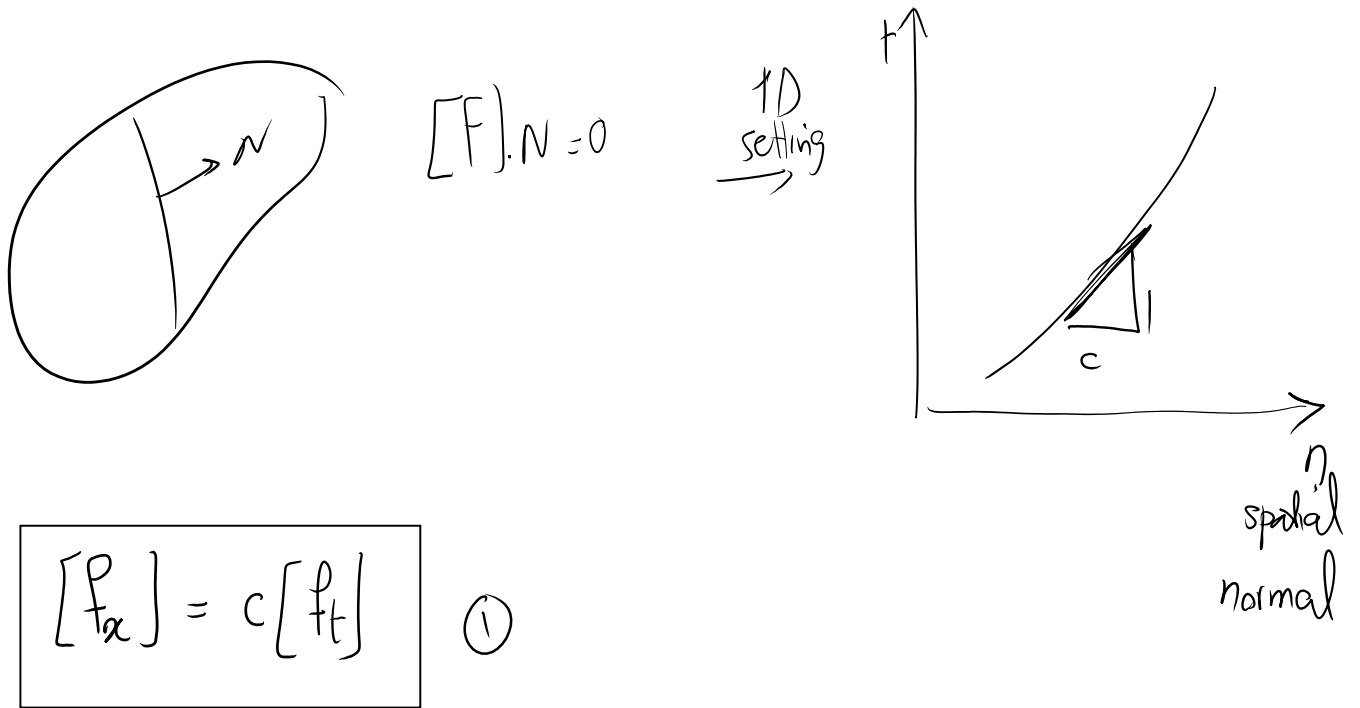


The other approach for solving Riemann solutions (using jump conditions):

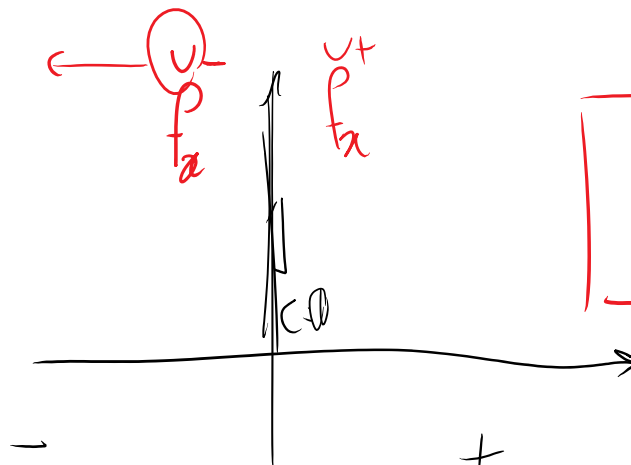


So basically jumps on $[f_x]$ & $[f_t]$ are not arbitrary

special cases:

