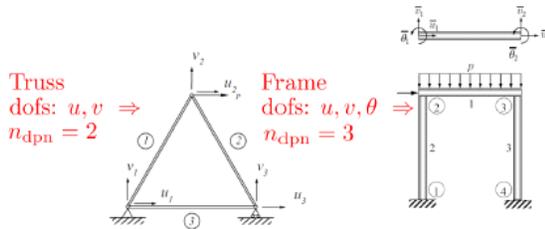


Steps 8 and 9 set element dofMap (8) element dofs edofs (vector of unknowns, done in step 9)
Simplified pseudo-codes

Step 8: Element dof maps M_t^e : Simplified limited case



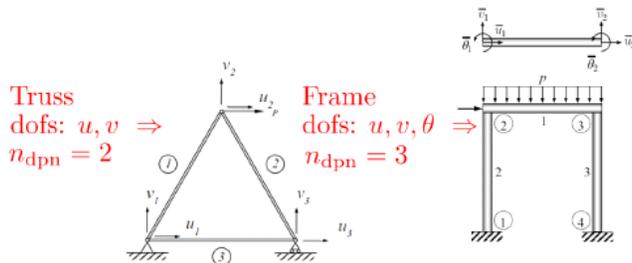
```

A simplified pseudo code looks like: ec dof = 1 dof counter for element
for en = 1: neNodes number of element nodes
  gn = LEM(en) global node number for element node en
  for endof = 1: ndofpn This number is fixed now, e.g., 2 for 2D trusses
    dofMap(ec dof) = node(gn).dof(endof).pos
    gndof = endof, we bypass some steps here
    ec dof = ec dof + 1 increment counter
  end
end
end
    
```

- Two major simplifications are:
 - number of dof per node is fixed for all nodes.
 - $gndof = endof$: That is dof number endof of node en of element is the same dof in its corresponding global node. For example U_1 in trusses is always 1st dof for element nodes and 1st for global nodes as well.

420 / 456

Step 9: Set element dofs a^e : Simplified limited case

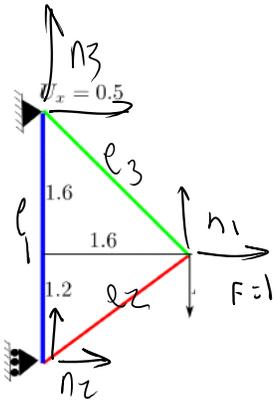


- Similar to steps 1, 2, and 8, step 9 can be greatly simplified if we assume all nodes share exactly the same set of dofs.
- Noting n_{dofpn} (ndofpn) = Number of dof. per node, simplified merged steps 8 & 9 are:

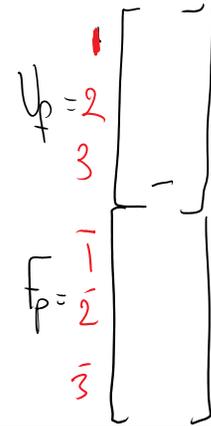

```

dofs = zeros(nedof) element dofs (edof) resized to number of element dofs and zeroed
ec dof = 1 dof counter for element
for en = 1: neNodes number of element nodes
  gn = LEM(en) global node number for element node en
  for endof = 1: ndofpn This number is fixed now, e.g., 2 for 2D trusses
    if (node(gn).dof(endof).p == true) gndof = endof, we bypass some steps here
      dofs(ec dof) = node(gn).dof(endof).value; e dof val = corresponding global val
    end
    dofMap(ec dof) = node(gn).dof(endof).pos
    ec dof = ec dof + 1 increment counter
  end
end
end
            
```

422 / 456



node	p	pos	v	f
1	false	1	?	0
	false	2	?	-1
2	true	1	0	
	false	3	?	0
3	true	5	.5	
	true	3	0	

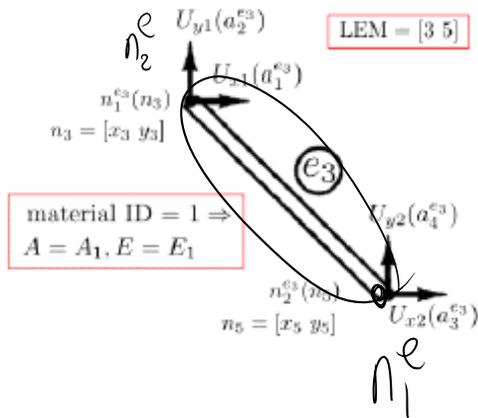


e	LEM	doF Map	doFs
1	[2, 3]	[1 3 2 5]	[0 ? .5]
2	[2, 1]	[1 3 1 2]	[0]
3	[3, 1]	[2 3 1 2]	[.5]

Step 10: Computing element stiffness matrix

Three things needed:

1. Element type
2. Element connectivity (what nodes form the element)
3. Material and section properties



$$K^e = \begin{bmatrix} k_{xx}^b & -k^b \\ -k^b & k^b \end{bmatrix}$$

$$k^b = \left(\frac{AE}{L}\right)^p \begin{bmatrix} c^2 & cs \\ cs & s^2 \end{bmatrix}$$

