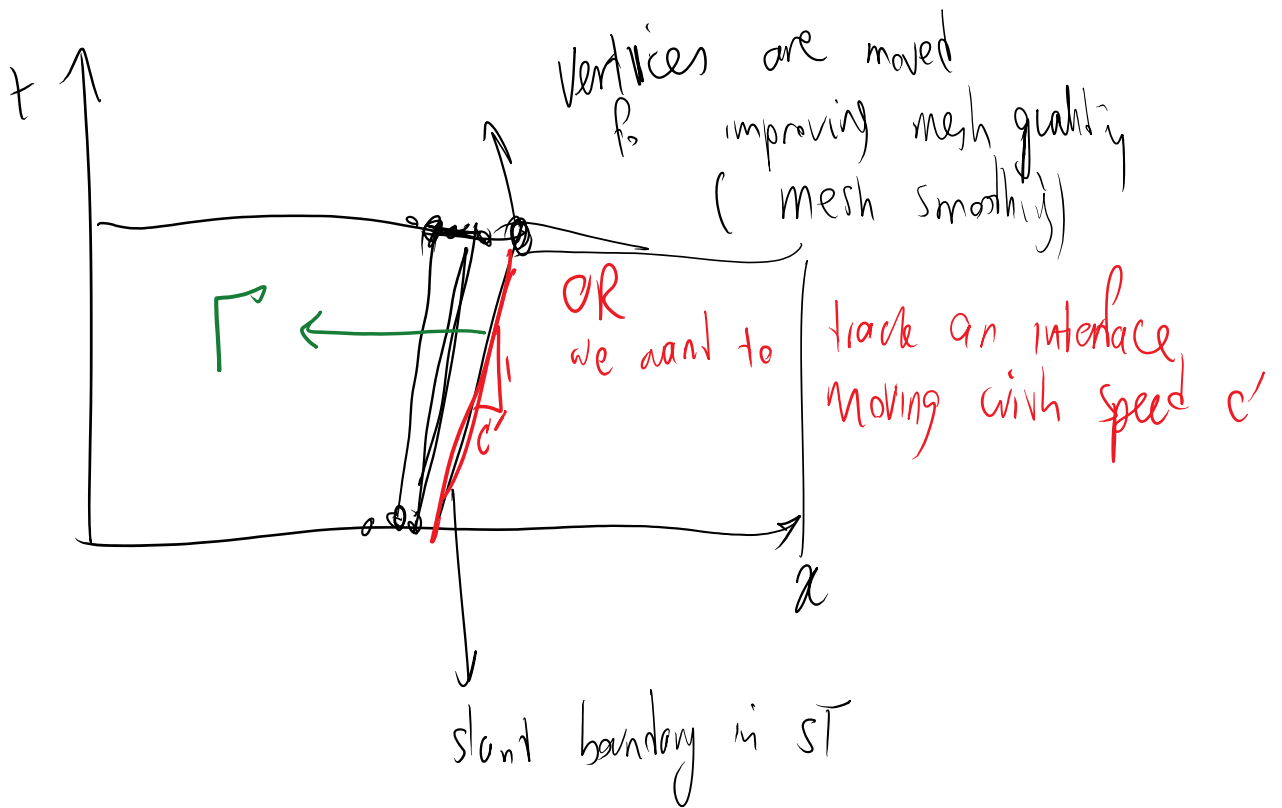
we get the Riemann solution on the Riemann front

terms do not influence the Riemann Solution!

... solution on the SAME point

(because unlike time-marching DG methods we have the solution between time steps)

2.3. Related to fully unstructured meshes (aSDG method)
OR SDG method with front tracking.



aSDG + face



2.3 \rightarrow challenges of non-vertical faces

Let's revisit weighted residual statement for spacetime methods.

$$F = \begin{bmatrix} f_x \\ f_t \end{bmatrix} \rightarrow \begin{array}{l} \text{spatial flux} \\ \text{temporal flux} \end{array}$$

$$\int_Q F \cdot N \, ds = 0 \equiv \int_{\partial Q} \vec{F} \cdot \vec{n} \, ds = 0$$

