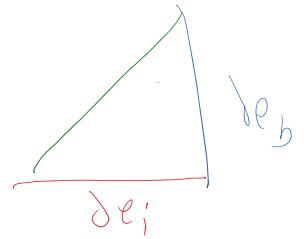


Weighted residual copied for the element on the right boundary

$$\int_e \left[ \hat{T}(a_3 + a_5) + \hat{q}(a_6 + a_2 + a_4 + a_5 x + a_6 t) \right] dv$$

$$+ \int_{\partial e_i} \hat{T}(a_1 + a_2 x + a_3 t) + \hat{q}(a_4 + a_5 x + a_6 t) dt$$

$$+ \int_{\partial e_b} \hat{q}(1 - (a_2 + a_5 x + a_6 t)) dt = 0$$



$$\hat{T} = \begin{pmatrix} 1 \\ x \\ t \\ 0 \\ 0 \\ 0 \end{pmatrix} \quad \hat{q} = \begin{pmatrix} 0 \\ 0 \\ 1 \\ x \\ t \\ 0 \end{pmatrix}$$

$\int x \cdot x \, dv$      $\int x \cdot t \, dv$      $\int t \cdot t \, dv$      $\int x \, dv$      $\int t \, dv$

$\int_e x \cdot x \, dv = A \left( \frac{|x| + |x|}{6} + \frac{|x| + |x|}{12} \right) = \frac{A}{2} \quad (A = \frac{1}{2})$

$\int_e x \cdot t \, dv = A \left( \frac{|x|}{6} + \frac{|t|}{12} \right) = \frac{A}{4}$

all interior integrals

$\int_e x \, dA = \frac{2}{3} A$	$\int_e t \, dA = \frac{1}{3} A$
$\int_e x^2 \, dA = \frac{1}{2} A$	$\int_e t^2 \, dA = \frac{1}{6} A$ ★
$\int_e x t \, dA = \frac{1}{4} A$	

$I_i$  interior integral =  $\begin{pmatrix} 1 \\ x \\ t \\ 0 \\ 0 \\ 0 \end{pmatrix} (a_3 + a_5) + \begin{pmatrix} 0 \\ 0 \\ 0 \\ 1 \\ x \\ t \end{pmatrix} (a_6 + a_2 + a_4 + a_5 x + a_6 t) \, dA$

interior integral =  $\int_{\hat{\Omega}} (a_3 + a_5) \mathbf{1} \cdot \mathbf{n} \, d\hat{\Omega}$

$$= A \left\{ \begin{matrix} a_3 + a_5 \\ \frac{2}{3}(a_3 + a_5) \\ \frac{1}{3}(a_3 - a_5) \\ 0 \\ 0 \\ 0 \end{matrix} \right\} + \begin{matrix} 0 \\ 0 \\ 0 \\ a_6 + a_2 + a_4 + a_5 \times \frac{2}{3} + a_6 \frac{1}{3} \\ (a_6 - a_2 + a_4) \times \frac{2}{3} + a_5 \frac{1}{3} + a_6 \frac{1}{4} \\ (a_6 + a_2 + a_4) \frac{1}{3} + a_5 \frac{1}{4} + a_6 \frac{1}{6} \end{matrix}$$

use  $\star$

(1a)

Inflow face integral:

$$I_{inf} = \int_{\partial \hat{\Omega}_i} \hat{T} (a_1 + a_2 x + a_3 t) + \hat{q} (a_4 + a_5 x + a_6 t) \, d\hat{\Omega}_i$$

$t=0$

We can either use constant, linear, and bi-linear integrals for a line from the last session or in this particular case, simply integrate over x

$$\int_0^1 \begin{bmatrix} 1 \\ x \\ 0 \\ 0 \\ 0 \end{bmatrix} (a_1 + a_2 x + a_3 t) + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \\ 0 \end{bmatrix} (a_4 + a_5 x + a_6 t) \, dx$$

$$I_{inf} = \begin{bmatrix} a_1 \frac{1}{2} \\ a_1 \frac{1}{2} + a_2 \frac{1}{3} \\ 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ a_4 + a_5 \frac{1}{2} \\ a_4 \frac{1}{2} + a_5 \frac{1}{3} \end{bmatrix}$$

(1b)