Geometry aspects

$$1. L = \sqrt{\Delta x^2 + \Delta y^2}$$

$$\Delta x = x_{n2} - x_{n1}$$

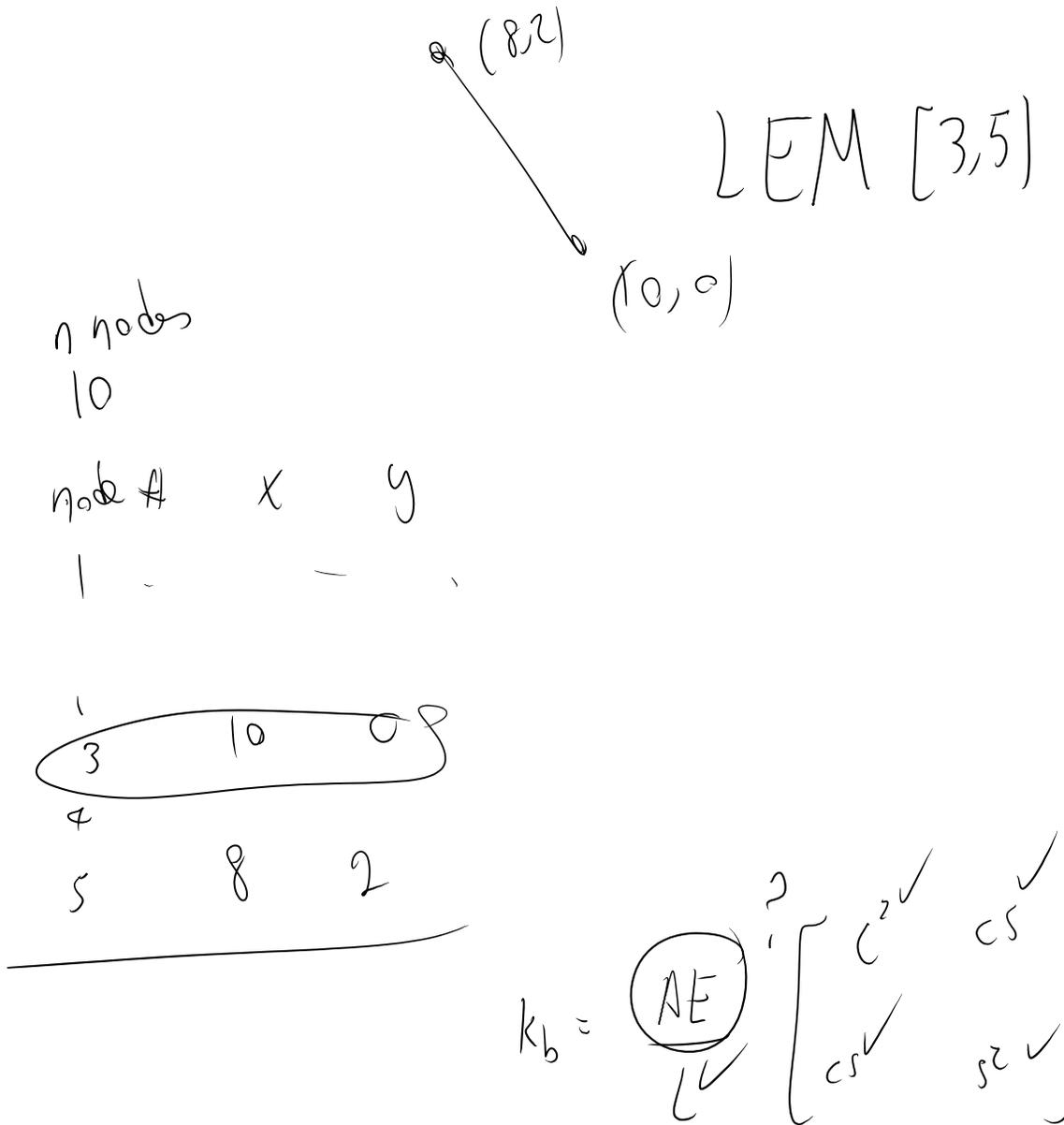
$$\Delta y = y_{n2} - y_{n1}$$

$$2. c = \frac{\Delta x}{L}$$

$$3. s = \frac{\Delta y}{L}$$

We don't store element node coordinates in it (either in element class or in the text file) because:

1. No need to store repeated geometry information of the same node in the global system.
2. What if we change the coordinate of a node (for example sensitivity analysis)



Again for material (E) and section (A) properties, we specify element material section number and read those later in the file.

