Difference between the global and local approaches

Global approach is what we have covered so far

Finite Element Method: Global

Global shape functions:

 $\mathbf{K} = \int_{0}^{2} \begin{bmatrix} B_{1} \\ B_{2} \\ B_{3} \\ B_{4} \end{bmatrix} EA \begin{bmatrix} B_{1} & B_{2} & B_{3} & B_{4} \end{bmatrix} dx = \begin{bmatrix} \int_{0}^{2} B_{1}B_{1} dx & \int_{0}^{2} B_{1}B_{2} dx & \int_{0}^{2} B_{1}B_{3} dx & \int_{0}^{2} B_{1}B_{4} dx \\ & \int_{0}^{2} B_{2}B_{2} dx & \int_{0}^{2} B_{2}B_{3} dx & \int_{0}^{2} B_{2}B_{4} dx \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & \\ & & & & & \\ & & & & & & \\ & & & & \\ & & & & \\ & & & & & \\ & & & & & \\ & & & & \\ & & & & & \\ & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & \\ & & & & & & \\ & & & & & \\ & & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ &$ 

$$= \begin{bmatrix} \int_{e_1} B_1 B_1 dx + \int_{e_2} B_1 B_1 dx & \int_{e_2} B_1 B_2 dx & 0 & 0 \\ & \int_{e_2} B_2 B_2 dx + \int_{e_3} B_2 B_2 dx & \int_{e_3} B_2 B_3 dx & 0 \\ & \int_{e_3} B_3 B_3 dx + \int_{e_4} B_3 B_3 dx & \int_{e_4} B_3 B_4 dx \\ & & \int_{e_4} B_4 B_4 dx \end{bmatrix}$$



All the elements locally look the same

## **ELEMENT DOF MAP**

Map from LOCAL ELEMENT DOFs to GLOBAL DOFs

## **ELEMENT NODAL MAP**

NMAP

Map from LOCAL ELEMENT NODES to GLOBAL NODES



- NMAP is used to create the geometry of the element
- M is used to transfer local to global stiffness matrix and force vector



How the local (element-centered approach works)

Continue with local approach:

$$K = \int_{0}^{2} B^{T} EAB dx = \int_{e_{1}}^{K^{2}} B^{T} EAB dx + \int_{e_{2}}^{K^{2}} B^{T} EAB dx + \int_{e_{3}}^{K^{2}} B^{T} EAB dx + \int_{e_{4}}^{K^{2}} B^{T} EAB dx = (327)$$

$$K = \int_{e_{1}}^{0} \left[ \begin{array}{c} \beta_{1} \\ \beta_{2} \\ \beta_{3} \\ \beta_{4} \end{array} \right] \left[ EA \left[ \beta_{1} \\ \beta_{2} \\ \beta_{3} \\ \beta_{4} \end{array} \right] \left[ EA \left[ \beta_{1} \\ \beta_{2} \\ \beta_{3} \\ \beta_{4} \end{array} \right] \left[ EA \left[ \beta_{1} \\ \beta_{2} \\ \beta_{3} \\ \beta_{4} \right] \right] \left[ A \left[ \beta_{1} \\ \beta_{1} \\ \beta_{2} \\ \beta_{3} \\ \beta_{4} \right] \right] dx$$

$$P_{1} \left[ \begin{array}{c} \beta_{1} \beta_{1} \\ \beta_{2} \\ \beta_{3} \\ \beta_{4} \end{array} \right] \left[ EA \left[ \beta_{1} \\ \beta_{2} \\ \beta_{3} \\ \beta_{4} \right] dx$$

$$P_{1} \left[ \begin{array}{c} \beta_{1} \beta_{1} \\ \beta_{2} \\ \beta_{3} \\ \beta_{4} \end{array} \right] dx$$

$$P_{1} \left[ \begin{array}{c} \beta_{1} \beta_{1} \\ \beta_{2} \\ \beta_{3} \\ \beta_{4} \end{array} \right] dx$$

$$P_{2} \left[ \begin{array}{c} \beta_{1} \beta_{1} \\ \beta_{2} \\ \beta_{3} \\ \beta_{4} \end{array} \right] dx$$

$$P_{2} \left[ \begin{array}{c} \beta_{1} \beta_{1} \\ \beta_{2} \\ \beta_{3} \\ \beta_{4} \end{array} \right] dx$$