Finally, we have the boundary integral

$$I_b = \int_{\partial \hat{\Omega}_b} \hat{q} (1 - a_4 - a_5 x - a_6 t) \, d\hat{\Omega}_b$$

$$= \int_{t=0}^1 \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \\ 0 \end{bmatrix} (1 - a_4 - a_5(1) - a_6(t)) \, dt$$

$$\begin{bmatrix} 1 \\ -x \\ t \end{bmatrix}$$

$$\bar{f}_b = \begin{bmatrix} 0 \\ 0 \\ 0 \\ -a_4 - a_5 - a_6/2 \\ -a_4 - a_5 - a_6/2 \\ a_4/2 - a_5/2 - a_6/3 \end{bmatrix}$$

→ go to the RHS

1c

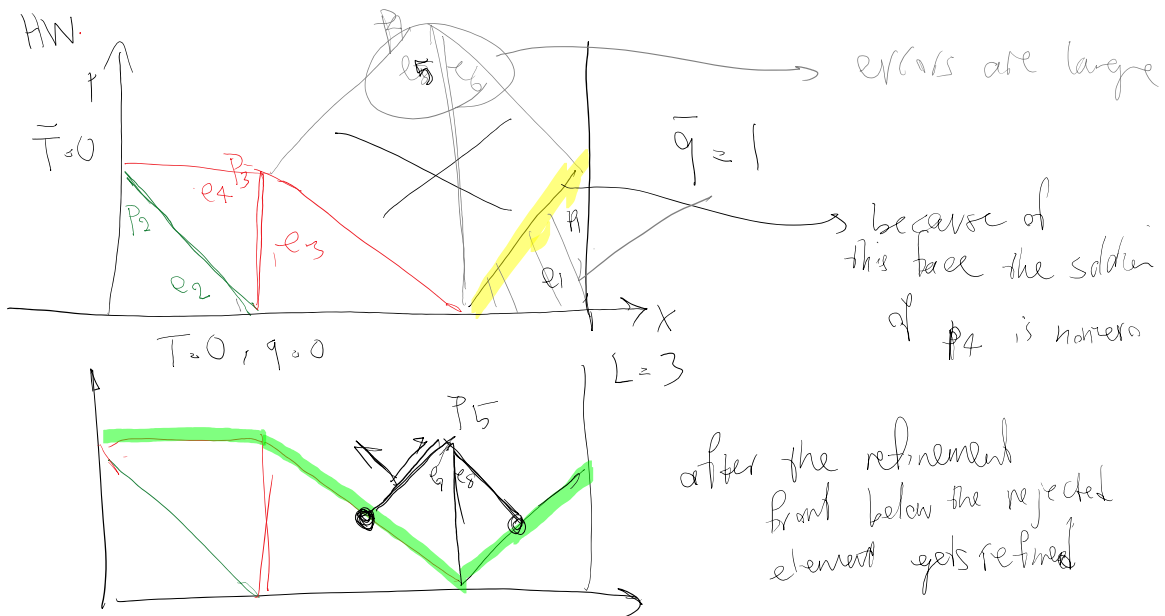
1a, 1b, 1c

$$\bar{f}_i + \bar{f}_b + \bar{f}_s = 0 \Rightarrow$$

$$K_{6 \times 6} a_{6 \times 1} = F_{6 \times 1} \rightarrow a = \begin{bmatrix} 0 \\ 0 \\ -3.27 \\ -6 \\ 3.27 \\ 15.27 \end{bmatrix}$$