Example

Input file format

dim 2

element type 3 → Truss element

```

dim 2
ndofpbn 2
Nodes
nNodes 3
id crd
1 0 0
2 2 0
3 1 1
Elements
ne 3
ie element type matID neNodes eNodes
1 3 1 2 1 3
2 3 2 2 3 2
3 3 1 2 1 2
PrescribedDOF
np 3
node dof_index value
1 1 0.01
1 2 0
2 2 0
FreeDOFs
nNonZeroForceDOFs 1
node dof_index value
3 1 2.5
Materials
nMat 2
id numPara Paras
1 2 100 1
2 2 200 2

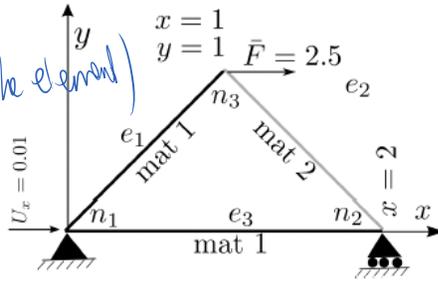
```

element type 3 → Truss element

node coordinates

LEM (nodes of the element)

material section #'s



$$E_1 = 100, A_1 = 1$$

$$E_2 = 200, A_2 = 2$$

A's

material block
E's

Function for calculating stiffness matrix

Approach 1: Matlab (non-object oriented), Fortran, ...

Function:

ComputeStiffness(type, ...)

```

{
  If (type == 0) // bar
  {
    }
  Else if (type == 1)
  {
    }
  ...
}

```

$$k = \frac{AE}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

Object-oriented design:

We have a general element class

```

class PhyElement
{

// Step 10: Compute element stiffness/force (ke, foe (fre: source term; fNe:
Neumann BC))
virtual void Calculate_ElementStiffness_Force() = 0;
};

```

each element provides its own implementation

Now for a bar element, we need to say a bar element **is** an element!

```

class PhyElementBar : public PhyElement
{

virtual void Calculate_ElementStiffness_Force();

}

```

it's a subclass

....
The function implementation is provided in a separate file for the bar element:

```

void PhyElementBar::Calculate_ElementStiffness_Force()
{
// compute stiffness matrix:
ke.resize(2, 2);
double factor = A * E / L;
ke(0, 0) = ke(1, 1) = factor;
ke(1, 0) = ke(0, 1) = -factor;
}

```

If you want to learn how these elements are created, watch the C++ pre-recorded session and the notation of factory

FYI:

Element forces:

$$f^e = f_r^e + f_N^e - \frac{f_D^e}{k_a}$$

Source term Neumann

physics specific

$$\frac{k^e}{k_a}$$

always the same formula

general

sum of all the other forces

$$f_o^e$$

- element specific
- becomes virtual function in O.O. programming

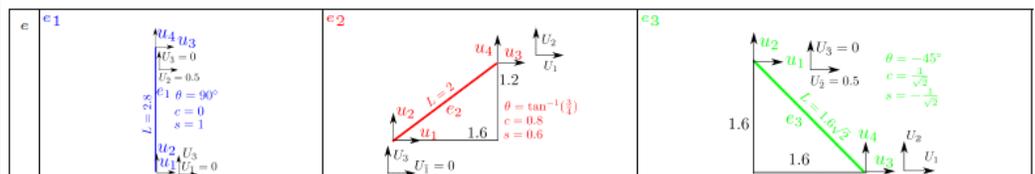
So the virtual function we discussed:

1. Calculates ke
2. Calculates feo

virtual void Calculate_ElementStiffness_Force();

Step 11: the assembly of the global K and F:

Truss example: Assembly of global system



$L=2.8$ $\theta = 90^\circ$ $c=0$ $s=1$ u_2, u_3 $u_1, u_4 = 0$		$L=1.6\sqrt{2}$ $\theta = 45^\circ$ $c = \frac{1}{\sqrt{2}}$ $s = \frac{1}{\sqrt{2}}$ u_1, u_2 u_3, u_4
$k^{e1} = \frac{(1)(1)}{2.8} \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & -1 \\ 0 & 0 & 0 & 0 \\ 0 & -1 & 0 & 1 \end{bmatrix}$ $\begin{bmatrix} \bar{1} & \bar{3} & \bar{2} & \bar{3} \\ 0 & 0 & 0 & 0 \\ 0 & 0.3571 & 0 & -0.3571 \\ 0 & 0 & 0 & 0 \\ 0 & -0.3571 & 0 & 0.3571 \end{bmatrix}$	$k^{e2} = \frac{(1)(1)}{2} \begin{bmatrix} 0.64 & 0.48 & -0.64 & -0.48 \\ 0.48 & 0.36 & -0.48 & -0.36 \\ -0.64 & -0.48 & 0.64 & 0.48 \\ -0.48 & -0.36 & 0.48 & 0.36 \end{bmatrix}$ $\begin{bmatrix} \bar{1} & \bar{3} & \bar{1} & \bar{2} \\ 0 & 0.32 & 0.24 & -0.32 & -0.24 \\ 0 & 0.24 & 0.18 & -0.24 & -0.18 \\ 0 & -0.32 & -0.24 & 0.32 & 0.24 \\ 0 & -0.24 & -0.18 & 0.24 & 0.18 \end{bmatrix}$	$k^{e3} = \frac{(1)(1)}{1.6\sqrt{2}} \begin{bmatrix} 0.5 & -0.5 & -0.5 & 0.5 \\ -0.5 & 0.5 & 0.5 & -0.5 \\ 0.5 & -0.5 & 0.5 & -0.5 \\ 0.5 & -0.5 & -0.5 & 0.5 \end{bmatrix}$ $\begin{bmatrix} \bar{2} & \bar{3} & \bar{1} & \bar{2} \\ 0 & 0.221 & -0.221 & -0.221 & 0.221 \\ 0 & -0.221 & 0.221 & 0.221 & -0.221 \\ 0 & -0.221 & 0.221 & 0.221 & -0.221 \\ 0 & 0.221 & -0.221 & -0.221 & 0.221 \end{bmatrix}$
$f_D^{e1} k^{e1} a_1^e = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0.3571 & 0 & -0.3571 \\ 0 & 0 & 0 & 0 \\ 0 & -0.3571 & 0 & 0.3571 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$	$f_D^{e2} a_2^e = \begin{bmatrix} 0.32 & 0.24 & -0.32 & -0.24 \\ 0.24 & 0.18 & -0.24 & -0.18 \\ -0.32 & -0.24 & 0.32 & 0.24 \\ -0.24 & -0.18 & 0.24 & 0.18 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$	$f_D^{e3} a_3^e = \begin{bmatrix} 0.221 & -0.221 & -0.221 & 0.221 \\ -0.221 & 0.221 & 0.221 & -0.221 \\ -0.221 & 0.221 & 0.221 & -0.221 \\ 0.221 & -0.221 & -0.221 & 0.221 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$
$f_c^{e1} = f_r^{e1} + f_N^{e1} - f_D^{e1} = \begin{bmatrix} 1 & 0 \\ 3 & 0 \\ 3 & 0 \\ 2 & 0 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$	$f_c^{e2} = f_r^{e2} + f_N^{e2} - f_D^{e2} = \begin{bmatrix} 1 & 0 \\ 3 & 0 \\ 3 & 0 \\ 2 & 0 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$	$f_c^{e3} = f_r^{e3} + f_N^{e3} - f_D^{e3} = \begin{bmatrix} 2 & -0.1105 \\ 3 & 0.1105 \\ 3 & 0.1105 \\ 2 & -0.1105 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$