(1) $c=0$ Vertical interface such as a material interface

value on the vertical interface



$$[f_x] = 0$$

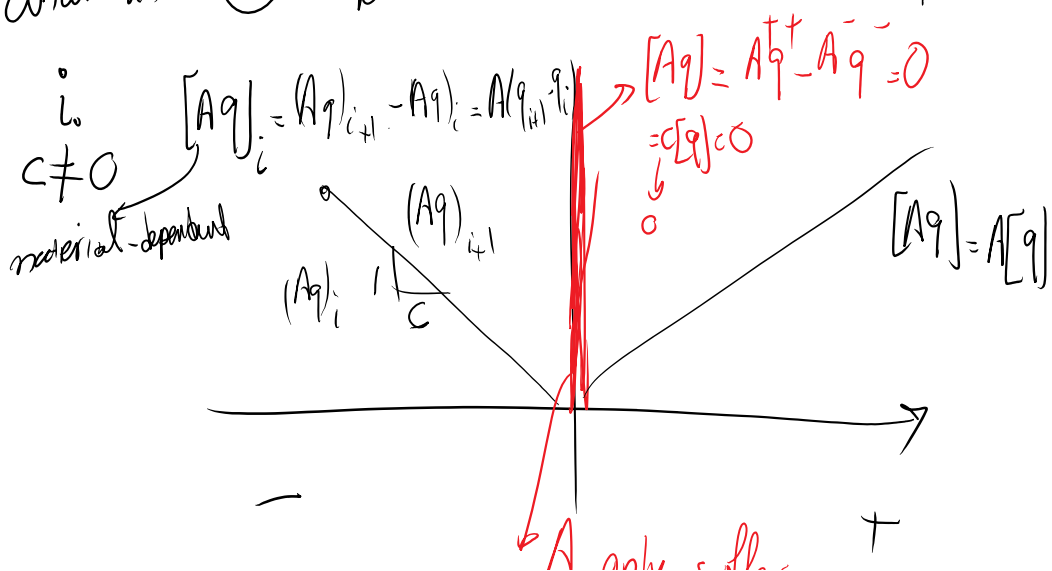
(2) $c \neq 0$ not interesting, because the interface is causal anyway

$$[f_t] = 0 \quad \left\{ \begin{array}{l} p_t^+ = p_t^- \\ \hline \text{in continuum} \\ \text{settings} \end{array} \right.$$

So what happens to (1) for a linear problem

$$\left. \begin{array}{l} p_t = q \\ p_x = Aq \\ [p_x] = c [p_t] \end{array} \right\} \rightarrow \boxed{[Aq] = c [q]} \quad (2)$$

what about (2) for a material interface problem:



Same for $c \neq 0$ on the + side

↳ A only suffers jump here ^T

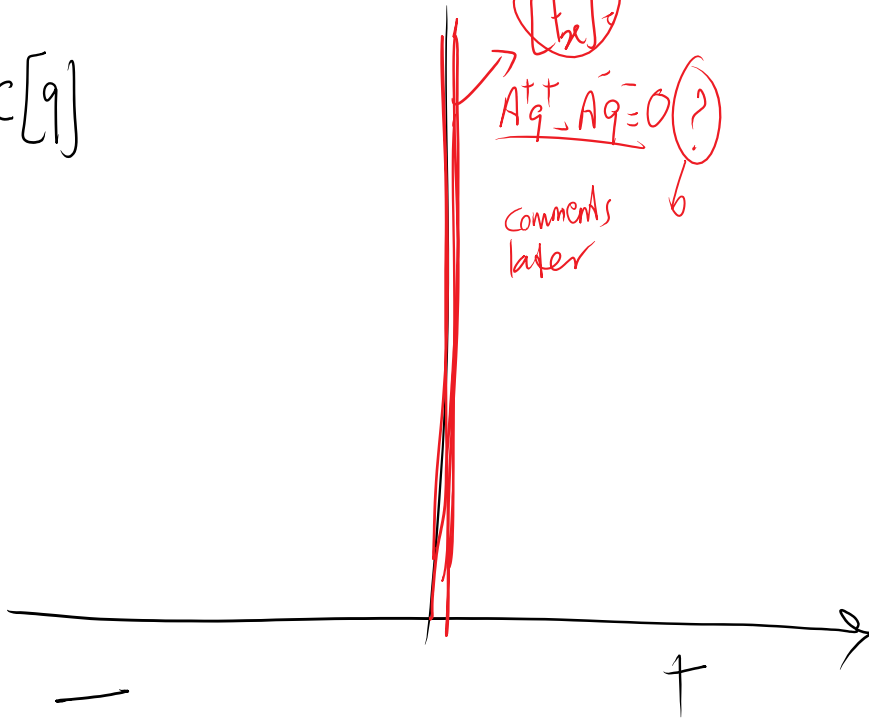
spatial flux is continuous

$$\bar{A}[q] = c[q]$$

$$c < 0$$

$$A^+ [q] = c[q]$$

$$c > 0$$



$$\bar{A}[q]_i = c[q]_i$$

↓
between region $(+1 \Delta x)_i$



c is an eigenvalue

$[q]_i$ is an eigenvector of A .

Solving elastodynamic problem with the new approach:

Balance of linear momentum

compatibility

$$\begin{cases} \dot{p} - \sigma_{,x} = \rho b \\ \dot{\epsilon} - v_{,x} = 0 \end{cases} \quad (2)$$

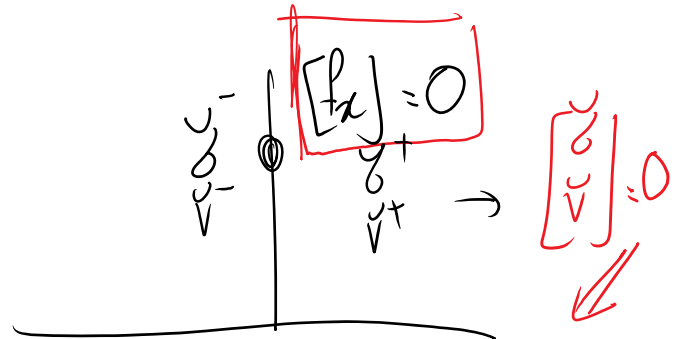
$$f_t = q = \begin{bmatrix} p \\ \epsilon \end{bmatrix}$$

$$f_x = \begin{bmatrix} -\sigma \\ -v \end{bmatrix}$$

correct spatial flux for this problem

$$A = \begin{bmatrix} 0 & -E \\ -\frac{1}{\rho} & 0 \end{bmatrix}$$

$$q_t + A q_x = 0$$



eigenvalues are $\pm c$

$$\begin{bmatrix} v \\ p \\ \dot{v} \\ \dot{p} \\ \epsilon \end{bmatrix} - \begin{bmatrix} p \\ \epsilon \end{bmatrix} = \alpha_1 V^1$$

1st eigenvalue of A^- corresponding to $-c^-$

$$R_0 \begin{bmatrix} p^- \\ \epsilon^- \end{bmatrix}$$

$$\begin{bmatrix} v^- \\ p^- \\ \dot{v}^- \\ \dot{p}^- \\ \epsilon^- \end{bmatrix} R_1^a$$

$$\begin{bmatrix} v^+ \\ p^+ \\ \dot{v}^+ \\ \dot{p}^+ \\ \epsilon^+ \end{bmatrix} R_1^b$$

v^-
 v^+ are unique values

$$\begin{bmatrix} p^+ \\ \epsilon^+ \end{bmatrix} = \alpha_2 V^2$$

2nd eigenvector of A^+ corresponding to c^+

$$\begin{bmatrix} \Gamma & 0 & 1 \\ \dots & \dots & \dots \end{bmatrix}$$

$\boxed{[P_x] = 0}$ always true (except some parts of compatibility
 - not the balance law parts - are relaxed)

$$P_x = A P_T \rightarrow A^- \begin{bmatrix} \dot{P}^- \\ \dot{\Sigma}^- \end{bmatrix} = A^+ \begin{bmatrix} \dot{P}^+ \\ \dot{\Sigma}^+ \end{bmatrix}$$

$$[P_x] = 0 \equiv \text{Jump} \begin{bmatrix} -\dot{J} \\ -\dot{V} \end{bmatrix} = 0$$

6 unknowns $\begin{pmatrix} \dot{P}^{\mp} \\ \dot{\Sigma}^{\mp} \end{pmatrix}$ & α_1, α_2 , 6 eqn 2x2 jumps
 & 2 for $[P_x] = 0$

and we solve it.