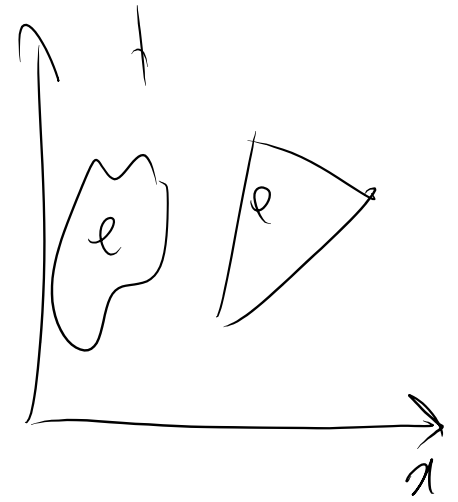
$$-\int_Q r \, ds$$

$$[F] \cdot N = 0 \quad \text{Jump part}$$

WRS of this

$$\int_e \omega (\nabla_{st} \cdot F - r) de +$$

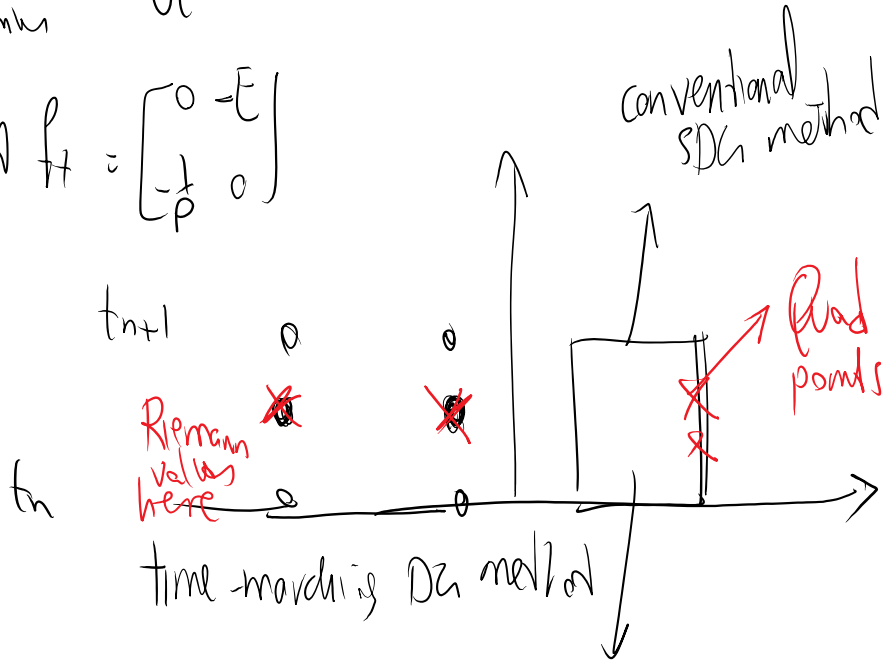
$$\int_{de} \omega [F] \cdot N ds = 0$$



$$\int_e \omega (\nabla_{st} \cdot F - r) de + \int_{de} \left[\omega (F_x^* - F_x) \cdot n_x + \omega (F_t^* - F_t) \cdot n_t \right] ds = 0$$

Example: 1D Elastodynamics

$$F_t = \begin{bmatrix} P \\ E \end{bmatrix} \quad F_x = \begin{bmatrix} -b \\ -v \end{bmatrix} = A F_t = \begin{bmatrix} 0 & -E \\ -1 & 0 \end{bmatrix}$$



$$\int_{\omega} (\rho^* - \rho) \vec{n}_x ds$$

eg solid mechanics $\vec{n}_H = 0$

$$\int_{\omega} (\rho^* - \rho) \vec{n}_H ds$$

$$\vec{n}_x = 0$$

$$\vec{f}_H = \begin{bmatrix} P \\ \epsilon \end{bmatrix}$$
 on horizontal faces

$$P^*, \epsilon^*$$

$$\int_{\omega} (\rho^* - \rho) \vec{n}_x ds$$

$$\vec{f}_x = \begin{bmatrix} -b \\ -v \end{bmatrix}$$
 ✓

$$b^*, v^*$$

2. For non-vertical faces -> we need to compute ALL star values. Typically Riemann solutions are only provided for f_x values because faces are often vertical.