$$T = -3.27t$$

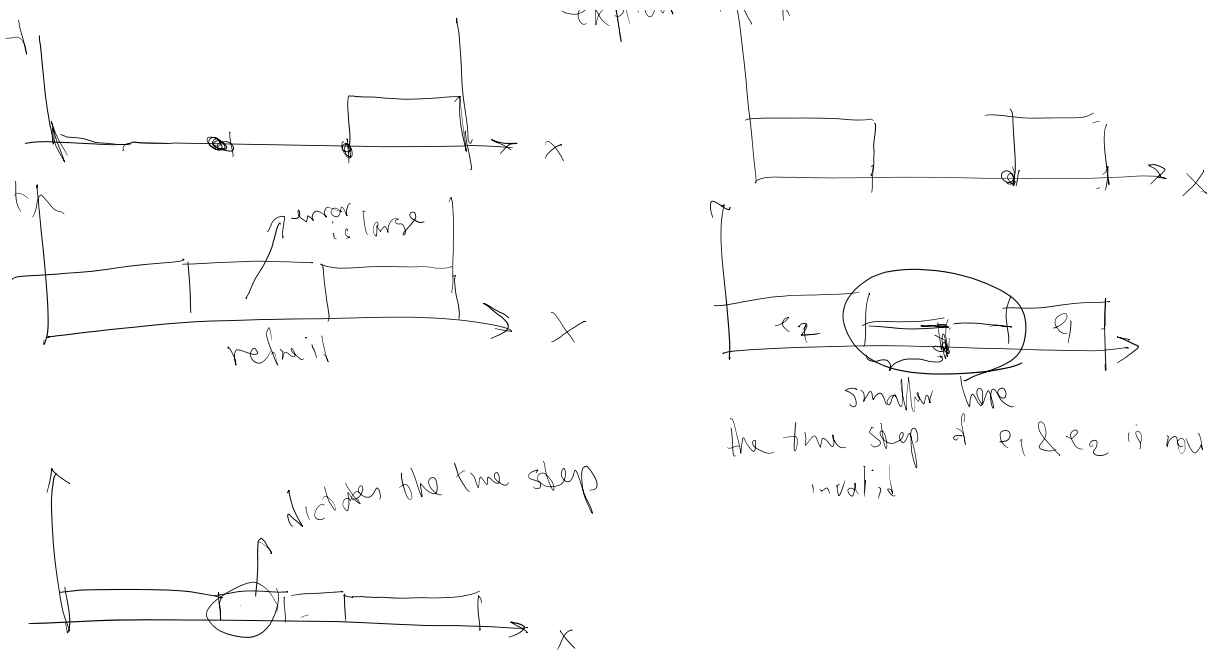
$$q = -6 + 3.27x + 15.27t$$



Because of the refinement both spatial and temporal size of the element decrease.

Comparison with a time marching scheme



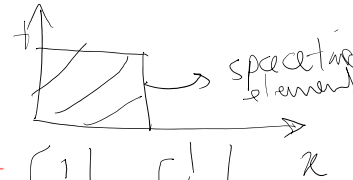


Advantages of cSDG method:

- Achieving high temporal orders in **semi-discrete methods (CFEMs and DGs)** is **very challenging** as the solution is only given at discrete times.
- Perhaps the **most successful method** for achieving high order of accuracy in **semi-discrete** methods is the Taylor series of solution in time and subsequent use of **Cauchy-Kovalevski or Lax-Wendroff procedure (FEM space derivatives  $\Rightarrow$  time derivatives)**. However, this method becomes increasingly challenging particularly for nonlinear problems.
- High temporal order adversely affect stable time step size for explicit DG methods (e.g.  $\frac{1}{2p+1}$  or worse for RKDG and ADER-DG methods).

Achieving high temporal order in time marching methods is difficult

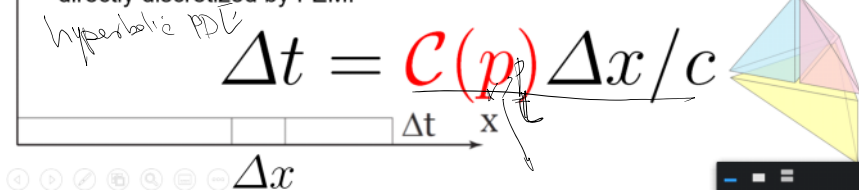
- Any spacetime method can easily achieve high order of accuracy in time



$$\begin{bmatrix} 1 \\ x_1 \\ x_2 \\ x_3 \end{bmatrix} \otimes \begin{bmatrix} 1 \\ t_1 \\ t_2 \\ t_3 \end{bmatrix}$$