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$$P_{2} \left[ \begin{array}{c} \beta_{1} \beta_{1} \\ \beta_{2} \\ \beta_{3} \\ \beta_{4} \end{array} \right] dx$$

$$P_{2} \left[ \begin{array}{c} \beta_{1} \beta_{2} \\ \beta_{3} \\ \beta_{4} \\ \beta_{5} \end{array} \right] dx$$

$$P_{3} \left[ \begin{array}{c} \beta_{1} \beta_{2} \\ \beta_{3} \\ \beta_{4} \end{array} \right] dx$$

$$P_{3} \left[ \begin{array}{c} \beta_{1} \beta_{2} \\ \beta_{3} \\ \beta_{4} \end{array} \right] dx$$

$$P_{3} \left[ \begin{array}{c} \beta_{1} \beta_{2} \\ \beta_{3} \\ \beta_{4} \end{array} \right] dx$$

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$$P_{3} \left[ \begin{array}{c} \beta_{1} \beta_{2} \\ \beta_{2} \end{array} \right] dx$$

$$P_{3} \left[ \begin{array}{c} \beta_{1} \beta_{2} \end{array} \right] dx$$

$$P_$$

$$\begin{split} \mathbf{K} &= \int_{0}^{2} \mathbf{B}^{T} EAB \, \mathrm{d}x = \overbrace{f_{e_{1}} \mathbf{B}^{T} EAB \, \mathrm{d}x}^{\mathbf{K}^{e_{1}}} + \overbrace{f_{e_{2}} \mathbf{B}^{T} EAB \, \mathrm{d}x}^{\mathbf{K}^{e_{2}}} + \overbrace{f_{e_{3}} \mathbf{B}^{T} EAB \, \mathrm{d}x}^{\mathbf{K}^{e_{3}}} + \overbrace{f_{e_{4}} \mathbf{B}^{T} EAB \, \mathrm{d}x}^{\mathbf{K}^{e_{4}}} + \overbrace{f_{e_{4}} \mathbf{B}^{T} EAB \, \mathrm{d}x}^{\mathbf{K}^{e_{4}}} = \\ &= \begin{bmatrix} \int_{e_{1}}^{e_{1}} B_{1} B_{1} \, \mathrm{d}x & 0 & 0 & 0 \\ \mathrm{sym.} & \int_{e_{3}}^{e_{2}} B_{2} B_{2} \, \mathrm{d}x} & \int_{e_{3}}^{e_{2}} B_{2} B_{3} \, \mathrm{d}x} & 0 \\ \mathrm{sym.} & \int_{e_{4}}^{0} B_{3} B_{3} \, \mathrm{d}x} & \int_{e_{4}}^{0} B_{3} B_{4} \, \mathrm{d}x \\ \mathrm{sym.} & \int_{e_{4}}^{0} B_{3} B_{3} \, \mathrm{d}x} & \int_{e_{4}}^{0} B_{3} B_{4} \, \mathrm{d}x \\ \mathrm{sym.} & \int_{e_{4}}^{1} B_{3} B_{3} \, \mathrm{d}x} & \int_{e_{4}}^{0} B_{3} B_{4} \, \mathrm{d}x \\ \mathrm{sym.} & \int_{e_{4}}^{1} B_{3} B_{3} \, \mathrm{d}x} & \int_{e_{4}}^{0} B_{3} B_{4} \, \mathrm{d}x \\ \mathrm{sym.} & \int_{e_{4}}^{1} B_{3} B_{3} \, \mathrm{d}x & \int_{e_{4}}^{1} B_{3} B_{4} \, \mathrm{d}x \\ \mathrm{sym.} & \int_{e_{4}}^{1} B_{3} B_{3} \, \mathrm{d}x & \int_{e_{4}}^{1} B_{3} B_{4} \, \mathrm{d}x \\ \mathrm{sym.} & \int_{e_{4}}^{1} B_{3} B_{3} \, \mathrm{d}x & \int_{e_{4}}^{1} B_{3} B_{4} \, \mathrm{d}x \\ \mathrm{sym.} & \int_{e_{4}}^{1} B_{3} B_{3} \, \mathrm{d}x & \int_{e_{4}}^{1} B_{3} B_{4} \, \mathrm{d}x \\ \mathrm{sym.} & \int_{e_{4}}^{1} B_{3} B_{3} \, \mathrm{d}x & \int_{e_{4}}^{1} B_{3} B_{4} \, \mathrm{d}x \\ \mathrm{sym.} & \int_{e_{4}}^{1} B_{3} B_{3} \, \mathrm{d}x & \int_{e_{4}}^{1} B_{3} B_{4} \, \mathrm{d}x \\ \mathrm{sym.} & \int_{e_{4}}^{1} B_{3} B_{3} \, \mathrm{d}x & \int_{e_{4}}^{1} B_{3} B_{4} \, \mathrm{d}x \\ \mathrm{sym.} & \int_{e_{4}}^{1} B_{3} B_{3} \, \mathrm{d}x & \int_{e_{4}}^{1} B_{3} B_{4} \, \mathrm{d}x \\ \mathrm{sym.} & \int_{e_{4}}^{1} (-2) (-2) \, 0 \, 0 \, 0 \\ \mathrm{sym.} & \int_{e_{4}}^{1} (-2) (-2) \, 0 \, 0 \, 0 \\ \mathrm{sym.} & \int_{e_{4}}^{1} B_{3} B_{3} \, \mathrm{d}x \\ \mathrm{sym.} & \int_{e_{4}}^{1} (-2) (-2) \, (-2) \, \frac{1}{2} (-2) (-2) \, \frac{1}{2} (-$$