$$\vec{n} \neq 0$$

$$\vec{n}_H \neq 0$$

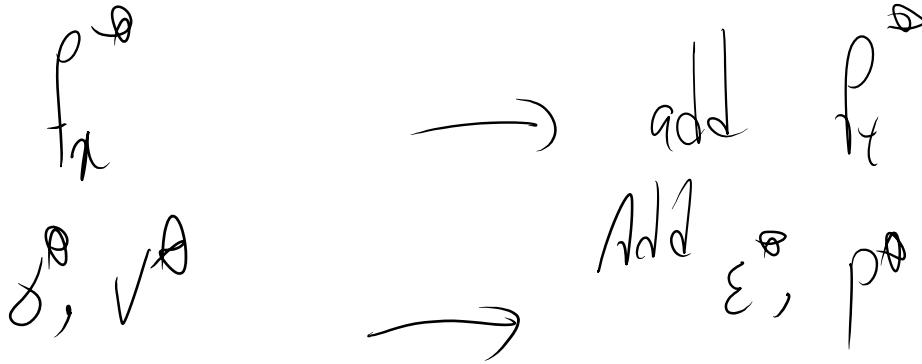
$$P^*$$
 needed

$$\vec{f}_x = \begin{bmatrix} P \\ \epsilon \end{bmatrix}$$

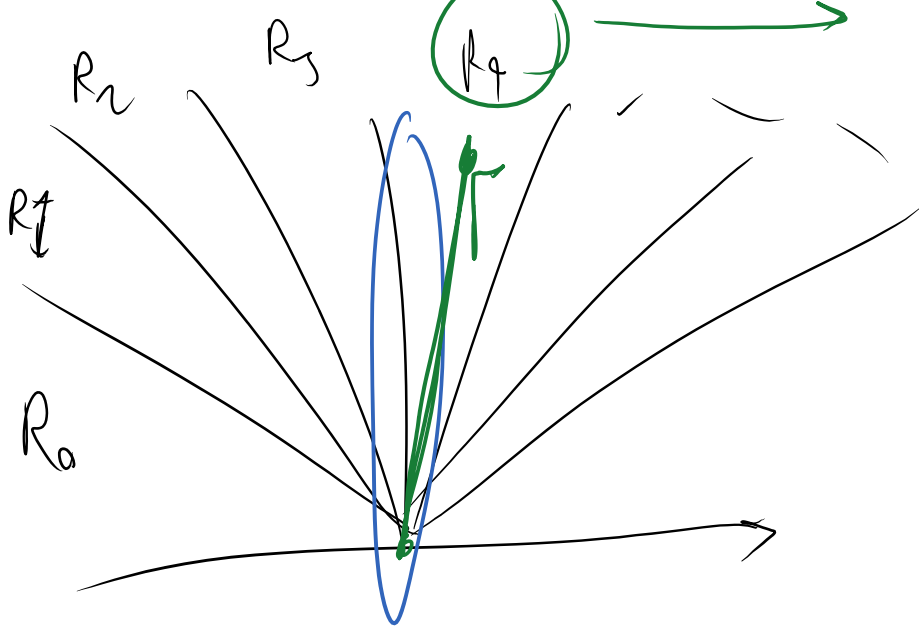
$$\vec{f}_x = \begin{bmatrix} P \\ \epsilon \end{bmatrix}$$

$$\omega \left(\frac{p_x}{\rho} \right) / \rho + \frac{v_x}{\rho} \frac{d}{dx} \left(\frac{p_x}{\rho} \right)$$

Solid Mechanics



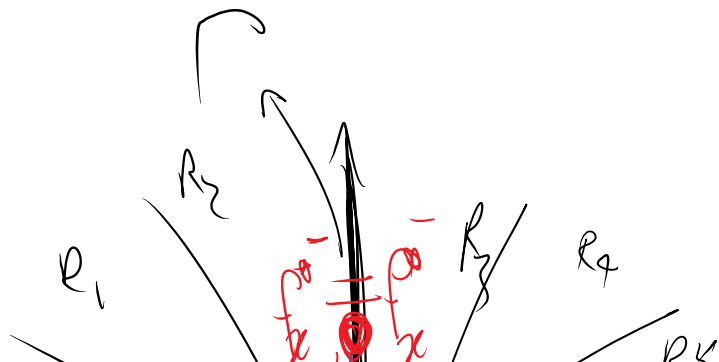
3. Values are needed on NON-Vertical faces (if the face is non-vertical)