$P_x = 3$     $P_t = 7$

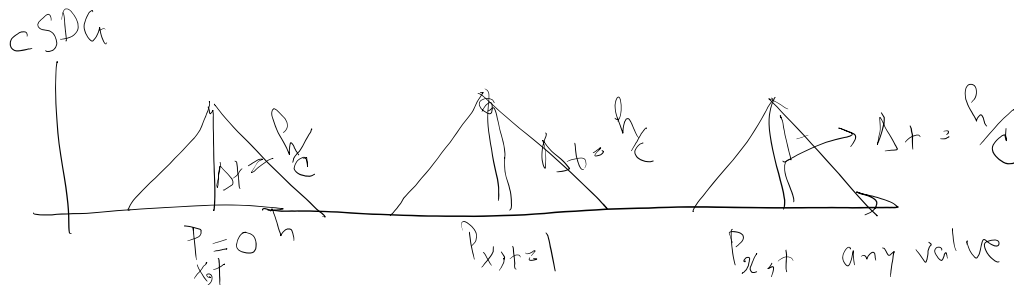
- Spacetime (CFEM and DG) methods**, on the other hand can achieve **arbitrarily high temporal order of accuracy** as the solution in time is directly discretized by FEM.



$C^r$  depends on spatial & temporal discretization types & orders in space time

$P_t = 5$     $C \sim \frac{1}{11} \approx 0.1$

For a 5th order method in time, the maximum time advance is reduced by about an order of magnitude.



In cSDG method, since the only constraint is keeping the outflow facets causal, the order of element has no effect on the maximum time advance of a vertex.

- Just because of this simple fact, for  $p = 5$ , the maximum step of cSDG method is about 10x of EXRK5!

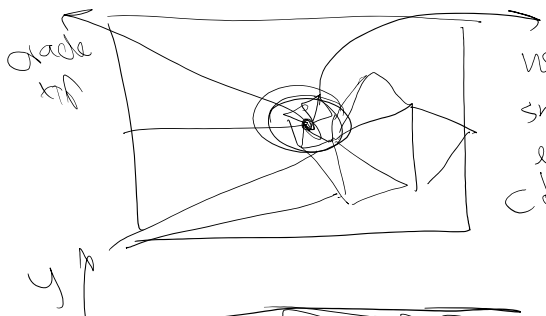
# 1. Asynchronous / no global time step

Problem statement:

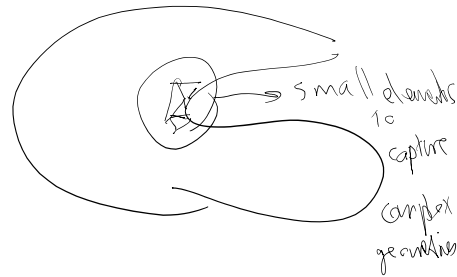
$$\Delta t = C(p) \Delta x / c$$

explicit method  
 Smallest element dictates global time step

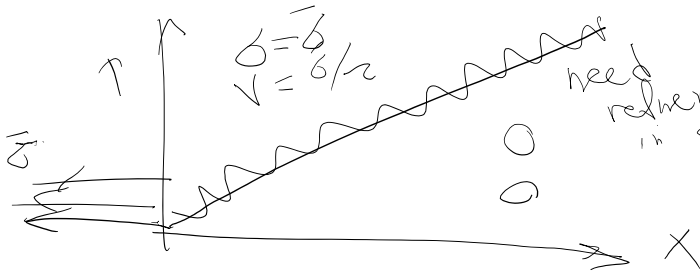
reasons for small elements



need small elements close to high gradient solution features



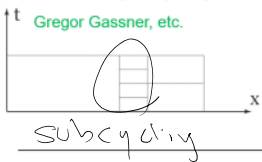
fluids need refined elements



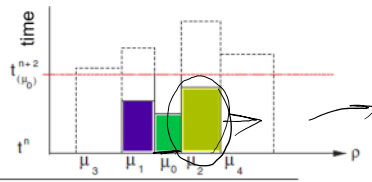
- **Implicit-Explicit (IMEX)** methods increase the time step by **geometry splitting** (implicit method for small elements) or **operator splitting**.



- **Local time-stepping (LTS)**: subcycling for smaller elements enables using larger global time steps



Gregor Gassner, etc.  
 A. Taube, M. Dumbser, C.D. Munz and R. Schneider, A high-order discontinuous Galerkin method with time accurate local time stepping for the Maxwell equations, Int. J. Numer. Model. 2009: 22:77-103



ADER DG

With cSDG method

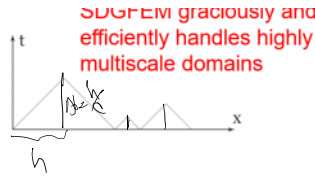
## aSDG

- Small elements locally have smaller progress in time (no global time step constrains)
- None of the complicated "improvements" of time

