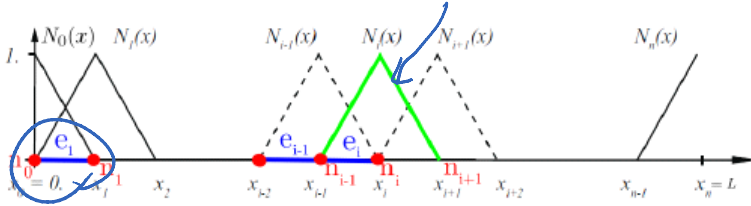


Our approach right now is global or shape function approach

We work with global shape functions $N_i(x)$



X

not directly working with elements

From last time

$$K = \int_{\text{Domain}} B^T D B dV$$

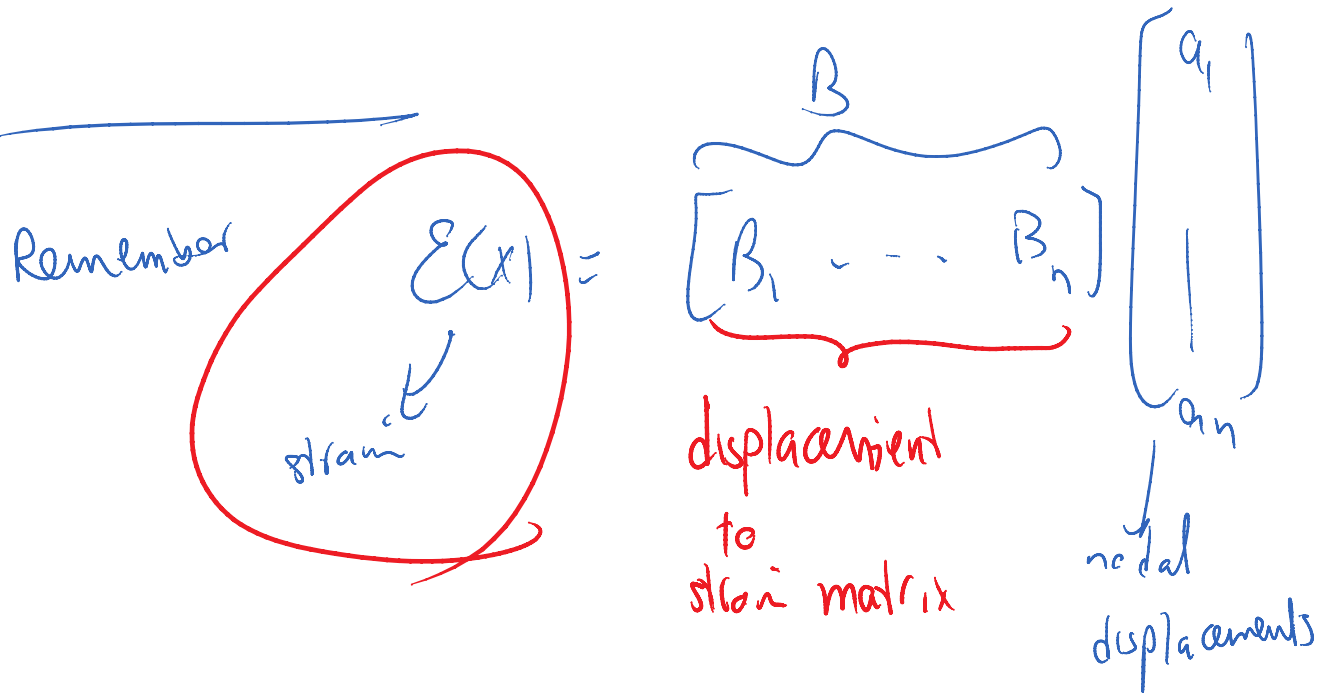
$$D = EA$$

$$B = L_m(N)$$

Solid bar $L_m = \frac{d}{dx}$ B_1 B_n

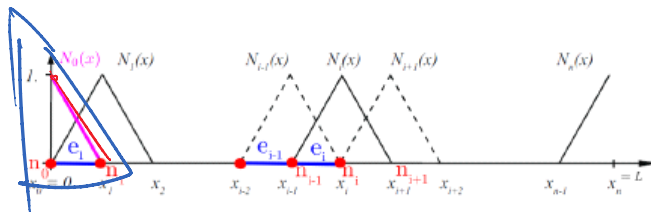
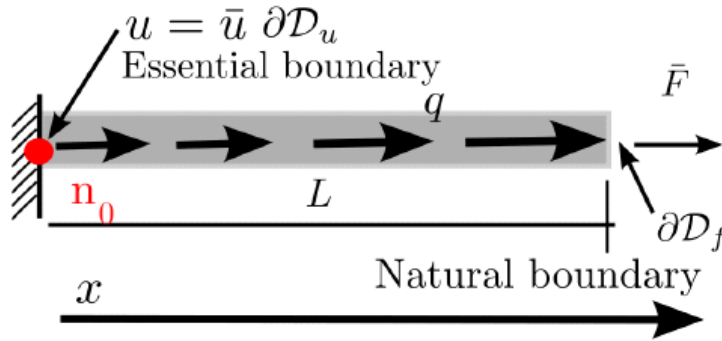
$$B = \frac{d}{dx} [N_1 \dots N_n] = \begin{bmatrix} \textcircled{N_1'} & \dots & N_n' \end{bmatrix}$$

R $[a_1]$



Forces from essential BC, natural BC, and source term (and concentrated forces)