Tricky place **CORRECT**

$[P_x] = 0$ must be satisfied at the interface

If want to be adventurous and solve the problem with fewer unknowns we can choose the quantities that form spatial flux as unknowns

$$\begin{aligned} \dot{\rho} - \rho_{,x} &= \rho b \rightarrow x \frac{1}{\rho} & \dot{v} - \frac{1}{\rho} \rho_{,x} &= \cancel{v} \nearrow 0 \\ \dot{E} - v_{,x} &= 0 \rightarrow x E & \dot{\delta} - E v_{,x} &= 0 \end{aligned}$$

$$q = \begin{pmatrix} v \\ \delta \end{pmatrix} \quad q_{,t} + A q_{,x} = 0$$

$$A = \begin{pmatrix} 0 & -\frac{1}{\rho} \\ -E & 0 \end{pmatrix} \quad [Aq] = 0 \quad \text{is it correct} \quad \begin{pmatrix} -\frac{1}{\rho} \delta \\ -E v \end{pmatrix} = 0$$

No it's not

but we know for this problem in conservation law correct

form $\rho_x = \begin{pmatrix} -\rho \\ -v \end{pmatrix} \Rightarrow \begin{pmatrix} \rho \\ v \end{pmatrix}$ continuous on the material interface

$$q_{,t} + A_2 q_{,x} = 0 \quad A_2 = \begin{pmatrix} 0 & \frac{1}{\rho} \\ -E & 0 \end{pmatrix}$$

$$y_{,t} + N y_{,x} = U$$

$$A^2 \begin{pmatrix} -E & 0 \end{pmatrix}$$

To get the jump conditions: \rightarrow solve the RIGHT eigenvalue problem

$$\det(A - \lambda I) = 0$$

$$\det \begin{pmatrix} -\lambda & -\frac{1}{\rho} \\ -E & -\lambda \end{pmatrix} = 0$$

$$\rightarrow \lambda = \mp c$$

$$c = \sqrt{\frac{E}{\rho}}$$

eigen vectors

$$\lambda = -c$$

$$\begin{pmatrix} c & \frac{1}{\rho} \\ -E & c \end{pmatrix} \begin{pmatrix} v_1 \\ v_2 \end{pmatrix} = 0$$

$$c v_1 - \frac{1}{\rho} v_2 = 0 \rightarrow$$

$$\underbrace{c\rho}_{Z} v_1 - v_2 = 0$$

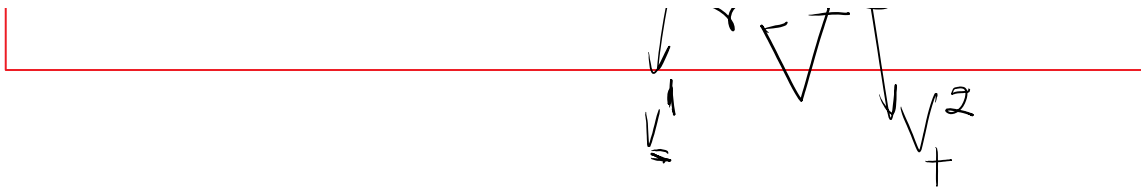
$$v_1 = 1 \quad v_2 = Z$$

$$\lambda^1 = -c, \vec{V}^1 = \begin{pmatrix} 1 \\ Z \end{pmatrix}$$

Similarly

$$\lambda^2 = c, \vec{V}^2 = \begin{pmatrix} 1 \\ -Z \end{pmatrix}$$

(3)



$$\begin{bmatrix} \alpha_1 \\ \alpha_2 \end{bmatrix} = \bar{V}^{-1} [q] = \frac{1}{z^- + z^+} \begin{bmatrix} z^+ & 1 \\ z^- & -1 \end{bmatrix} [q]$$

$$\begin{aligned} \alpha_1 &= \frac{(z^+ [V] + [\delta])}{z^- + z^+} \\ \alpha_2 &= \frac{z^- [V] - [\delta]}{z^- + z^+} \end{aligned} \quad (6)$$

Now we have α 's we can obtain q 's one region after the other:

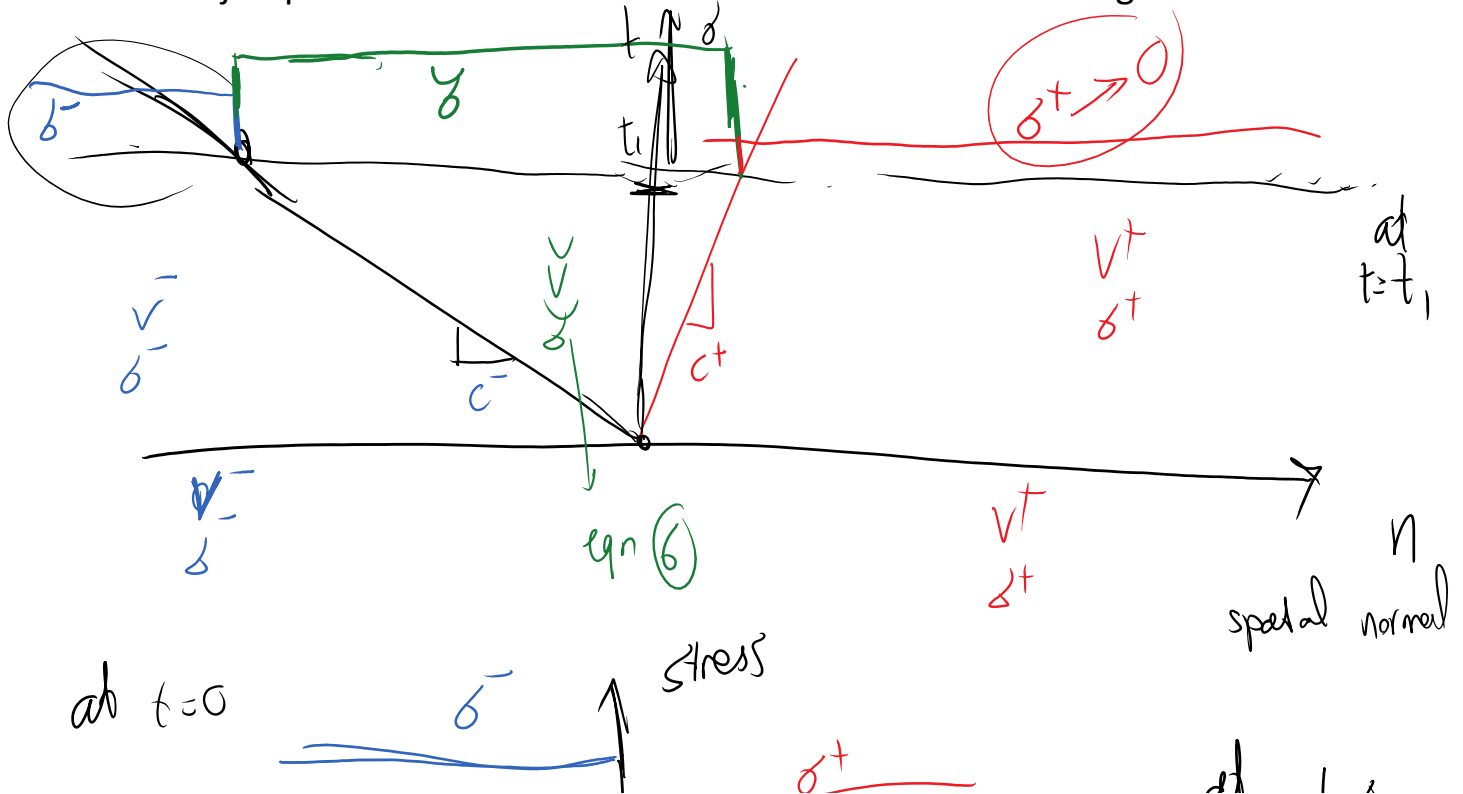
$$\begin{aligned} \check{q} - \bar{q} &= \alpha_1 \bar{V}_1 \\ \check{q} &= \bar{q} + \alpha_1 \begin{bmatrix} 1 \\ z^- \end{bmatrix} = \begin{bmatrix} V^- \\ \delta^- \end{bmatrix} + \frac{z^+ [V] + [\delta]}{z^- + z^+} \begin{bmatrix} 1 \\ z^- \end{bmatrix} \end{aligned}$$

$$\rightarrow \begin{pmatrix} v \\ \delta \end{pmatrix} = \begin{pmatrix} v^- + \frac{z^+ [v] + [\delta]}{z^- + z^+} \\ \delta^- + \frac{z^+ [v] + [\delta]}{z^- + z^+} \end{pmatrix} z^-$$