SDGFEM graciously and efficiently handles highly multiscale domains

ASDC

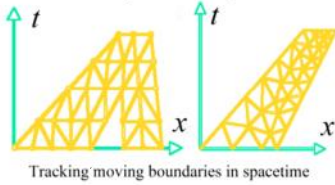
- Small elements locally have smaller progress in time (no global time step constrains)
- None of the complicated "improvements" of time marching methods needed



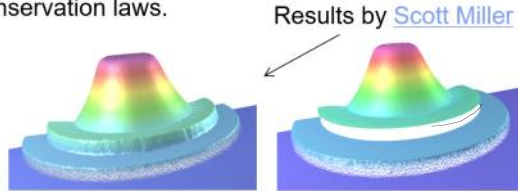
Each element takes its own 100% efficient maximum time advance.

## 2. Spacetime grids and Moving interfaces

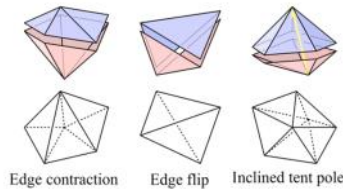
- **Problems with moving interfaces:**
  - \* Solid-fluid interaction
  - \* Non-linear free surface water waves
  - \* Helicopter rotors /forward flight
  - \* Flaps and slats on wings and piston engines
- Derivation of a conservative scheme is very challenging:
  - Even Arbitrary Lagrangian Eulerian (ALE) methods do not automatically satisfy certain geometric conservation laws.