B. Essential Boundary Conditions

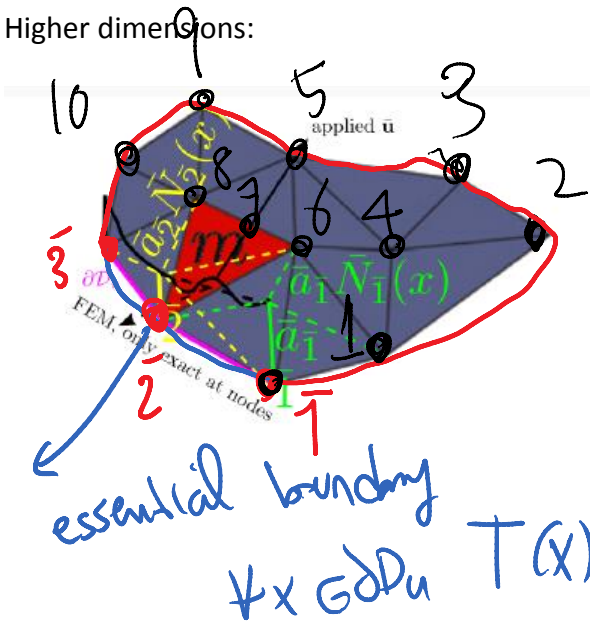


- We let, $\phi_p = \bar{u} N_0 \Rightarrow \phi_p(0) = \phi_p(x_0) = \bar{u} N_0(x_0) = \bar{u} \delta_{11} = \bar{u}$ (307)
- It is clear that for all the trial functions (i.e., shape functions corresponding to unknowns - $I \in \{N_1, \dots, N_{n_f}\}$, $N_I(0) = N_I(x_0) = \delta_{I0} = 0$. That is, trial functions satisfy homogeneous essential boundary condition.

$$\phi_p = \bar{u} N_0$$

$$\phi_p(0) = \bar{u} N_0(x_0) = \bar{u} \cdot 1 = \bar{u}$$

Higher dimensions:



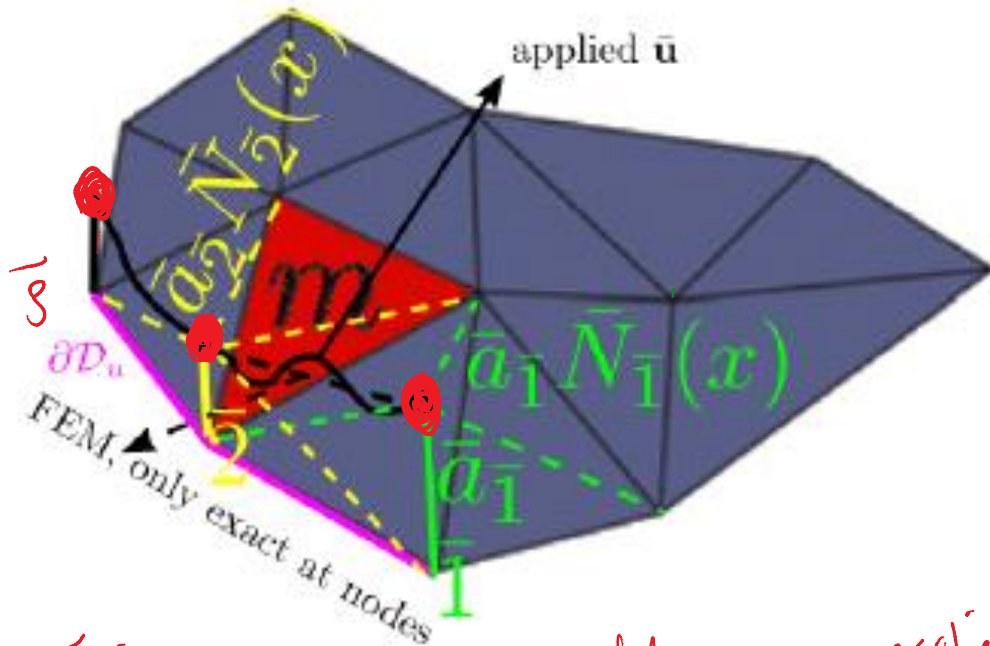
Thermal problem:
at each node has 1 temperature

$$n_f = 10; \text{ free dof's}$$

corresponds to

$$T_1, \dots, T_{10}$$

$$T^h(x) = \sum_{i=1}^{n_f} N_i(\vec{x}) a_i + \phi_p(\vec{x})$$



$$\forall x \in D_u$$

$$\phi_p(x) = \bar{T}(x)$$

in FEM ϕ_p takes prescribed values

ONLY at FE prescribed nodes:

$$N_{\bar{i}}(\bar{x}) = \begin{cases} 1 & \text{at node } \bar{i} \\ 0 & \text{at all the other nodes} \end{cases}$$

$$\phi_p(\vec{x}) = \sum_{\bar{i}=1}^{n_p} a_{\bar{i}} N_{\bar{i}}(\vec{x})$$

of prescribed dofs

#'s with $(\bar{\quad})$ correspond to prescribed dofs

$a_{\bar{i}}$: prescribed value at prescribed node # \bar{i}

$$\phi_p(n_{\bar{j}}) = \sum_{\bar{i}=1}^{n_p} a_{\bar{i}} N_{\bar{i}}(n_{\bar{j}})$$

$$= \delta_{\bar{i}\bar{j}} = \begin{cases} 1 & \bar{i} = \bar{j} \\ 0 & \text{otherwise} \end{cases}$$

