2016/04/06

Wednesday, April 06, 2016 11:39 AM

$$a_{p}\frac{\mathrm{d}^{p}u}{\mathrm{d}t^{p}} + a_{p-1}\frac{\mathrm{d}^{p-1}u}{\mathrm{d}t^{p-1}} + \dots + a_{1}\frac{\mathrm{d}u}{\mathrm{d}t} + a_{0}u(t) = 0 \qquad \Rightarrow \qquad u(t) = \sum_{i=1}^{\bar{p}} P_{i}(t)e^{\lambda_{i}t} \tag{368}$$

Numerical solution of systems as equation (368)

5.3.2.2 Absolute stability

• Consider the first order ODE,
$$\dot{x} - \lambda x = 0 \tag{373}$$

How can we solve (and also analyze) the stability of a p-th order ODE with the solution and analysis of first order ODE (373):

12 = (-5m) + im 11-52

12 = (-5W) + iW VI-52 $A_{1} e + A_{2} e + A_{3} e^{\lambda_{1}^{2} + \lambda_{1}^{2} + \lambda_{2}^{2}} e^{\lambda_{1}^{2} + \lambda_{1}^{2} + \lambda_{2}^{2}} e^{\lambda_{1}^{2} + \lambda_{1}^{2} + \lambda_{3}^{2}} e^{\lambda_{1}^{2} + \lambda_{1}^{2} + \lambda_{2}^{2}} e^{\lambda_{1}^{2} + \lambda_{1}^{2}} e^{\lambda_{1}^{2}} e^{\lambda_{1}^{2}} e^{\lambda_{1}^{2}} e^{\lambda_{$ $\lambda_1 = \lambda_2 = \sum_{i=1}^{n} \lambda_i$ uli) = A1 e + A2 te

Why the stability analysis of $a_{p}\frac{d^{p}u}{dt^{p}}+a_{p-1}\frac{d^{p-1}u}{dt^{p-1}}+\cdots+a_{1}\frac{du}{dt}+a_{0}u(t)=0$ we only consider optic where reduces to stability analysis all of $u=\int_{\mathbb{R}^{n}}u$ of $u=\int_{\mathbb{R}^{n}}u$

red u = Pilt) e Mil

whis is the showing

to u - Liuzo

we are interested in evaluating of a numerical method can stably solve

O = NK - V

for

h = AR + i Az

LET

 $\lambda_R < 0$

problems where physical solidien

time muching scheme has a bt

we care

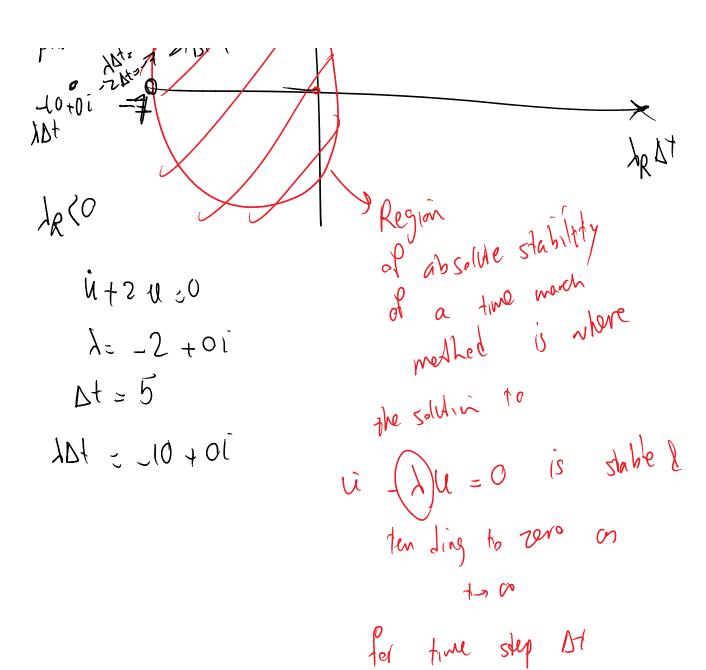
ahah

The P

plane

M. 7 101247.5

ett i th



Example Generalized Apphren
Real

U-Wu : 0 head

 $(1 + \alpha \Delta t \lambda^h)d_{n+1} = (1 + (1 - \alpha)\Delta t \lambda^h)d_n$

 $d_{n+1} = Ad_n$, where $A = \frac{1 + (1 - \alpha)\Delta t\lambda}{1 + \alpha \Delta t\lambda}$ Amplification factor

4/2

A stable method

Absolutely slable method

It's a numerical method

That the region of absolute stability overs

the entire negative real half place

This numerical method provides

stable soldier for any A when

stable soldier for any the Underlying physicial soldier is dynamically 0= W/- js he he that LR(0 Numerical method is slabk for Ahy

The difference between the concepts of A-stability and unconditional stability

 $\dot{x} - \lambda_0 x = 0, \quad (\lambda_0^I = 0, \lambda_0^R < 0)$ Assume la is real & negative fixed A numerical method for At is unconditionally shire it we can take arbitrary line step white still the numerical method is table 处域 schene is stable here for an undolonly slable numerial nellhood 10= 10+01: R. Dt = 1RAT +C u - 1, iu = b led by go from 0 to 00