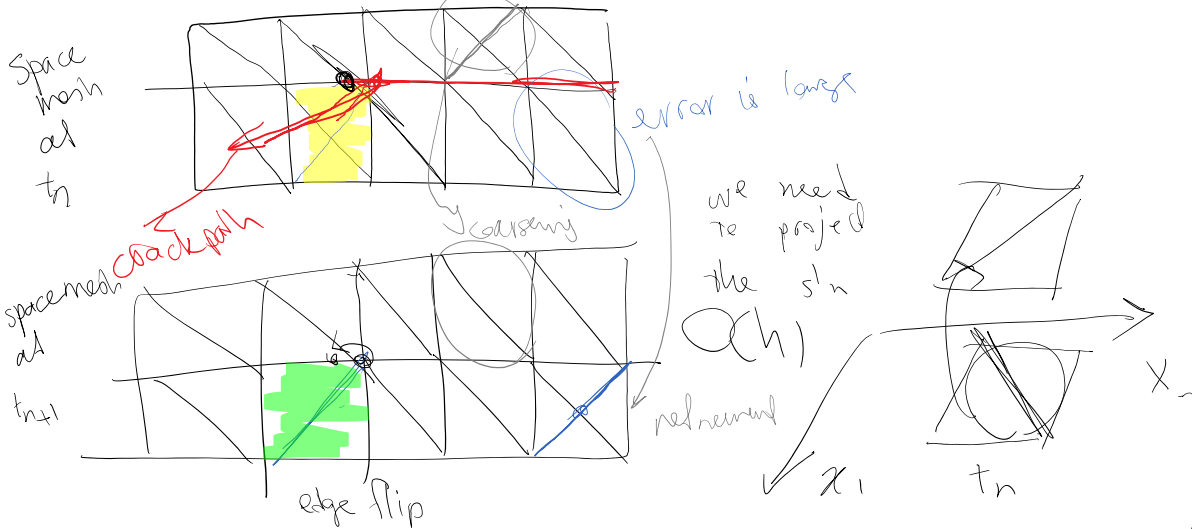
Tracking moving boundaries in spacetime



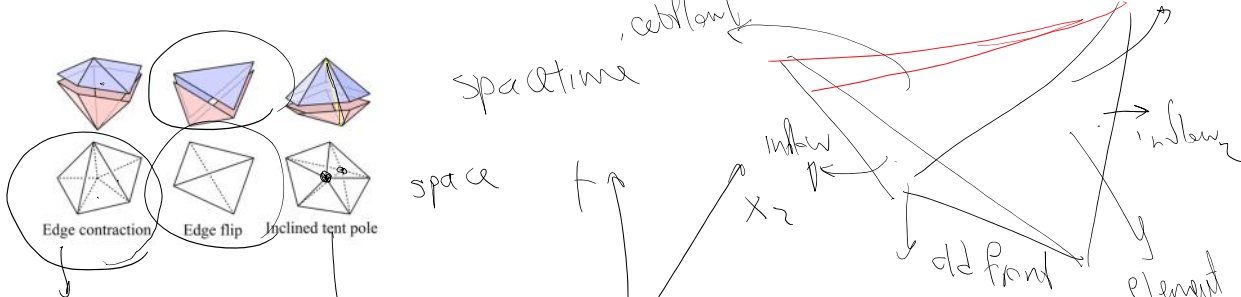
- **Spacetime mesh adaptive operations**  
Enable mesh smoothing and adaptive operations Without projection errors of semi-discrete methods.

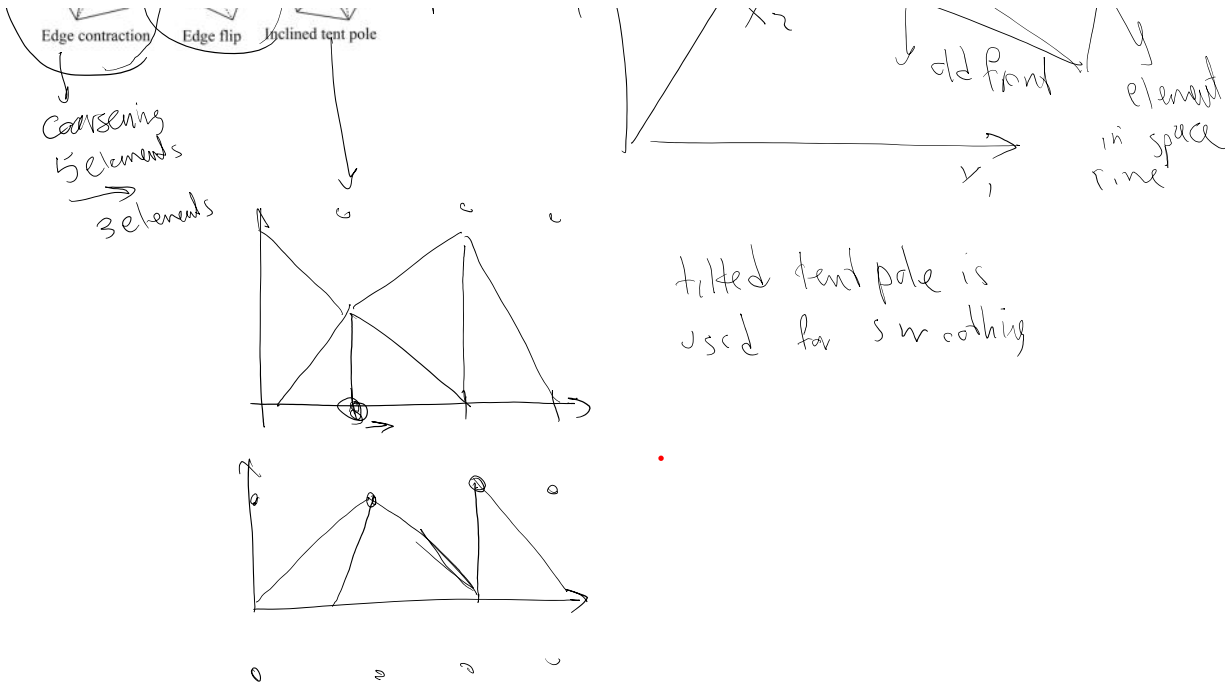


Time marching schemes going from an old space mesh to a new space mesh involves projection errors



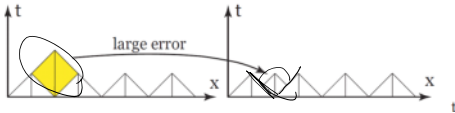
Refinement, edge flip, coarsening and even mesh smoothing operations involve projections from an old mesh to a new mesh.