$$= \sum_{i=1}^{n_p} a_i \delta_{ij} = a_j$$

becomes \bar{j}

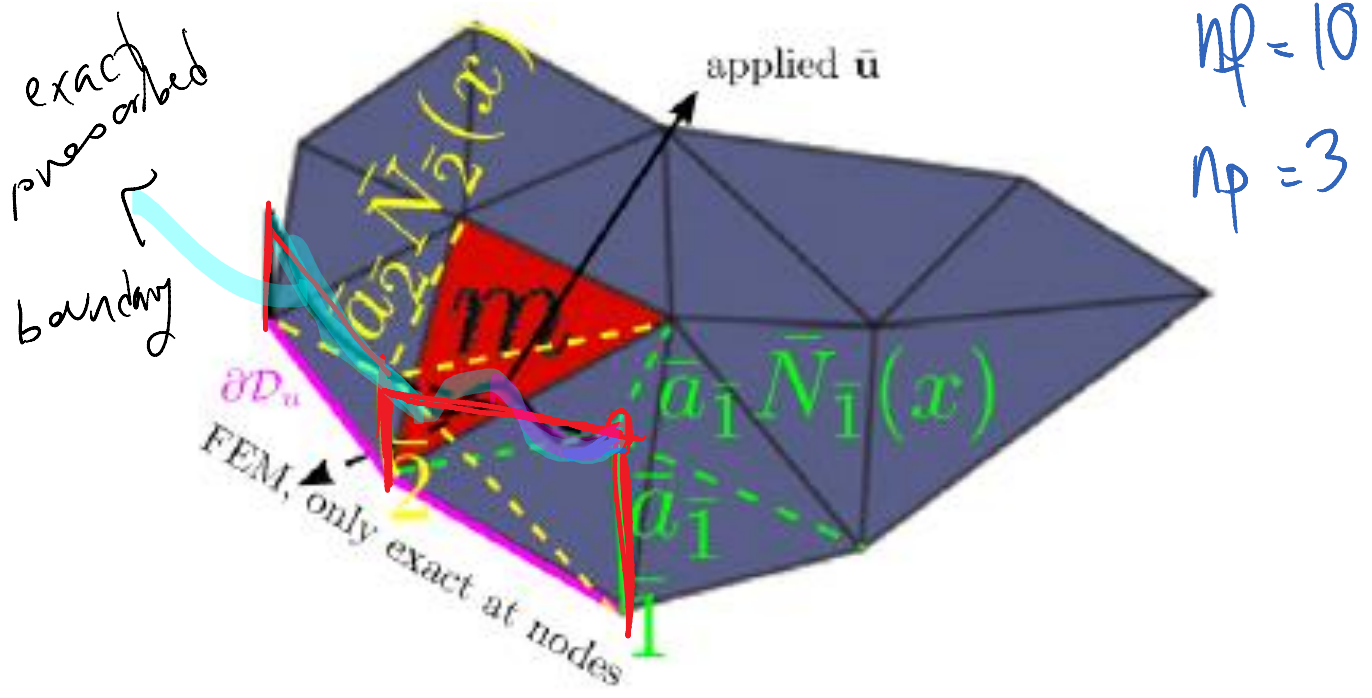
$$= \delta_{i\bar{j}} = \begin{cases} 1 & \text{if } i = \bar{j} \\ 0 & \text{otherwise} \end{cases}$$

$$\boxed{\Phi_p(n_{\bar{j}}) = a_{\bar{j}}}$$

the particular function matches the prescribed BC at **ALL** prescribed

nodes.

- It may not match prescribed values between nodes



Although the essential BC is not satisfied exactly (given that it only matches the prescribed values at FEM nodes) the error induced by this approximation is of the same order of magnitude of FEM discretization error and all the other errors that we will cover ->

This type of error is acceptable!

$$T(\vec{x}) = \sum_{i=1}^{n_f} \underbrace{a_i}_{\substack{\text{shape fun. @ free d.o.f.s} \\ \text{unknowns of the problem}}} N_i(x) + \phi_p(x)$$

n_p

$$\phi_p(x) = \sum_{i=1}^{n_p} a_i N_i(x)$$

prescribed value at prescribed node #i

$$\begin{aligned}
 T^h(x) &= \sum_{i=1}^{n_p} a_i N_i(x) + \sum_{i=1}^{n_p} a_i N_i(x) \\
 &= [N_1 \dots N_{n_p}] \begin{bmatrix} a_1 \\ a_2 \\ \vdots \\ a_{n_p} \end{bmatrix} + [N_1 \dots N_{n_p}] \begin{bmatrix} a_1 \\ \vdots \\ a_{n_p} \end{bmatrix} \\
 &= N a + \underbrace{N \bar{a}}_{\phi_p}
 \end{aligned}$$

Form of

F_D

force from essential BC

no

I=1...np

$$F_D = A(N_I, \Phi_P)$$

force
from
essential
BC

$$= A(N_I, \sum_{j=1}^{n_p} a_{j-} N_{j-}(x))$$

$$= \sum_{j=1}^{n_p} A(N_I, N_{j-}) a_{j-}$$

$$\begin{pmatrix} F_D \end{pmatrix}_{n_f \times 1} = \begin{pmatrix} K \end{pmatrix}_{n_f \times n_p} \bar{a}_{n_p \times 1}$$