$$\mathbf{K}^{e_{1}} = \begin{bmatrix} 2 & 0 & 0 & 0 \\ 0 & 0 & 0 \\ \text{sym.} & 0 & 0 \\ 0 & 2 & -2 & 0 \\ \text{sym.} & 2 & 0 \\ \text{sym.} & 2 & 0 \\ 0 \end{bmatrix} \qquad \mathbf{K}^{e_{3}} = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 2 & -2 & 0 \\ \text{sym.} & 2 & 0 \\ 0 \end{bmatrix} \qquad \mathbf{K}^{e_{4}} = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ \text{sym.} & 2 & -2 \\ 2 \end{bmatrix}$$
$$\mathbf{K} = \mathbf{K}^{e_{1}} + \mathbf{K}^{e_{2}} + \mathbf{K}^{e_{3}} + \mathbf{K}^{e_{4}} \Rightarrow \qquad \mathbf{K}^{e_{4}} = \begin{bmatrix} 4 & -2 & 0 & 0 \\ 4 & -2 & 0 \\ \text{sym.} & 4 & -2 \\ 2 \end{bmatrix}$$



$$E = \begin{bmatrix} x \\ -1 \end{bmatrix} E A \begin{bmatrix} x \\ z \end{bmatrix} dx$$

$$E A \begin{bmatrix} x \\ z \end{bmatrix} dx$$

$$E A \begin{bmatrix} 1 \\ -1 \end{bmatrix} (\begin{bmatrix} 1 \\ dx \end{bmatrix})$$

$$E A \begin{bmatrix} 1 \\ -1 \end{bmatrix} (\begin{bmatrix} 1 \\ dx \end{bmatrix})$$

$$E X = \begin{bmatrix} A \\ -1 \end{bmatrix} \begin{bmatrix} 1 \\ -1 \end{bmatrix} \begin{bmatrix} -1 \\ -1 \end{bmatrix}$$