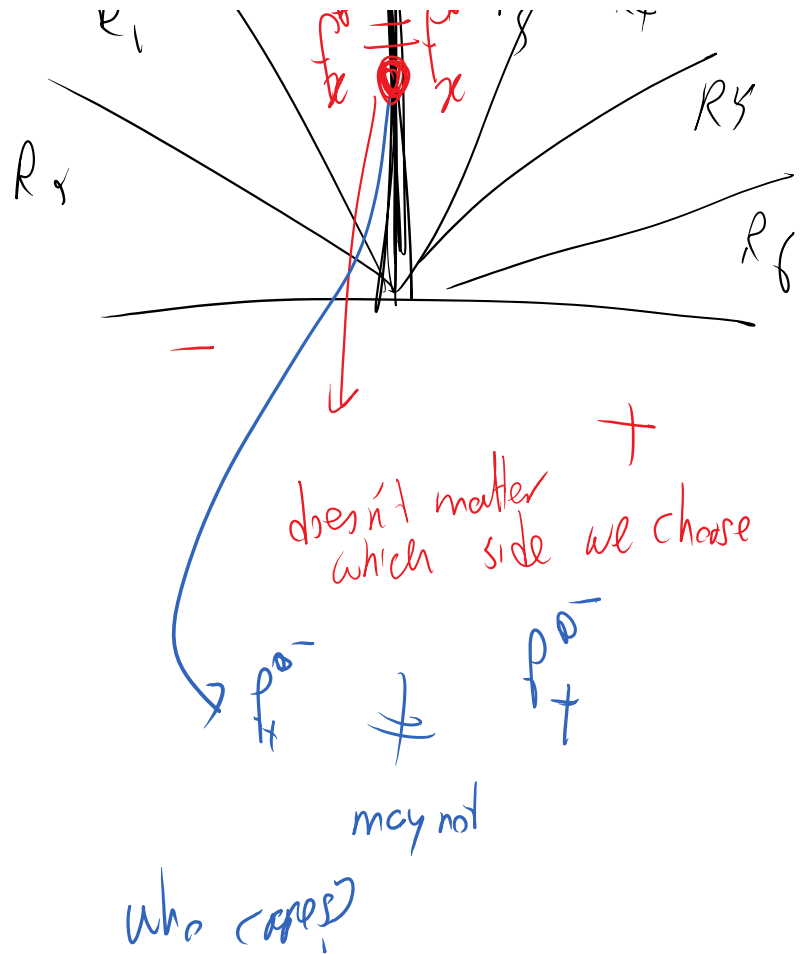


we need to choose the solution for this region

Conventional DG only needs the solution here

Trick question





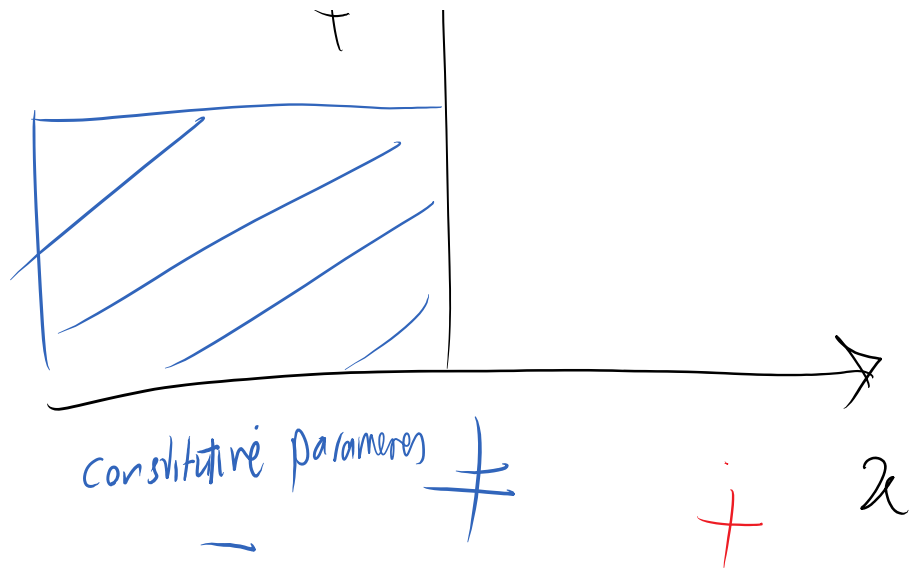
Summary:

Spacetime DG methods:

1. No need to worry about source terms when computing target (Riemann fluxes) [there are also some advantages in the stability of these methods when solving problems with high source terms].
 2. Both f_x^* and f_t^* are needed in general.
 3. Solutions are needed for all regions of Riemann solution.
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Material Interfaces and Riemann solutions:



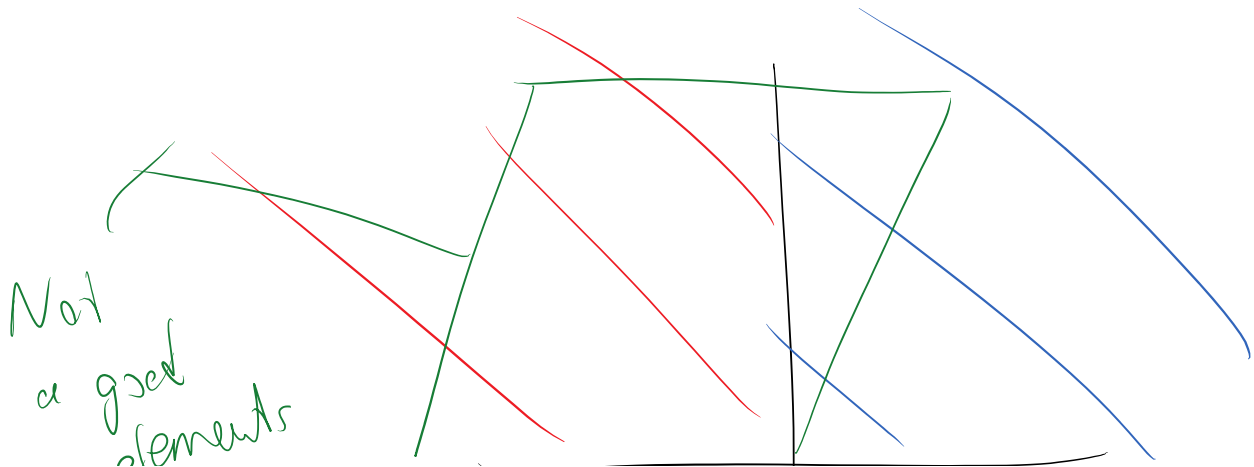


OR even different physics

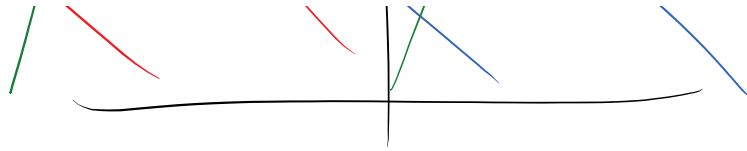
Solid
Elastodynamics

Fluid
e.g. Acoustics
or more advanced

The good news is that we only need to solve the star values on the vertical direction because element boundaries cannot fall inside either of these two regions.



a given elements



In general the element boundary must track discontinuity (when can be nonvertical).

Example:

Solution mechanics, two different materials

Approach 1: characteristic values

$$\begin{aligned} \int \dot{p} - \sigma_{,x} &= p b \\ \dot{\sigma} - \frac{E}{\rho} p_{,x} &= 0 \\ \dot{\Sigma} &= \frac{1}{\rho} p_{,x} = 0 \\ \dot{E} - v_{,x} &= 0 \end{aligned}$$

$$q = \begin{bmatrix} p \\ \sigma \end{bmatrix}$$

$$q_{,t} + A q_{,x} = 0$$

$$A = \begin{bmatrix} 0 & -1 \\ -\frac{E}{\rho} & 0 \end{bmatrix}$$

In general we must be careful about interface matching conditions no matter how we express the system of conservation laws.