$$\begin{matrix} \cancel{K} \\ \end{matrix}_{I \bar{j}} = A(N_I, N_{\bar{j}})$$

I=1...np

free dofs

prescribed

$$J = 1 \dots np$$

free dots

prescribed dots

Remember

was

$$K_{IJ} = A(N_I, N_J)$$

I, J both go from 1 to n_f

Summary:

$$K_a = F$$

$$F = F_r + F_N - \underbrace{F_D}_{\text{essential BC}}$$

$$K_{n_f \times n_f} = A \left(\underbrace{\begin{matrix} N^T \\ n_f \times 1 \end{matrix}} \right) \underbrace{\begin{matrix} N \\ 1 \times n_f \end{matrix}} = \int_V B^T D B \, dV$$

$$F_D = K_{fp} (a_p)_p$$

$$(K_{fp})_{n_f \times n_p} = A \left(\begin{matrix} N^T \\ n_f \times 1 \end{matrix} \right) \underbrace{\begin{matrix} N \\ 1 \times n_p \end{matrix}} = \int_V B^T D \underline{B} \, dV$$

Second force

$$(F_r)_I = \int_0^L \underbrace{N_I(x)}_{\text{shape term}} q \, dx$$

for the bar

for the bar

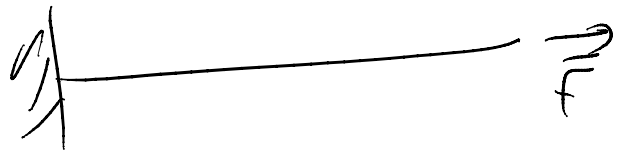
In general

$$F_r = \int_V N^T r dV \quad \text{⊕}$$

general expression for source term force

Force from natural BC

1D bar



Natural
Neumann

$$(F_N)_I = \bar{F} N_I(x=L)$$

shape function

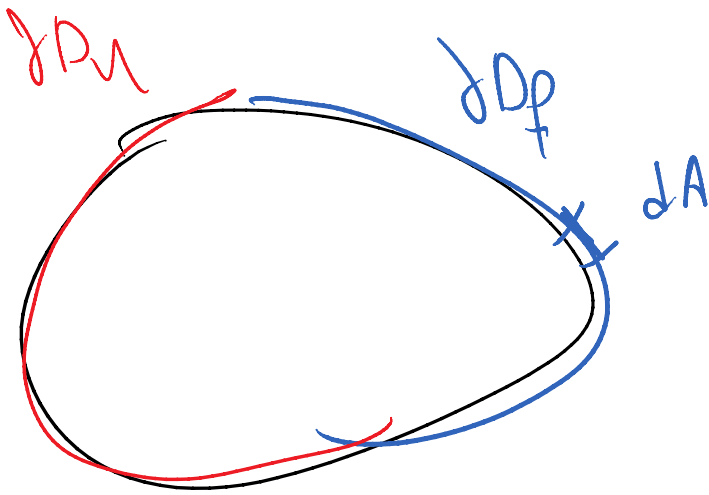
general expression

$$F_N = \int_{\partial \Omega_f} N^T \bar{f} dA$$

letter N

natural

prescribed boundary condition



1D

$$\int_{\delta D_f} N^T \bar{F} dA \quad \text{on boundary} = N^T(x=L) \bar{F}$$

A diagram of a 1D bar element. The left end is fixed to a wall, indicated by a vertical line and a diagonal hatching. The right end is free. A force F is applied at the free end, pointing to the right. The displacement at the free end is labeled $\delta D_f(x=L)$.