p. rows used (assembly)

free columns $K_{(i,j)} = k^{(s)}$

p. columns used in calculating p^e $p^e = K a^e$

$$K = \begin{bmatrix} 0.32+0.221 & 0.24-0.221 & -0.24 & -0.24 \\ 0.24-0.221 & 0.18+0.221 & -0.18 & -0.18 \\ -0.24 & -0.18 & 0.3571+0.18 & 0 \end{bmatrix} = \begin{bmatrix} 0.5410 & 0.019 & -0.24 \\ 0.019 & 0.401 & -0.18 \\ -0.24 & -0.18 & 0.5371 \end{bmatrix}$$

$$F = F_N + F_e = \begin{bmatrix} 0 \\ -1 \\ 0 \end{bmatrix} + \begin{bmatrix} 0.1105 \\ -0.1105 \\ 0 \end{bmatrix} = \begin{bmatrix} 0.1105 \\ -1.1105 \\ 0 \end{bmatrix} \Rightarrow U = K^{-1}F = \begin{bmatrix} U_1 \\ U_2 \\ U_3 \end{bmatrix} = \begin{bmatrix} -0.2123 \\ -3.2980 \\ -1.200 \end{bmatrix}$$

initiated by free of forces

for e_3 dofMap = $\begin{bmatrix} \bar{2} & \bar{3} & \bar{1} & \bar{2} \end{bmatrix}$

for $i = 1$: number Element dof (4)

$I = \text{dofMap}(i)$ ($i=1, I=\bar{2}$)

if $I < 0$ presented

continue

end

$F(I) + = f^e(i)$ assembly of force

for $j = 1$: element # of dof (4)

$J = \text{dofMap}(j)$

if $J < 0$

continue

end

1) 1 T I) U/T The first

$$K(I, J) = K(I, J) + k^e(i, j);$$

end

end

```

for e = 1:ne loop over elements
  fee = feo element total force = element all forces except essential force
  for i = 1:nedof loop over rows of ke; nedof = element # dof
    I = dofMap(i) local to global dof map  $M_t^e$ 
    if (I > 0) I corresponds to a free dof, we skip prescribed dofs
      for j = 1:nedof loop over columns of ke
        J = dofMap(j) global dof corresponding to j
        if (J > 0) now both I and J are free and can add ke(i,j) to global K
          K(I, J) = K(I, J) + ke(i, j)
        else J < 0, prescribed dof j; add contributions of  $f_D^e = k^e a^e$  to  $f_e^e$ 
          fee(i) = fee(i) - ke(i, j) * edofs(j) edofs: element dofs =  $a^e$ 
        end
      end
    end
    F(I) = F(I) + fee(i) element's total force fee component i'th is computed → added to F(I)
  end
end
end
end

```

431 / 456

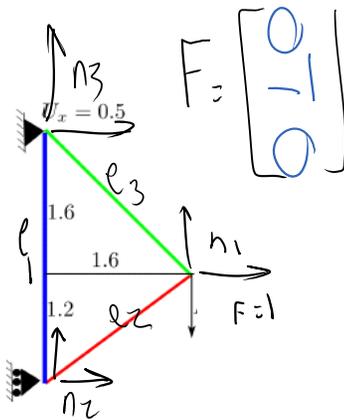
Step 12: Solve global (free) dof a from $Ka = F$