$$2x = \begin{bmatrix} 2 \\ 1 \\ -1 \end{bmatrix}$$

$$2x = \begin{bmatrix} 1 \\ -1 \end{bmatrix}$$

$$2x = \begin{bmatrix} 1 \\ -1 \end{bmatrix}$$

$$x = \begin{bmatrix} 1 \\ -1 \end{bmatrix}$$

$$x = \begin{bmatrix} 1 \\ -1 \end{bmatrix}$$

$$K^{e_{1}} = \begin{bmatrix} 2 & 0 & 0 & 0 \\ ymn & 0 & 0$$

$$\mathbf{K}^{e_{1}} = \begin{bmatrix} 2 & 0 & 0 & 0 \\ 0 & 0 & 0 \\ \text{sym.} & 0 & 0 \\ 0 \end{bmatrix} \qquad \mathbf{K}^{e_{2}} = \begin{bmatrix} 2 & -2 & 0 & 0 \\ 0 & 2 & -2 & 0 \\ \text{sym.} & 2 & 0 \\ \text{sym.} & 2 & 0 \\ 0 \end{bmatrix} \qquad \mathbf{K}^{e_{3}} \qquad \mathbf{K}^{e_{4}} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ \text{sym.} & 2 & -2 \\ 2 & 2 \end{bmatrix} \qquad \mathbf{K} = \mathbf{K}^{e_{1}} + \mathbf{K}^{e_{2}} + \mathbf{K}^{e_{3}} + \mathbf{K}^{e_{4}} \Rightarrow \qquad \mathbf{K}^{e_{4}} = \begin{bmatrix} 4 & -2 & 0 & 0 \\ 0 & 4 & -2 & 0 \\ \text{sym.} & 4 & -2 \\ 2 & 2 \end{bmatrix}$$



Element 2





Same with the other elements



Using element nodal dof maps to assemble Example from class on 2016/09/20





Comparison of local and global stiffness matrices and force vectors

## Weak statement for finite element formulation

• Similar to our development for solid bar, stiffness matrix can be expressed as,

$$\mathbf{K} = \int_{D} \mathbf{B}^{\mathrm{T}} \mathbf{D} \mathbf{B} \, \mathrm{d} \mathbf{v} \tag{341}$$

• Recalling (312) forces are given by:

$$\mathbf{F}_{r} = \left(\mathbf{N}^{\mathrm{T}}, r\right)_{r} = \int_{\mathcal{D}} \mathbf{N}^{\mathrm{T}} r \, \mathrm{d} \mathbf{v} \quad \text{source term force}$$
(342a)

$$\mathbf{F}_{N} = \left(\mathbf{N}^{\mathrm{T}}, \bar{\mathbf{F}}\right)_{N} = \int_{\partial \mathcal{D}_{f}} \mathbf{N}^{\mathrm{T}} \bar{\mathbf{F}}.\mathbf{N} \, \mathrm{ds} \quad \text{essential BC force}$$
(342b)

$$\mathbf{F}_{D} = \mathcal{A}\left(\mathbf{N}^{\mathrm{T}}, \phi_{p}\right) = \int_{\mathcal{D}} L_{m}(\mathbf{N})^{\mathrm{T}} \mathbf{D} L_{m}(\phi_{p}) \,\mathrm{d}\mathbf{v} = \left\{\int_{\mathcal{D}} \mathbf{B}^{\mathrm{T}} \mathbf{D} \bar{\mathbf{B}} \,\mathrm{d}\mathbf{v}\right\} \bar{\mathbf{a}}$$
$$= \mathbf{K}_{fp} \bar{\mathbf{a}} \quad \text{essential BC force} \tag{342c}$$

$$= \mathbf{K}_{fp} \mathbf{a} \quad \text{essential BC force} \tag{342}$$

$$\begin{bmatrix} F_{n,1} \end{bmatrix}$$

$$\mathbf{F}_{n} = \begin{bmatrix} I_{n1} \\ \vdots \\ F_{nn_{\mathrm{f}}} \end{bmatrix} \quad \text{nodal forces} \tag{342d}$$

and the total force is given by (cf. (311)):

$$\mathbf{F} = \mathbf{F}_r + \mathbf{F}_N + \mathbf{F}_n - \mathbf{F}_D \tag{343}$$

Next, we related element-level stiffness and force to global ones.

lord level  

$$k^{2} : \int_{e} B^{eT} DB^{e} dV$$
  
 $k^{2} : \int_{e} B^{eT} DB^{e} dV$   
 $k^{2} : \int_{e} N^{e} r dV$   
 $k^{r} : \int_{e} N^{e} r dV$   
 $k^{r} : \int_{e} N^{e} r dV$ 







global system?