$$Kq = F$$

$$F = F_r + F_N - F_D + F_n$$

nodal forces
 ↑
 forces

F_r : source term
 F_N : Neumann potential
 F_D : potential
 F_n : nodal forces

$$K = \int_V B^T D B dV$$

$$= \int_0^L \frac{A}{dx} N^T E A N dx \quad \text{1D bar}$$

$$F_r = \int_V N^T r dV$$

r : body force

$$= \int_0^L N^T q dx$$

q : 1D bar force

Neumann
natural BC

essential BC

$$F_N = \int_{\partial D_f} N^T \bar{f} dA = N^T(x=L) \bar{F}$$

1D bar

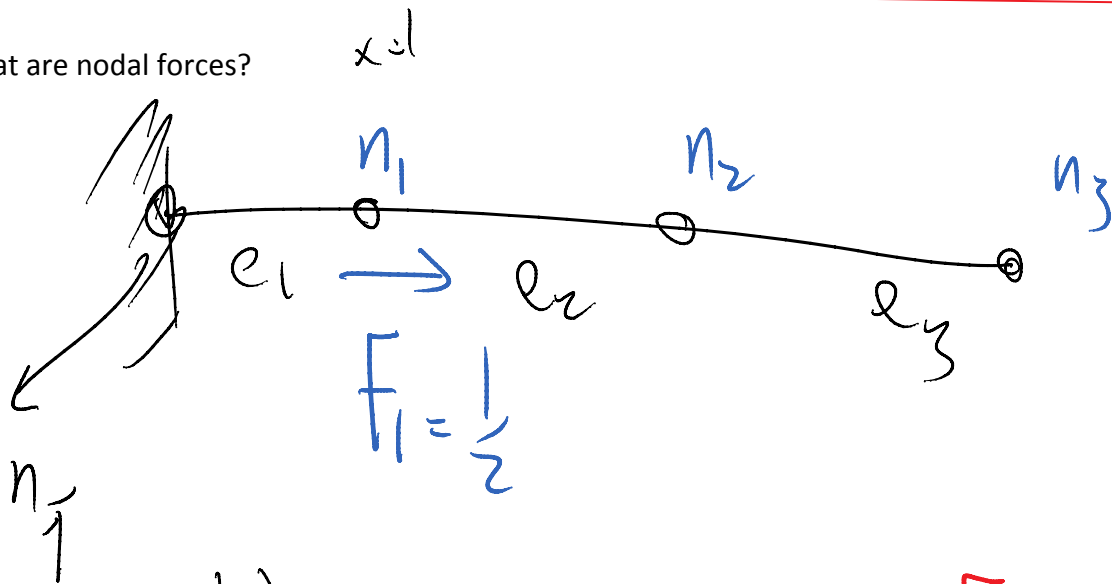
$$F_D = K_{fp} \bar{a}$$

$$K_{fp} = \int_V B^T D B dV =$$

$$\int \left(\frac{dN}{dx} \right) EA \left(\frac{d\bar{N}}{dx} \right) dx$$

1D bar

What are nodal forces?



$$(K)_{3 \times 3} a_{3 \times 1} = F_{r+} + F_N - F_D + F_n$$

3x1 3x1

$$\begin{bmatrix} \frac{1}{2} \\ 0 \\ 0 \end{bmatrix}$$

How do we show it?

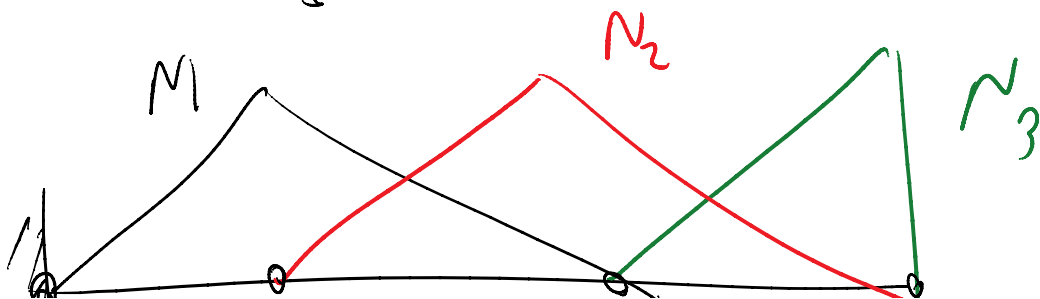
can be treated as a load if a source term in δ function form

