

Some points on PML from last time:

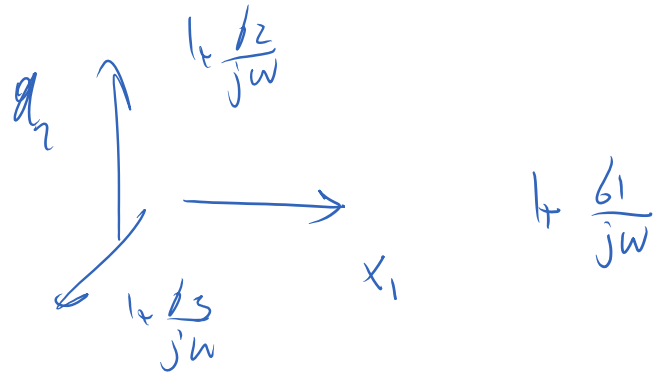
stretching looks like $S(\omega) = 1 + \frac{\sigma_i}{j\omega}$

σ_i 's have units of frequency

direction

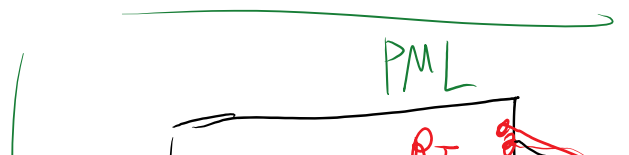
frequency

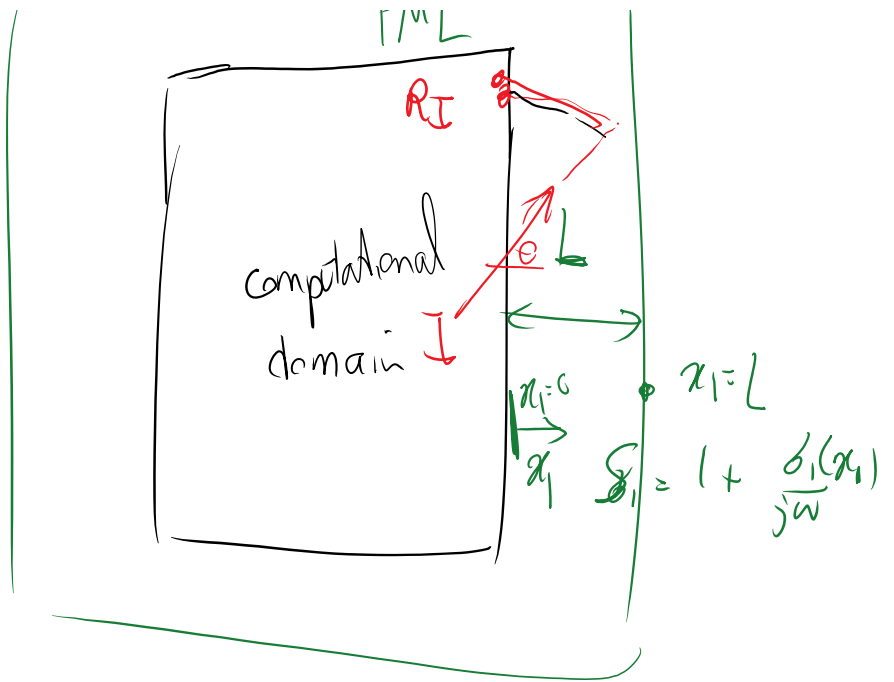
imaginary number $j^2 = -1$



there are better stretching functions that work well for evanescent waves and for $\omega \rightarrow 0, \infty$.

- these materials are dispersive (properties depend on ω)
- very difficult to model in time domain (TD).