- Two major computational costs during FEM solve are:
 - Assembly:** Refers to: all node, element, and dof set up; computation of local ke and fee; assembly of those to global system. This step **scales linearly versus n_e (ne)**
 - Linear algebra solution: $Ka = F$:** We solve for unknown a. Although conceptually simple, this step is a **major source of computational cost**. It **scales higher than linear versus n_e** ⇒ As the problem size increases this term becomes more dominant.
- Solution of $Ka = F$:
 - WE DO NOT OBTAIN a from $a = K^{-1}F$: **We do not invert K.**
 - We only solve the problem for the specific RHS of F.
 - In Comparison K^{-1} corresponds to the solution of $Ka = F$ for n_f RHS of $F = e_i, i = 1, \dots, n_f$ where n_f is the number of rows (and columns) of K.
 - We employ methods such as LU factorization that computationally only solve the problem for the given RHS F.
 - We take advantage of the structure of stiffness matrix: **symmetry, bandedness, sparsity** in choosing the right solution technique.
 - order of free dofs affects band of the matrix** → various algorithms reorder free dofs such that the matrix band get smaller and the solution cost is optimized.
 - In your term projects you can simply employ simply compute

433 / 456

At this stage for the truss example we have:

Tuesday, November 07, 2017
7:52 AM



node	p	pos	v	f
1	false	1	.	0
	false	2	.	-1
2	true	1	0	.
	false	3	.	0
3	true	2	.5	.
	true	3	0	.

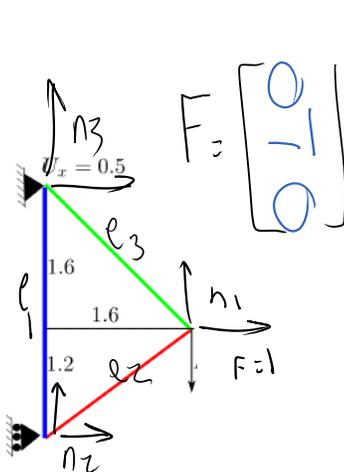
$$\begin{aligned}
 & \begin{matrix} \uparrow \\ \downarrow \\ \leftarrow \end{matrix} \begin{matrix} 1 \\ 2 \\ 3 \end{matrix} \\
 & \begin{matrix} \uparrow \\ \downarrow \\ \leftarrow \end{matrix} \begin{matrix} 1 \\ 2 \\ 3 \end{matrix}
 \end{aligned}$$

e	LEM	doF Map	dofs
1	[2, 3]	[1 3 2 3]	[.5]
2	[2, 1]	[1 3 1 2]	[0]
3	[3, 1]	[2 3 1 2]	[.5]

Solution is done:

FEM postprocessing:

Tuesday, November 07, 2017



node unknowns: vs of free d.o.f & f's of pres. d.o.f

node	p	pos	v	f
1	false	1	?	0
	false	2	.	-1
2	true	1	0	?
	false	3	.	0
3	true	2	.5	.
	true	3	0	.

$$\begin{aligned}
 & \begin{matrix} \uparrow \\ \downarrow \\ \leftarrow \end{matrix} \begin{matrix} 1 \\ 2 \\ 3 \end{matrix} \\
 & \begin{matrix} \uparrow \\ \downarrow \\ \leftarrow \end{matrix} \begin{matrix} 1 \\ 2 \\ 3 \end{matrix}
 \end{aligned}$$

e	LEM	doF Map	dofs	fe
1	[2, 3]	[1 3 2 3]	[0 ? .5 0]	?
2	[2, 1]	[1 3 1 2]	[0]	
3	[3, 1]	[2 3 1 2]	[.5]	

We fine:

Nodes:

- Free dofs -> value
- Prescribed dofs -> forces

Elements:

- Dofs (element values): only the free dofs are unknowns at this stage.
- Element forces

Global Level:

- Support forces F_p

Step 13: Assign a to nodes and elements

```

for n = 1:nNodes
  for dofi = 1: node(n).nndof num dof for node (n)
    if node(n).ndof(dofi).p == false free dof
      posn = node(n).ndof(dofi).pos position of dof in global free F
      node(n).ndof(dofi).v = dofs(posn) set free dof val to corresponding val in global dofs (a)
    end
  end
end
end
  
```

435 / 456

Step 13a filled in the tables below:

node unknowns: v's of free dofs & f's of pres. dofs

node	p	pos	v	f
1	false	1	-2.123	0
	false	2	-3.29	-1
2	true	1	0	?
	false	3	-1.2	0
3	true	2	.5	
	true	3	0	

Handwritten notes on the right show force vectors: $F_p = \begin{bmatrix} 2 \\ 3 \end{bmatrix}$ and $F = \begin{bmatrix} 2.123 \\ -3.29 \\ -1.2 \end{bmatrix}$.

e	LEM	dof Map	dofs	fe
1	[2, 3]	[1 3 2 3]	[0 ? 0.5 0]	?
2	[2, 1]	[1 3 1 2]	[0]	
3	[3, 1]	[2 3 1 2]	[.5]	