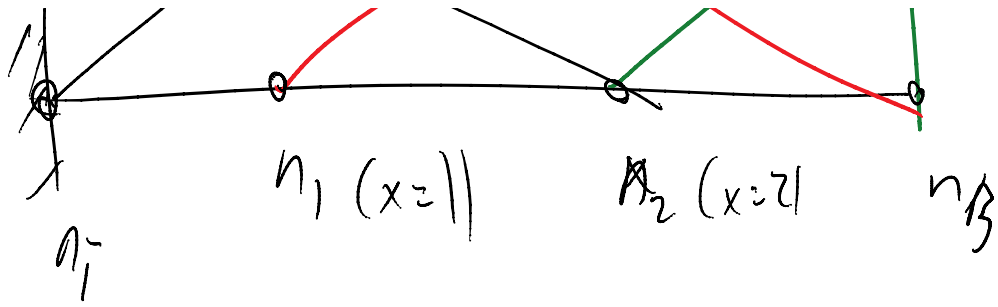
$$q = \delta(x-1) \frac{1}{2}$$

$$(F_r)_I = \int_0^L N_I(x) q \, dx$$

$$= \int_0^L N_I(x) \delta(x-1) \left(\frac{1}{2}\right) dx$$

$$N_I(x=1) \frac{1}{2} = N_I(\text{Node 1}) \frac{1}{2} = \frac{1}{2} \delta_{1I}$$





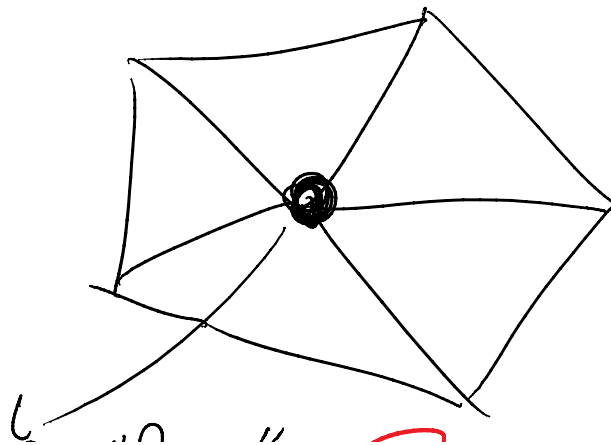
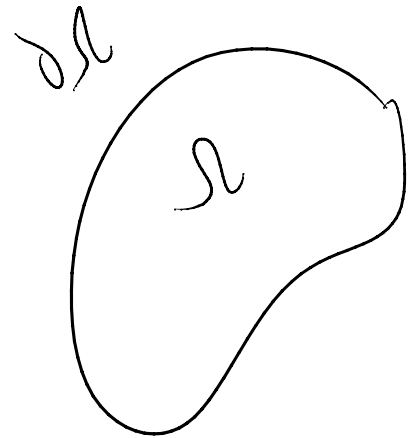
This way you show

$$F_n = \begin{bmatrix} f_1 \\ \vdots \\ f_n \end{bmatrix}$$

Thermal problem balance law

balance of energy

$$\int_{\partial \Omega} q \cdot dS - \int_{\Omega} Q dV = 0$$

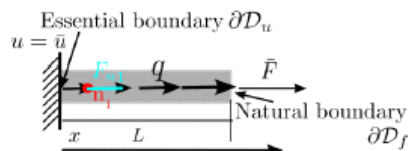


nodal "force" Concentrated version
of Q "point-like
input energy"

Summary: Force vectors

- Force vector is given by:

$$\mathbf{F} = \mathbf{F}_r + \mathbf{F}_N + \mathbf{F}_n - \mathbf{F}_D \quad (311)$$



- \mathbf{F}_r , \mathbf{F}_N , \mathbf{F}_n and \mathbf{F}_D are given by (cf. (301) and (310))

$$\mathbf{F}_r = (\mathbf{N}^T, q)_r = \int_{\mathcal{D}} \mathbf{N}^T q \, dv = \int_0^L \begin{bmatrix} N_1 \\ \vdots \\ N_{n_f} \end{bmatrix} q \, dx \quad (312a)$$

$$\mathbf{F}_N = (\mathbf{N}^T, \bar{F})_N = \int_{\partial \mathcal{D}_f} \mathbf{N}^T \bar{F} \, ds = \left(\begin{bmatrix} N_1 \\ \vdots \\ N_{n_f} \end{bmatrix} \bar{F} \right)_{x=L} \quad (312b)$$