$R =$
 reflection coefficient = $\exp\left(-\frac{2c\theta}{\text{wave speed}} \int_0^L \delta(x_1) dx_1\right)$

$\delta(x_1)$ constant

$S_1 = 1 + \frac{\delta_1}{j\omega}$ ← constant

$$R = \exp\left(-2c\theta \frac{L\delta_1}{c}\right)$$

$\theta \rightarrow \frac{\pi}{2}$ worst

$\theta \rightarrow 0$ the best

$L \rightarrow \infty$ $R \rightarrow 0$ ✓
 $\delta_1 \rightarrow \infty$ $R \rightarrow 0$

$R \dots 1 \dots \delta_1(x)$

0 1

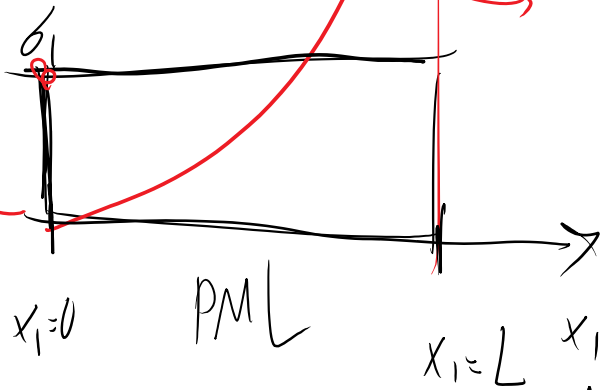
$$S_i(\omega) = 1 + \frac{\sigma_1(x)}{j\omega}$$

$$\sigma_1(x) = \sigma^0 \left(\frac{1}{L-x} - \frac{1}{x} \right)$$

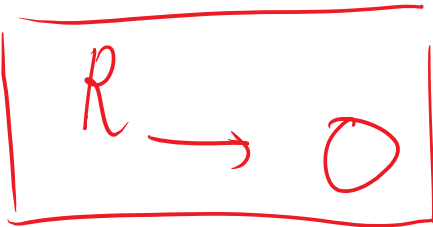
$$\sigma_1(0) = 0$$

$$\sigma_1(L) \rightarrow \infty$$

Comp. domain

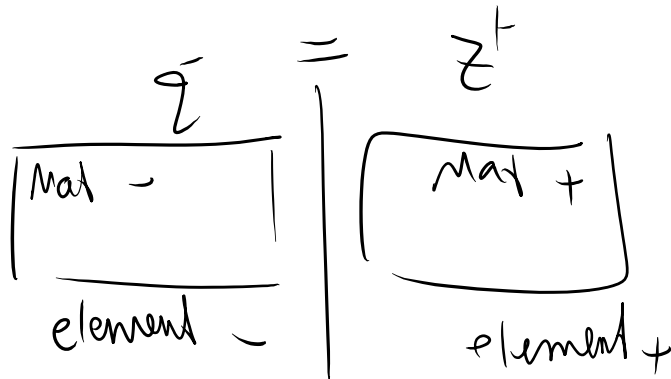


shifted hyperbolic function



- benefits
1. No sudden material property change
 2. $\sigma(x \rightarrow L) \rightarrow \infty \Rightarrow R \rightarrow 0$
- Continuum aspects

Even if two materials have matching impedances \rightarrow
numerically we get some reflection



but have some numerical reflection! Guddadi!

that's where property ① becomes useful.

In DG methods the continuity of material property is not as important and in fact some studies show that unlike CFEM, FD, a sudden jump in σ_1 (constant value) may still result in better numerical results.

Going back to 2D, 3D, Riemann solutions

2D x time

$$\dot{p} + p_{x_1, x_1} + p_{x_2, x_2} + p_{x_3, x_3} = s$$

\downarrow
 q

q^+
 $n(y_1)$
 $\vec{n}_y = (1, 0)$

often we assume that on each side we have constant value

The best way is to solve this in the local coordinate system

$$\dot{p} + p_{y_1, y_1} + p_{y_2, y_2} + p_{y_3, y_3} = s$$

\downarrow
 these quantities are zero because of IC set up

$$n_y = (1, 0, 0)$$

↓ spatial normal

$$f \cdot n =$$

$$p_y^x n_{y_1} + p_y^y \frac{n_{y_2}}{0} + p_y^z \frac{n_{y_3}}{0}$$

$$= p_y^x n_{y_1}$$

that's all we need

Benefits of stn in local coordinate:

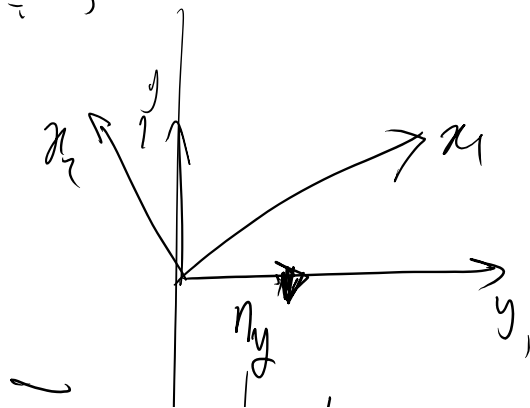
- ① Right away get rid of p_y^z, p_y^y
- ② we only get what's needed p_y^x

To demonstrate this better, let's consider a linear problem

$$q + A_1^x q_{lx_1} + A_2^x q_{lx_2} + A_3^x q_{lx_3} = f \quad \text{from top}$$

$$q_{ly_1} = A_1^x \begin{pmatrix} x \\ y \\ 0 \end{pmatrix}_1 + A_2^x \begin{pmatrix} x \\ y \\ 0 \end{pmatrix}_2 + A_3^x \begin{pmatrix} x \\ y \\ 0 \end{pmatrix}_3$$

$$= A_n$$



$$\dot{q} + A_n q_{y_1} = g$$

$$= A_n \quad - \quad \left| \begin{array}{c} n_y \\ \vdots \end{array} \right. + \quad \left. \begin{array}{c} \vdots \\ g \end{array} \right.$$

expressed in x system

typical routine for star value calculation

① q^{x-}, q^{x+}

values are computed in global x coordinate system

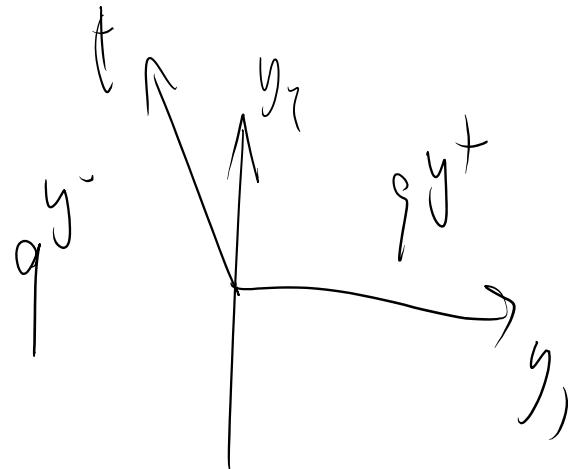


use n_y^x (normal vector n_y expressed in x system) to rotate components of q^{x-}, q^{x+} to y coordinate system