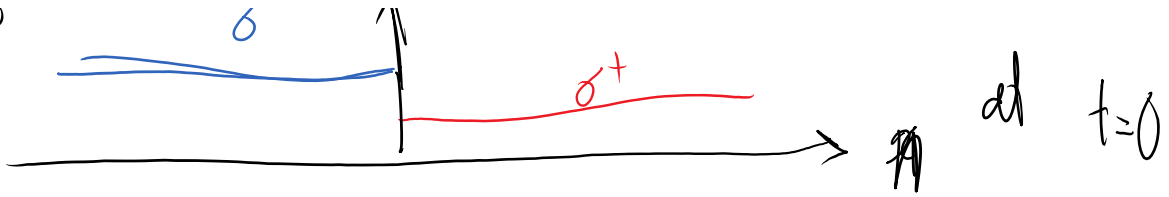
$$\begin{aligned} v &= \frac{v^- z^- + v^+ z^+}{z^- + z^+} + \frac{1}{z^- + z^+} [\delta] \\ \delta &= \frac{\delta^- z^+ + \delta^+ z^-}{z^- + z^+} + \frac{z^- z^+}{z^- + z^+} [v] \end{aligned} \quad (6)$$

As expected, this matches our solution from characteristic approach.

Relation of jump condition-based Riemann solutions and scattering coefficients



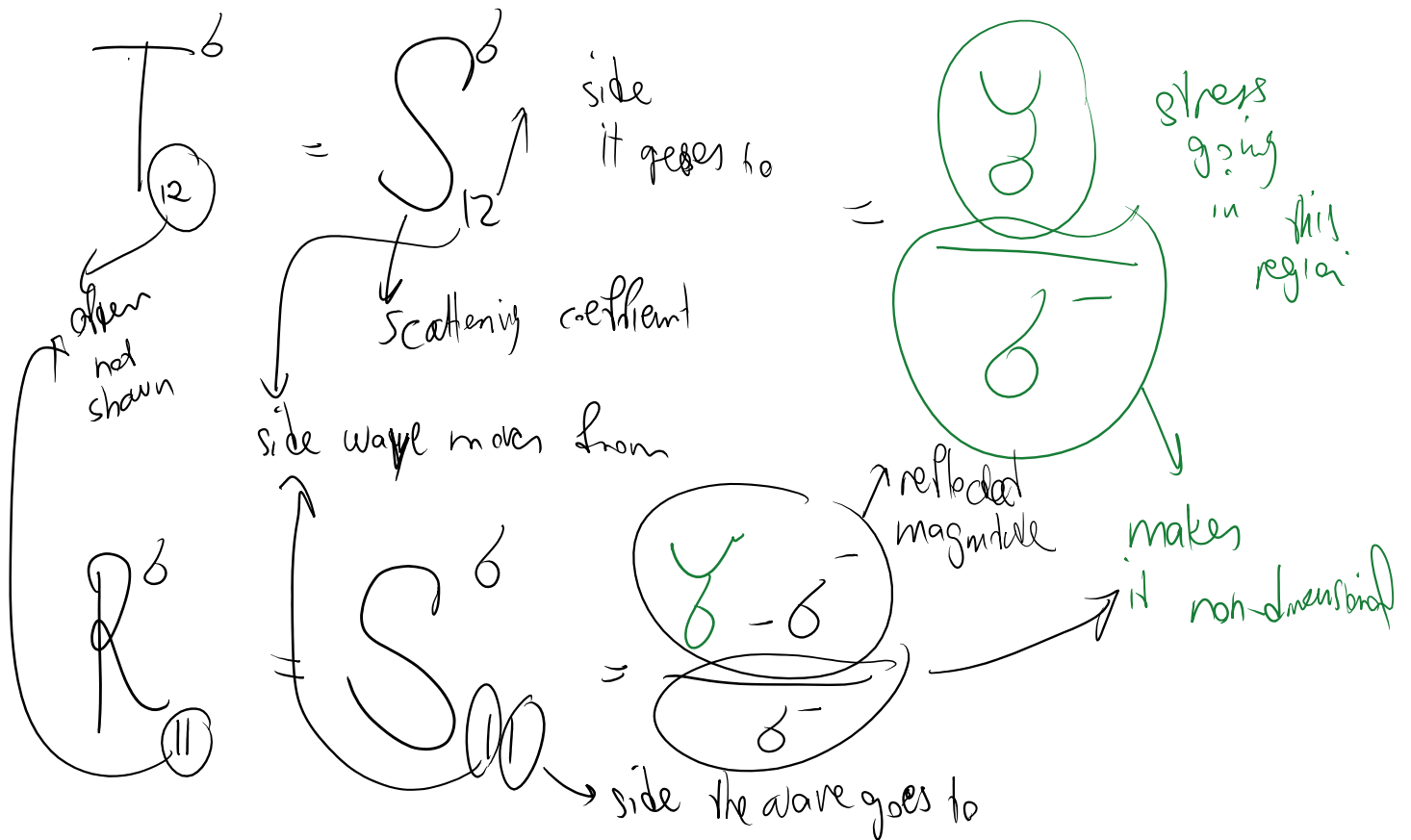
at $t=0$



To compute transmission and reflection coefficients we assume that there is a stress wave moving from the left side (-) and has reached the material interface at time $t = 0$.

On the right side (+) solution is zero at time zero ($\sigma^+, v^+ = 0$) (1)