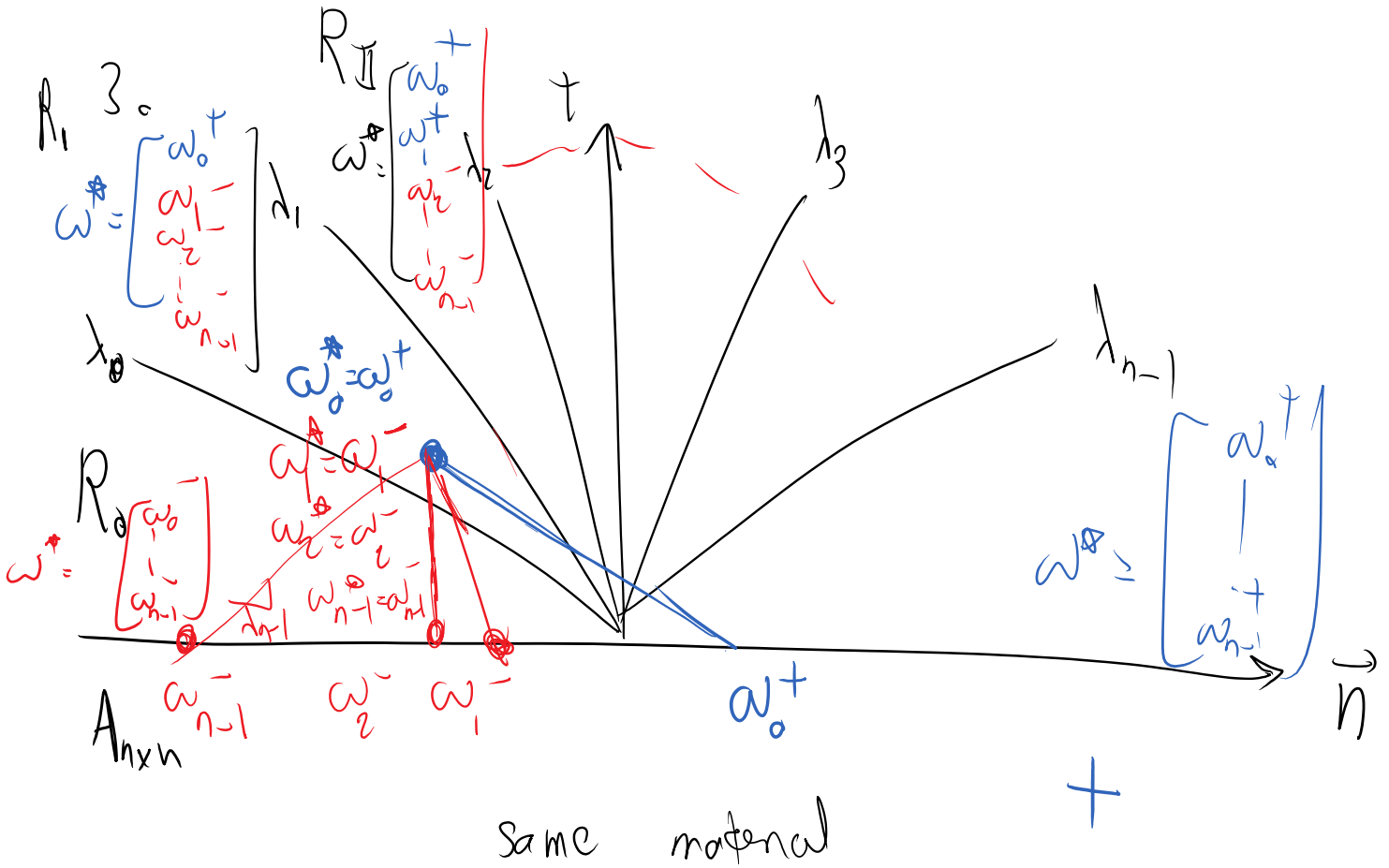
The solution scheme from the last times:

$$L_0 W = U q \rightarrow \text{matrix left eigenvectors}$$

$$\lambda_0 \dot{W}_n - \lambda_n W_{n,x} = 0$$

$$\begin{pmatrix} \frac{E}{c^2} \\ 0 \\ c^2 \end{pmatrix}$$

2. $\omega_n - \lambda_n \omega_{n,x} = 0$ eigenvalue λ_n



3. For all regions we have ω^*

we want $f_k^* = q^* = U^T \omega^* \quad \omega = U q$

$f_k^* = A q^* = A U^T \omega^* = U D U^T \omega^*$

$$= \int^4 D\omega^3$$