$$\mathbf{F}_D = \mathcal{A}(\mathbf{N}^T, \phi_p) = \int_{\mathcal{D}} \frac{d}{dx} \mathbf{N}^T EA \frac{d}{dx} \phi_p \, dv \quad (312c)$$

$$= \left\{ \int_{\mathcal{D}} \mathbf{B}^T EA \bar{\mathbf{B}} \, dv \right\} \bar{\mathbf{a}} = \left\{ \int_0^L \begin{bmatrix} B_1 \\ \vdots \\ B_{n_f} \end{bmatrix} EA [\bar{B}_1 \quad \dots \quad \bar{B}_{n_p}] \, dx \right\} \begin{bmatrix} \bar{a}_1 \\ \vdots \\ \bar{a}_{n_p} \end{bmatrix} = \mathbf{K}_{ff} \bar{\mathbf{a}}$$

$$\mathbf{F}_n = \begin{bmatrix} F_{n1} \\ \vdots \\ F_{n_{n_f}} \end{bmatrix} \quad (312d)$$

p48 / 456

Force Essential Boundary Condition

- We have used (309) in (312c) to write,

$$\mathbf{F}_D = \mathcal{A}(\mathbf{N}^T, \phi_p) = \mathbf{K}_{fp} \bar{\mathbf{a}} \quad (313)$$

- The prescribed to free stiffness matrix \mathbf{K}_{fp} is an $n_f \times n_p$ matrix given by,

$$\mathbf{K}_{fp} = \int_{\mathcal{D}} \mathbf{B}^T E A \bar{\mathbf{B}} \, dv = \int_0^L \begin{bmatrix} B_1 \\ \vdots \\ B_{n_f} \end{bmatrix} EA [\bar{B}_1 \quad \cdots \quad \bar{B}_{n_p}] \, dx \quad (314)$$

- From (306) we had,

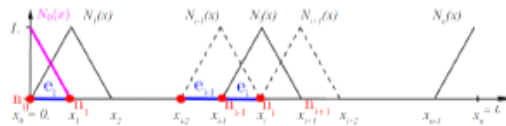
$$\mathbf{K} = \mathcal{A}(\phi^T, \phi) = \int_{\mathcal{D}} \mathbf{B}^T E A \mathbf{B} \, dv = \int_0^L \begin{bmatrix} B_1 \\ B_2 \\ \vdots \\ B_{n_f} \end{bmatrix} EA [B_1 \quad B_2 \quad \cdots \quad B_{n_f}] \, dx$$

where \mathbf{K} was an $n_f \times n_f$ matrix.

- "Prescribed" dofs \bar{i} do not go into \mathbf{K} because their value $\bar{a}_{\bar{i}}$ are already known.
- This is opposite to dofs $I = 1, \dots, n_f$ which correspond to "free" dofs.

Force Essential Boundary Condition

For example for the problem in the figure $n_p = 1$, $\bar{1} = 0$, $\bar{a}_{\bar{1}} = \bar{u} \Rightarrow$



$$\mathbf{F}_D = \bar{a}_{\bar{1}} \int_0^L \begin{bmatrix} B_1 \\ \vdots \\ B_{n_f} \end{bmatrix} EA \bar{B}_{\bar{1}}(x) \, dx = \bar{u} \int_0^L \begin{bmatrix} B_1 \\ \vdots \\ B_{n_f} \end{bmatrix} EA B_0(x) \, dx \quad (315)$$

$$\mathbf{F}_D = \left(\int_0^L \begin{bmatrix} B_1 \\ \vdots \\ B_{n_f} \end{bmatrix} EA \begin{bmatrix} B_{\bar{1}} & B_{\bar{2}} & \cdots & B_{\bar{n}_p} \end{bmatrix} dx \right) \begin{bmatrix} \bar{a}_{\bar{1}} \\ \vdots \\ \bar{a}_{\bar{n}_p} \end{bmatrix}$$

$$F_D = \left(\int_0^L \begin{bmatrix} B_1 \\ | \\ B_{n_f} \end{bmatrix} EA B_T \right) a_T$$

(Ca_{n_f})

$$a_T = \bar{u}$$

WR no boundary conditions
on weight function

Weak form weight function
satisfies homogeneous
essential BC "