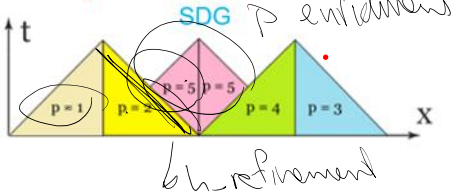


### 3. Adaptive mesh operations

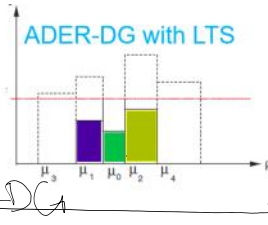
- Local-effect adaptivity: no need for reanalysis of the entire domain



- Arbitrary order and size in time:



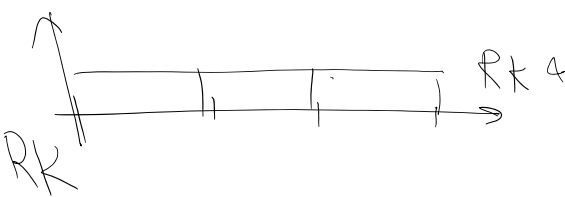
Example:  
LTS by  
Dumbser,  
Munz, Toro,  
Lorcher, et. al.



order in time can change element by element

h-refinement and p-enrichment can easily be done as with all the other DG methods (compared to CFEMs)

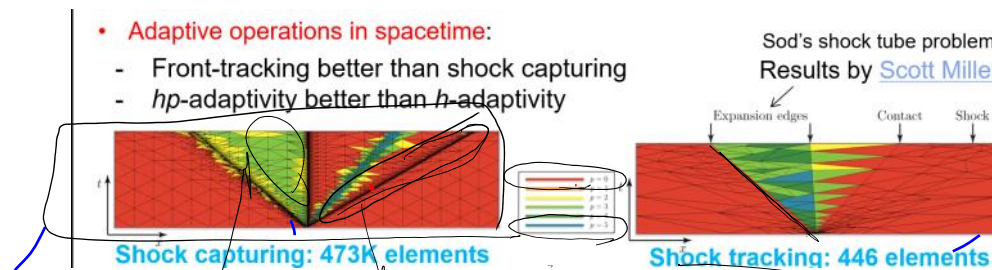
- The main advantage is that we can arbitrary change the order in time per element!



With time marching schemes it is very difficult to have different temporal orders for different parts of the domain.

- Adaptive operations in spacetime:

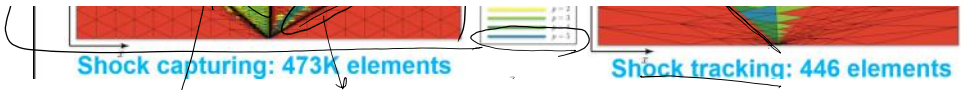
- Front-tracking better than shock capturing
- hp-adaptivity better than h-adaptivity



Why using  $p=0$  around shock

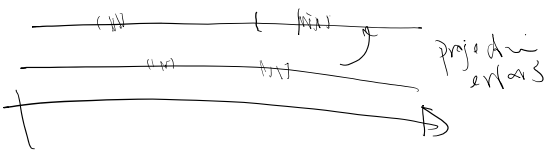
error =  $Ch^{min(p, 1)}$

exact solution regularity  $C^s$

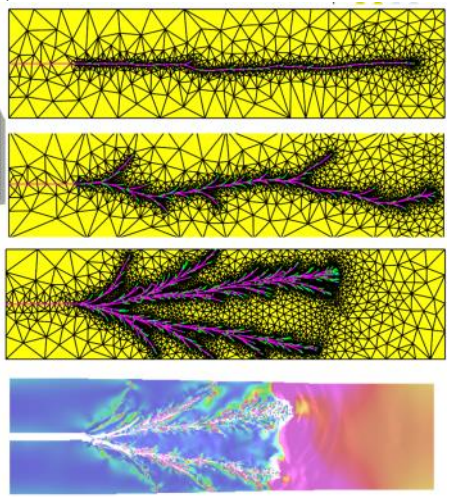


(2)  $p > 0$  unstable under high resolution

high order element  
 $p = 0$  along the shock

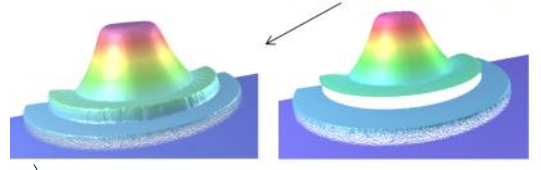


Same shock tracking schemes can be used to track crack faces in spacetime



2D version of the same problem above  
 observation laws.

Results by Scott Miller



shock capturing

shock tracking discontinuity