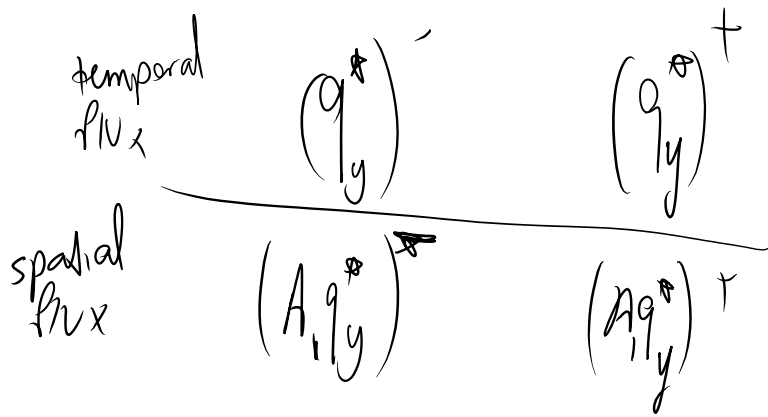
②

q^{y-}, q^{y+}

compute A_1 matrix as well

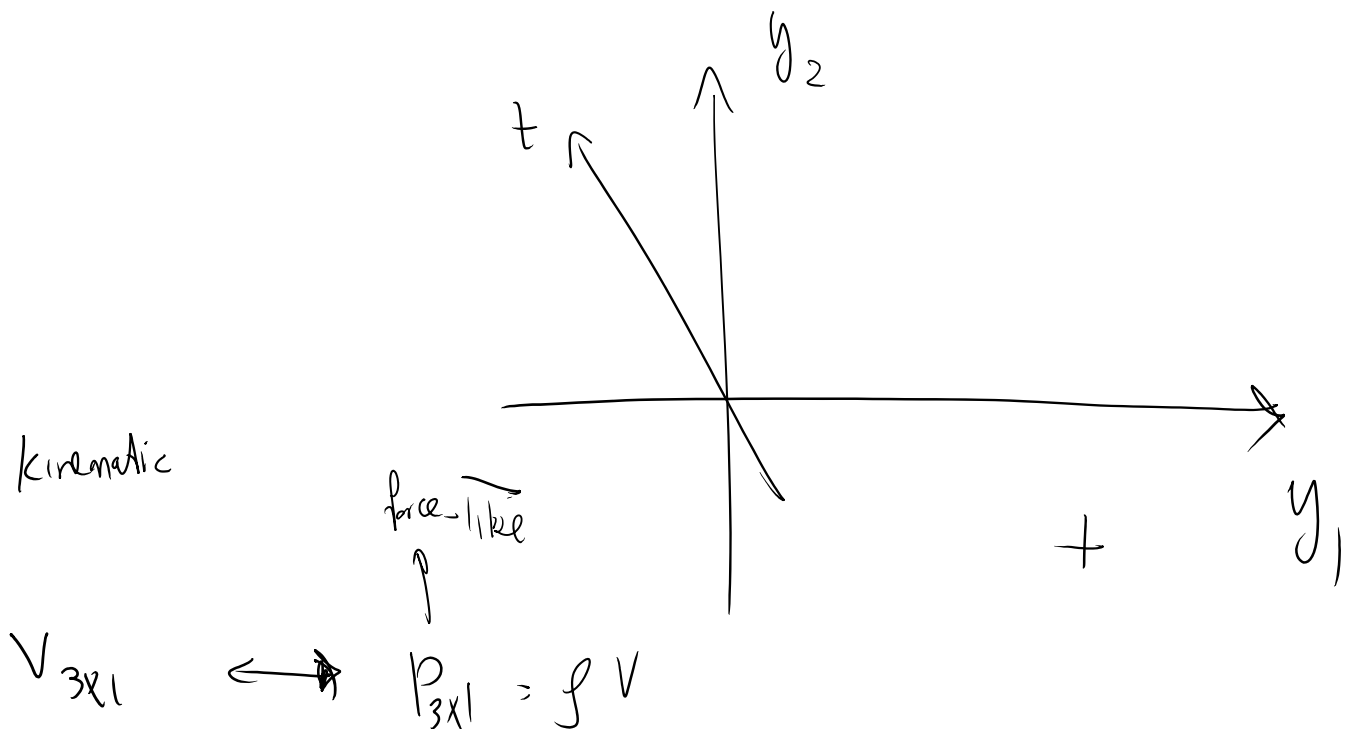


③ Solve the Riemann problem



(3) Most often the WRS is objective & can be expressed in any coordinate system including y , so we directly compute WRS (WRS) in this system

Example: 3D elastodynamics:



$$\epsilon_{3 \times 3} \text{ symmetric tensor} \longleftrightarrow \sigma_{3 \times 3} = C_{3 \times 3 \times 3 \times 3} \epsilon_{3 \times 3}$$

Using Voigt notation

$$\gamma = \begin{bmatrix} \epsilon_{11} \\ \epsilon_{22} \\ \epsilon_{33} \\ \epsilon_{12} \\ \epsilon_{23} \\ \epsilon_{31} \end{bmatrix}$$

$$S = \begin{bmatrix} S_{11} \\ S_{22} \\ S_{33} \\ S_{12} \\ S_{23} \\ S_{31} \end{bmatrix}$$

$$S_{6 \times 1} = C_{6 \times 6} \gamma_{6 \times 1}$$

Voigt stresses

$$\gamma_{6 \times 1} = D_{6 \times 6} S_{6 \times 1}$$

compliance

$$f_n = \begin{bmatrix} \epsilon \\ S \\ \gamma \\ V \end{bmatrix}$$

$$V_{3 \times 1} \longleftrightarrow P_{3 \times 1} = pV$$

$$\gamma_{6 \times 1} \longleftrightarrow S_{6 \times 1} = C_{6 \times 6} \gamma$$