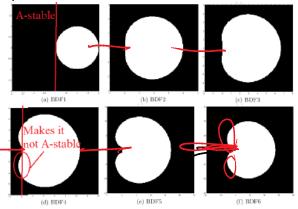
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Can se get well-behald numerical methods
LMS

That are higher order than 2

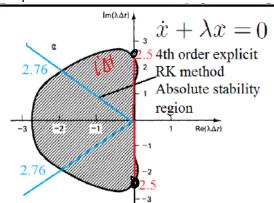
with some compromise on A-slahills

Compromise of BDF methods



Absolute stability regions: the region of absolute stability is the set of points in the complex plane outside the white region The region of absolute stability contains all the negative real axis. these methods are Undertranally stable for solving $\dot{u} = \lambda \ u = 0$

Use in practice



$$\ddot{x} + x = 0$$

$$\chi_{3} e^{\lambda t} \qquad \qquad \chi_{4|2} 0$$

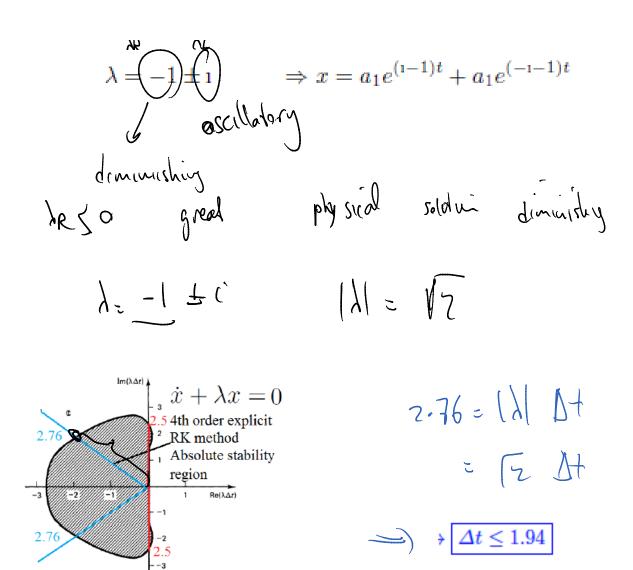
$$\lambda = \pm i$$

$$\chi_{4} e^{it} + \Lambda_{2} e^{it}$$

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 $\lambda_{2}, \lambda_{3} = \frac{1}$

 $\Rightarrow x = a_1 e^{(i-1)t} + a_1 e^{(-i-1)t}$

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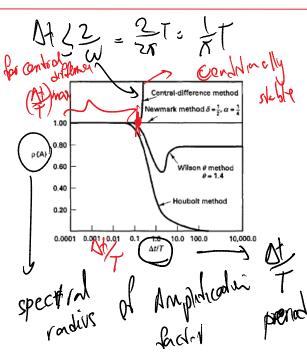
5.4.1 Control of high frequency numerical noise

- In the figure observe spectral radius of different time marching methods versus normalized element size.
- T = ω/2π is the period of a given SDOF.
- Clearly, as expected central-difference method becomes unstable for $\Delta t/T > \frac{1}{\pi}$: As we observed in (357) (also (358)) central difference method is stable if $\Delta t\omega \leq 2$, $T = \frac{\omega}{2\pi} \Rightarrow \Delta t/T \leq \frac{1}{\pi}$
- Other methods in the figure are unconditionally stable.
- One very important aspect of a time marching method in these plots is,

$$\rho_{\infty} = \lim_{\Delta t/T \to \infty} \rho(\mathbf{A}(\frac{\Delta t}{T})) \tag{387}$$

for example for Wilson- θ method $\rho_{\infty} \approx 0.8$

UN+1 = AUN



spectral radius Tperpod = Zj = Fw ODE of consideration i + waso Newmark method $\delta = \frac{1}{2}$, $\alpha = \frac{1}{4}$ 1.00 8· & /00/9 0.80 ρ**(Α)** 0.60 0.40 Houbolt method 0.20 0.0001 0.001 0.01 10.0 100.0 MDOF MÜ + KU:0 ~ + win=0 Wi TH WI (Wz . --

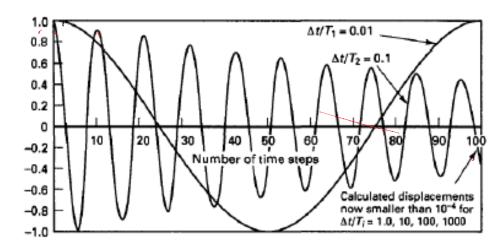
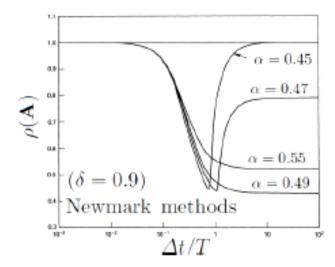


Figure 9.7 Displacement response predicted with increasing $\Delta t/T$ ratio; Wilson θ method, $\theta = 1.4$ [Bathe, 2006]



$$\frac{\left(\delta + \frac{1}{2}\right)^2}{4}$$
best
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wed hol