Please **write** these in your notes and leave several lines blank below it

Step 13b: filling the element dof unknowns

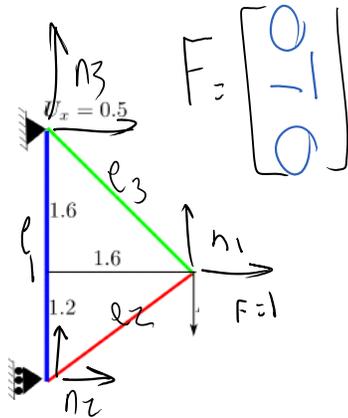
```

for e = 1:ne loop over elements
  for i = element(e).nedof loop over element dofs; nedof = # dof (n_dof^e)
    posn = element(e).dofMap(i) corresponding global position using dofMat (M_i^e)
    if (posn > 0) free dof
      element(e).edofs(i) = dofs(posn)
      set free element dof a^e to corresponding val in global dofs (a)
    end
  end
end
end

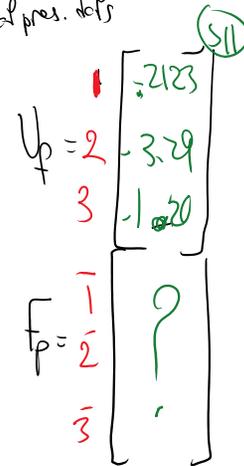
```

436 / 456

node unknowns: vs of free dofs & fs of pres. dofs



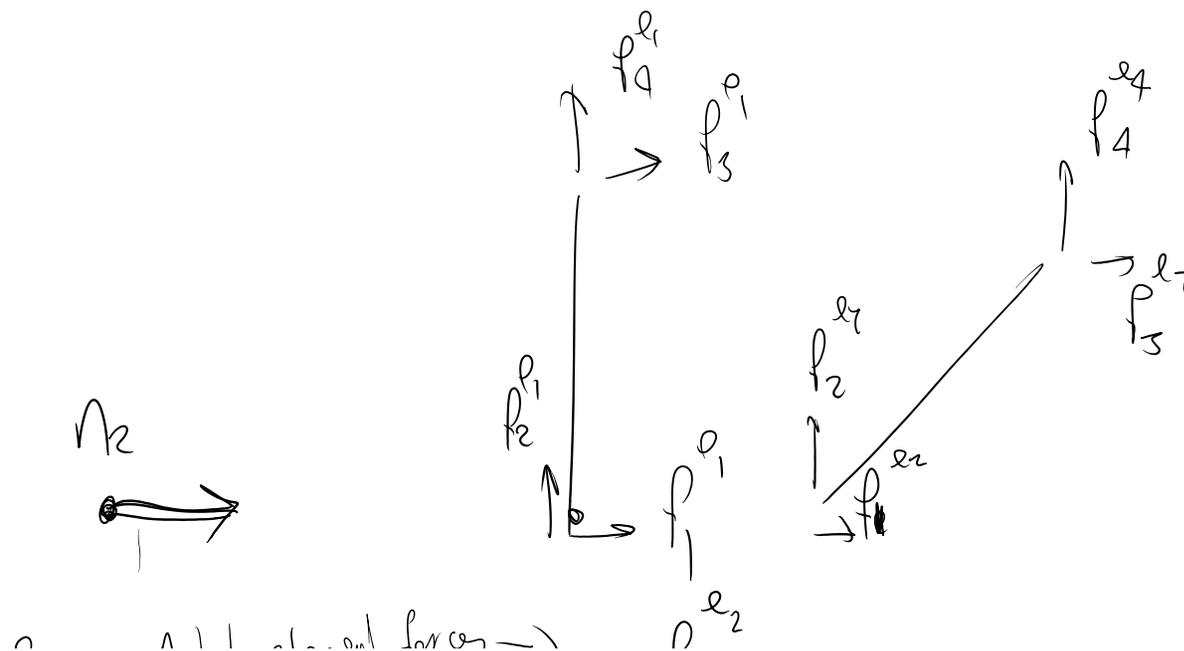
node	p	pos	v	f
1	false	1	-2.123	0
	false	2	-3.29	-1
2	true	1	0	?
	false	3	-1.2	0
3	true	2	.5	
	true	3	0	



e	LEM	dofMap	dofs	fe
1	[2, 3]	[1 3 2 3]	[0 0 -1.2 0.5 0]	?
2	[2, 1]	[1 3 1 2]	[0]	
3	[3, 1]	[2 3 1 2]	[.5 0]	

For support forces we need to do in two steps:

Step a: Compute element forces



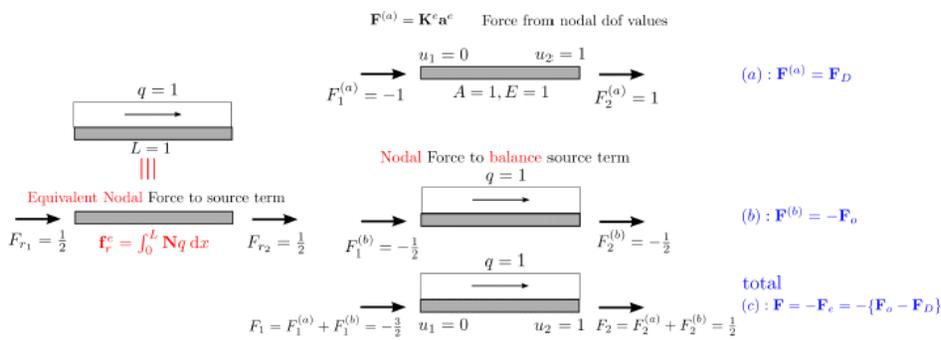
$$f_r^e = \frac{L}{2} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} \begin{bmatrix} 1 \\ 2 \\ 1 \end{bmatrix}$$

$\frac{1}{2} \rightarrow$  $\rightarrow \frac{1}{2}$

$$f_{\text{nodal}}^e = f_D^e - f_r^e = - \begin{pmatrix} f_r^e & f_D^e \\ f_D^e & f_r^e \end{pmatrix}$$

is applied on element nodes

Step 14: Compute prescribed dof forces: a) elements



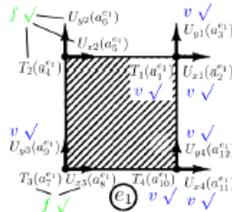
Nodal forces of the element

$$= \cancel{\begin{pmatrix} f_r^e & f_D^e \\ f_D^e & f_r^e \end{pmatrix}} = - \begin{pmatrix} f_r^e & f_D^e \\ f_D^e & f_r^e \end{pmatrix}$$

- → (T_{other} - T_D)

How to actually compute element forces:

Step 14: Compute prescribed dof forces: a) elements

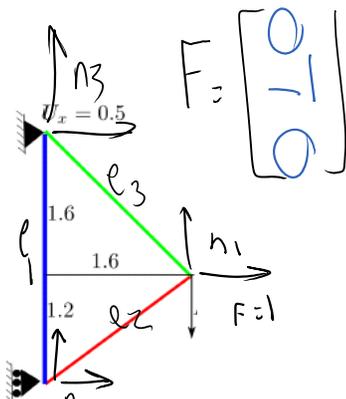


- Steps for calculation of F_p from elements: 1. calculation of element nodal forces; 2. Assembling those to correct position in F_p . Corresponding pseudocode:

```

for e = 1:ne loop over elements
  fee = feo element total force = element all forces except essential force
  for i = 1:nedof loop over rows of ke; nedof = element # dof
    I = dofMap(i) local to global dof map Mie
    if (I < 0) I corresponds to a prescribed dof, we skip free dofs
      for j = 1:nedof loop over columns of ke. ALL columns (dofs) of p and f used
        fee(i) = fee(i) - ke(i, j) * edofs(j) edofs: element dofs = ae
      end
      Fp(-I) = Fp(-I) - fee(i)
      1. element's total force fee component i'th is computed → added to Fp(-I)
      2. -I used because I < 0: prescribed dof
      3. fee is subtracted
    end
  end
end
end
end
  
```

$$f^e = - (f_{other}^e - f_D^e)$$

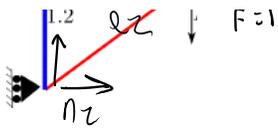


node unknowns: vs of free dofs & fs of pres. dofs

node	p	pos	v	f
1	false	1	-2.123	0
	false	2	-3.29	-1
2	true	1	0	?
	false	3	-1.2	0
3	true	2	.5	
	true	3	0	

$$F_p = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} = \begin{bmatrix} -2.123 \\ -3.29 \\ -1.2 \end{bmatrix}$$

$$F_p = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} = \begin{bmatrix} ? \\ ? \\ ? \end{bmatrix}$$



3	true	$\frac{2}{3}$	0					$p = \begin{bmatrix} 2 \\ 3 \end{bmatrix}$
---	------	---------------	---	--	--	--	--	--

e	LEM	dofMap	dofs	fe
1	[2, 3]	[$\bar{1}$ 3 $\bar{2}$ $\bar{3}$]	[0 $\bar{2}$ 0.5 0]	0 -4285 0 -4255
2	[2, 1]	[$\bar{1}$ 3 1 2]	[0]	.5715 .4286 .57 .4286
3	[3, 1]	[$\bar{2}$ $\bar{3}$ 1 2]	[5 0]	.5715 .5714 .5717 .5717

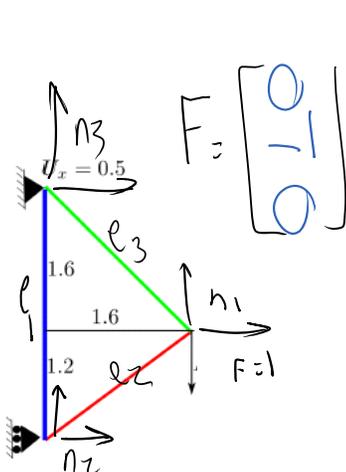
step 14a

Step 14a ... continued -> computing forces in Fp

We loop over the elements

Loop over their dofs

For prescribed dofs add the element force to global Prescribed forces Fp



node unknowns: vs of free dofs & fs of pres. dofs

node	p	pos	v	f
1	false	1	-2.123	0
	false	2	-3.29	-1
2	true	1	0	
	false	3	-1.2	0
3	true	$\bar{2}$.5	
	true	$\bar{3}$	0	