$$\begin{bmatrix} p \\ P \\ \epsilon \\ E \end{bmatrix}_n - \begin{bmatrix} \gamma \\ V \\ V \\ V \end{bmatrix} = 0$$

$$v_{6 \times 1} \longleftrightarrow \gamma_{6 \times 1} = C_{6 \times 6}^v \gamma$$

$$C_{6 \times 6}^v - \underbrace{v_{6 \times 6}} = v$$

$\begin{matrix} P \\ \gamma \end{matrix} \rightarrow \text{should go to } 9 \text{ vector}$

what if we want to make our lives easier in terms of interface matching conditions

I prefer working with spatial flux quantities put in q as 1) in case of material property jumps the solution on vertical interface does not jump $[fy] = 0$, 2) we need spatial fluxes on vertical faces anyway (for most DGs).

$$q = \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ \hline s_{11} \\ s_{22} \\ s_{33} \\ s_{12} \\ s_{23} \\ s_{31} \end{bmatrix}$$

$\begin{matrix} v_2 \\ s_{12} \\ s_{21} \end{matrix}$

$$\begin{array}{l}
 6 \text{ eqns} \\
 \frac{1}{\rho} \nabla \cdot \sigma = \dot{p} - \nabla \cdot b = pb \quad 3 \text{ eqns} \\
 \dot{\epsilon}_{3 \times 3} - \nabla v = 0 \quad 6 \text{ eqns} \\
 C \times \sigma
 \end{array}$$

$$\begin{cases} \dot{V} - \frac{1}{\rho} \nabla \cdot \sigma = b \\ \dot{\sigma} - C(\nabla V) = 0 \end{cases}$$

2a

$$\begin{aligned} \dot{V}_1 - \frac{1}{\rho} (\sigma_{11,1} + \sigma_{12,2} + \sigma_{13,3}) &= b_1 \\ \dot{V}_2 - \frac{1}{\rho} (\sigma_{21,1} + \sigma_{22,2} + \sigma_{23,3}) &= b_2 \\ \dot{V}_3 - \frac{1}{\rho} (\sigma_{31,1} + \sigma_{32,2} + \sigma_{33,3}) &= b_3 \end{aligned}$$

3 eqns

$$S_0 \begin{bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{33} \\ \sigma_{12} \\ \sigma_{23} \\ \sigma_{31} \end{bmatrix}$$

$$\begin{bmatrix} S_1 \\ S_2 \\ S_3 \\ S_4 \\ S_5 \\ S_6 \end{bmatrix} = D_{6 \times 6} \begin{bmatrix} \epsilon_{11} \rightarrow u_{1,1} \\ \epsilon_{22} \rightarrow u_{2,2} \\ \epsilon_{33} \rightarrow u_{3,3} \\ 2\epsilon_{12} \rightarrow (u_{1,2} + u_{2,1}) \\ 2\epsilon_{23} \rightarrow (u_{2,3} + u_{3,2}) \\ 2\epsilon_{31} \rightarrow (u_{3,1} + u_{1,3}) \end{bmatrix}$$

take the
time
derivative

$$\dot{S} - D \begin{bmatrix} V_{1,1} \\ V_{2,2} \\ V_{3,3} \\ V_{1,2} + V_{2,1} \\ V_{2,3} + V_{3,2} \\ \vdots \end{bmatrix} = 0$$

2b

6 eqns

$$\begin{pmatrix} v_{2,3} + v_{3,2} \\ v_{3,1} + v_{1,3} \end{pmatrix}$$

9 eqns

for example 1st eqn for 2D

$$S_1 - G_{11} v_{1,1} - D_{12} v_{2,2} - D_{13} v_{3,3} - D_{14} (v_{1,2} + v_{2,1}) - D_{15} (v_{2,3} + v_{3,2}) - D_{16} (v_{3,1} + v_{1,3}) = 0$$