As will be seen later "a stress wave moving to the right on the left side" \rightarrow imposes a relation between σ, v (2)



$$T^\sigma = S_{12} = \frac{\sigma}{\sigma^-} \quad T.R.I$$

$$\begin{aligned}
 1 &= \gamma_{11} = \frac{v}{\delta^-} \\
 R^\delta &= \delta_{11}^\delta = \frac{\gamma - \delta^-}{\delta^-} = \frac{\gamma}{\delta^-} - 1 \\
 T &= R + 1 \\
 \delta_{11}^\delta &= \delta_{11}^\delta + 1
 \end{aligned} \quad (7)$$

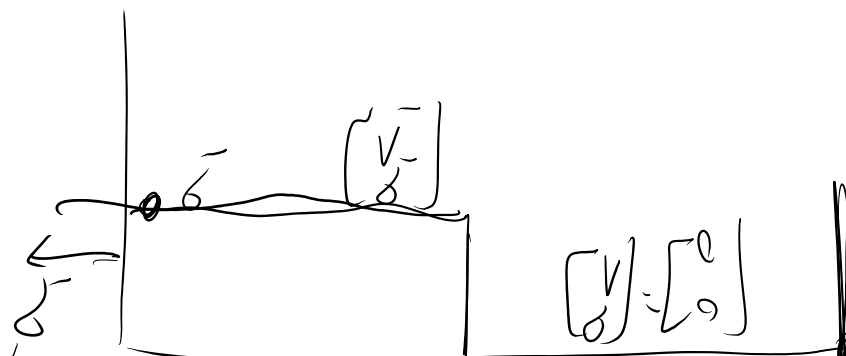
All we need to do is to plug γ in (7)

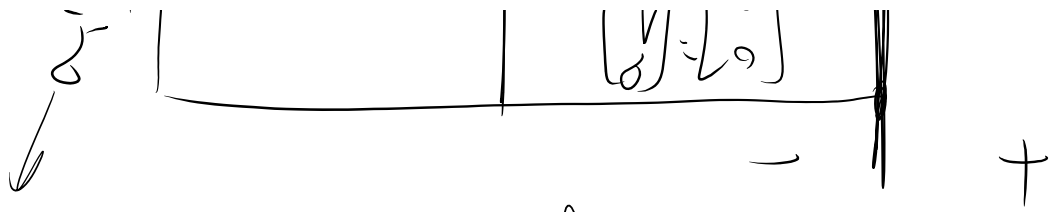
$$\gamma = \frac{\cancel{z^-} \delta^- + z^+ \delta^-}{z^- + z^+} + \frac{z^- z^+}{z^- + z^+} [v]$$

$$\begin{aligned}
 [v] &= \frac{v^+}{z^+} - v^- \\
 &= -v^-
 \end{aligned}$$

$$\gamma = \frac{z^+ \delta^-}{z^- + z^+} - \frac{z^- z^+}{z^- + z^+} v^- \quad (8)$$