$F_p = \begin{bmatrix} 2 \\ 3 \end{bmatrix}$	$\begin{bmatrix} -2.123 \\ -3.29 \\ -1.20 \end{bmatrix}$
--	--

Step 14a continued

e	LEM	dofMap	dofs	fe
1	[2, 3]	[$\bar{1}$ 3 $\bar{2}$ $\bar{3}$]	[0 $\bar{2}$ 0.5 0]	0 -4285 0 -4255
2	[2, 1]	[$\bar{1}$ 3 1 2]	[0]	.5715 .4286 .57 .4286
3	[3, 1]	[$\bar{2}$ $\bar{3}$ 1 2]	[5 0]	.5715 .5714 .5717 .5717

step 14a

Step 14: Compute prescribed dof forces: b) nodes

Step 14b:

Add Fp values to prescribed node forces

To do so:

Loop over nodes

Loop over dofs of nodes

For those that are prescribed use their position to get the right force from global reaction forces (Fp)

Pseudo-code

```

for n = 1:nNodes
  for dofi = 1: node(n).ndof num dof for node (n)
    if node(n).ndof(dofi).p == true prescribed dof
      posn = node(n).ndof(dofi).pos position of dof in global prescribed force Fp
      node(n).ndof(dofi).f = Fp(-posn)
      1. set prescribed dof force to corresponding force in global Fp (Fp)
      2. posn < 0; prescribed dof
    end
  end
end

```

node unknowns: vs of prescribed & f's of pres. dofs

node	p	pos	v	f
1	false	1	-2.123	0
	false	2	-3.29	-1
2	true	1	0	.5715
	false	3	-1.2	0
3	true	2	.5	-.5715
	true	3	0	1

e	LEM	oFMap	dofs	fe
1	[2, 3]	[1 3 2 3]	[0 0 1.2 0 5 0]	[.4285 0 .4255]
2	[2, 1]	[1 3 1 2]	[0]	[.5715 .4286 .57 .4286]
3	[3, 1]	[2 3 1 2]	[5 0]	[.5715 .5714 .5714 .5714]

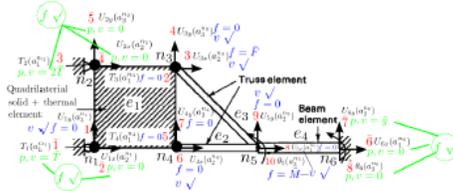
Handwritten calculations and annotations include: $U_p = 2$, $P = 2$, and various numerical values like 2.123, 3.29, 1.20, 5715, 4285, 4286, 5714, 5714. There are also circled numbers 14 and 15, and arrows indicating relationships between the tables and the calculations.

At this point all node, element, and global values are computed and we can output things in the last step (step 15)

The only point to mention is that for elements, again each element type has its own virtual (in object oriented framework) output function. For example, for bars and trusses one axial force may suffice, whereas for beams and frames we may compute y, θ, M, V at m

number of points along their length. The following slides describe this process

Step 15: Compute/output nodes & elements: a) nodes



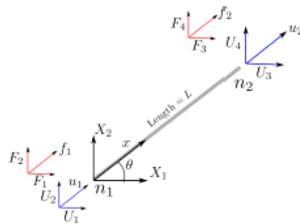
- After **free dof values** and **prescribed dof forces** are calculated, we can output the results.
- Node output is general, while element output is specific to its type. Sample pseudocode:

```

for n = 1:nNodes
  print: node (n) from (nNodes) nodes
  coord: (node(n).coordinate)
  for dofi = 1: node(n).nddof num dof for node (n)
    print dof:
      dof (dofi) from (node(n).nddof) dofs
      Field: (node(n).nddof(dofi).Field)
      Index: (node(n).nddof(dofi).index)
      Value: (node(n).nddof(dofi).value)
      Force: (node(n).nddof(dofi).force)
      prescribed: (node(n).nddof(dofi).p) may only be output for debugging purposes
      position: (node(n).nddof(dofi).position) may only be output for debugging purposes
  end
end
  
```

- Refer to slides 398 and 397 for other data members in node and dof objects.

Step 15: Compute/output nodes & elements: b) elements



- The computation and output of an element is again a **black box** function.
- Each element has its own specific compute/output function.
- For example, for truss elements we only need to compute axial force (figure above, also cf. 315 and (387)):

$$T = AE \{c(U_3 - U_1) + s(U_4 - U_2)\}$$

- For a beam element, moment M and shear force V change along the beam and they need a completely different process for computation (cf. page 374).
- These functions will be **virtual** in an object-oriented language. Sample pseudocode:
- For example, the virtual function's implementation for a truss element computes and outputs T from equation above/

```

for e = 1:ne loop over elements
  elements(e).Compute_Output_Element() virtual function on page 394
end
  
```