2 others are

$$S_4 - S_{41} v_{1,1} - D_{42} v_{2,2} - D_{43} v_{3,3} - S_{44} (v_{1,2} + v_{2,1}) - D_{45} (v_{2,3} + v_{3,2}) - S_{46} (v_{3,1} + v_{1,3}) = 0$$

$$\dot{q} + \dots = 0$$

$$q =$$

$$\begin{pmatrix} v_1 \\ v_2 \\ v_3 \\ S_1 \\ S_2 \\ S_3 \\ S_4 \\ S_5 \\ S_6 \end{pmatrix}$$

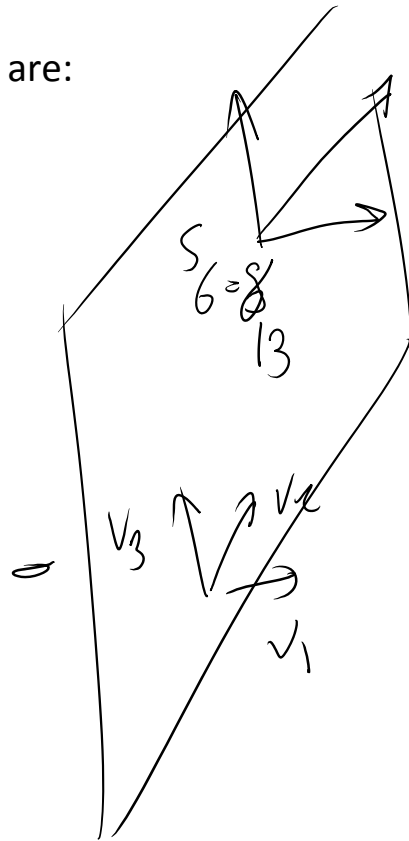
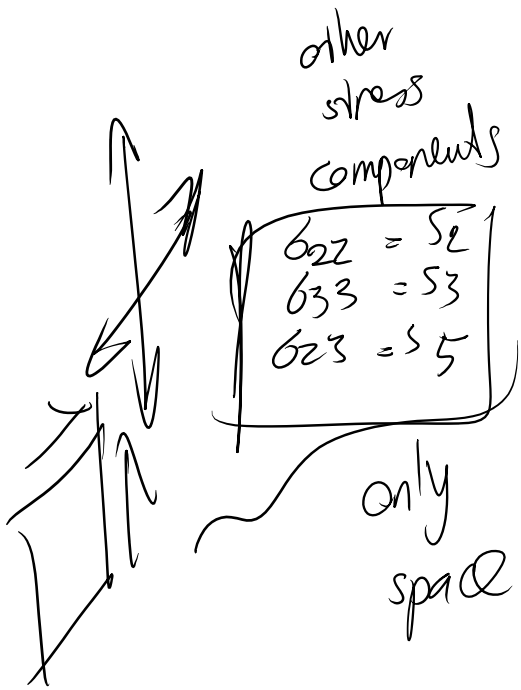
$$\dot{q} + A_1 q_{,1} + A_2 q_{,2} + A_3 q_{,3} = 0$$

$A =$

	$V_{1,1}$	$V_{2,1}$	$V_{3,1}$	$S_{1,1}$	$S_{2,1}$	$S_{3,1}$	$S_{4,1}$	$S_{5,1}$	$S_{6,1}$
V_1				$-p$					
V_2							$-p$		
V_3									$-p$
S_1	C_{11}	C_{14}	C_{16}						
S_2	C_{21}	C_{24}	C_{26}						
S_3	C_{31}	C_{34}	C_{36}						
S_4	C_{41}	C_{44}	C_{46}						
S_5	C_{51}	C_{54}	C_{56}						
S_6	C_{61}	C_{64}	C_{66}						

A_1

The eigenvalue for this matrix are:



$$S_4 = \sigma_{12} \quad \sigma_{1i}$$

$$S_1 = \sigma_{11}$$

+

v_1, v_2, v_3 are continuous

$\sigma_{11}, \sigma_{12}, \sigma_{13}$

S_1, S_4, S_6 are continuous

$\sigma_{23}, \sigma_{33}, \sigma_{32}$
can suffer jump