For a "right-going" wave is there a condition between δ^-, v^-



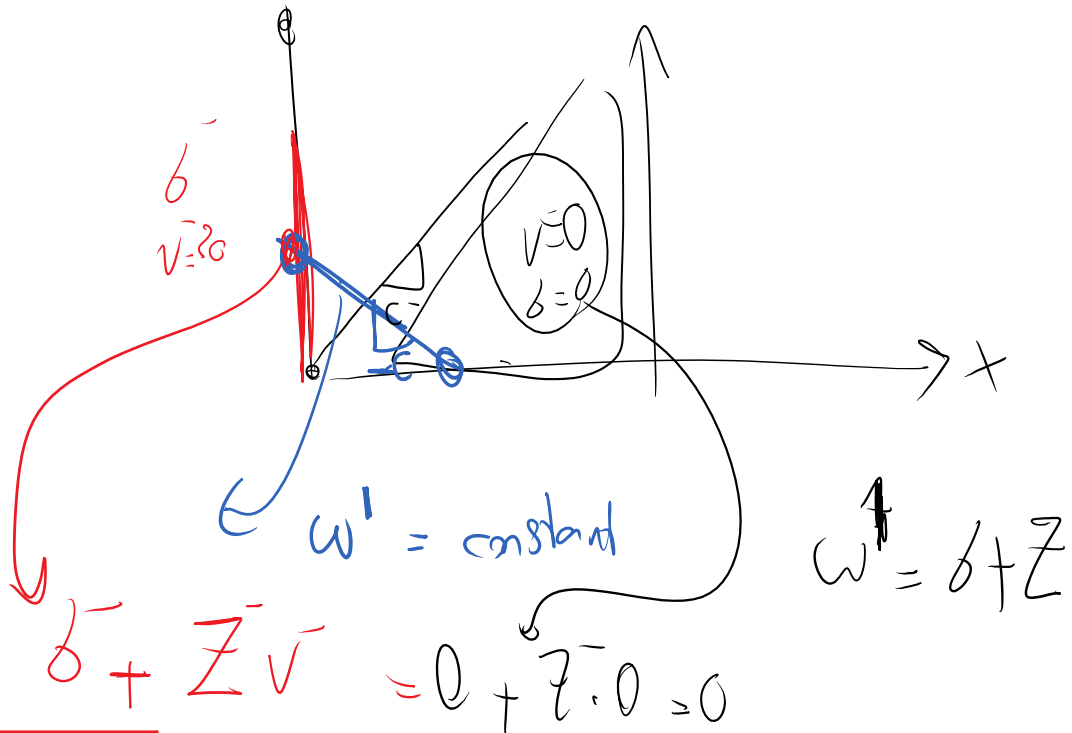


if δ^- is applied

natural BC

V^- is not specified

where V^- comes from?



$$V^- = -\frac{\delta^-}{Z^-} \quad (9)$$

$$|V| = \frac{\delta}{Z}$$

$$|\delta| = |V| Z$$

plug (9) into (8) to get:

$$\delta^- \rightarrow \delta^+, \quad \omega^- \rightarrow \omega^+, \quad \dots$$

$$\gamma = \frac{z^+ \delta^-}{z^- + z^+} - \frac{z^- z^+}{z^- + z^+} \begin{pmatrix} -\delta^- \\ z^- \end{pmatrix}$$

$$\gamma = \frac{z^+ \delta^- + z^+ \delta^-}{z^- + z^+} \rightarrow \boxed{\gamma = \frac{2z^+}{z^- + z^+} \delta^-} \quad 10$$

$$\rightarrow T = \frac{\gamma}{\delta^-} = \frac{2z^+}{z^- + z^+}$$

$$R = \frac{\gamma - \delta^-}{\delta^-} = T - 1 = \frac{2z^+ - z^- - z^+}{z^- + z^+} =$$

$$T = \frac{2z^+}{z^- + z^+}$$

$$R = \frac{z^+ - z^-}{z^- + z^+}$$

$\rightarrow \delta_{\perp}$
 δ_{\parallel}

$$\frac{z^+ - z^-}{z^- + z^+}$$