

From last time

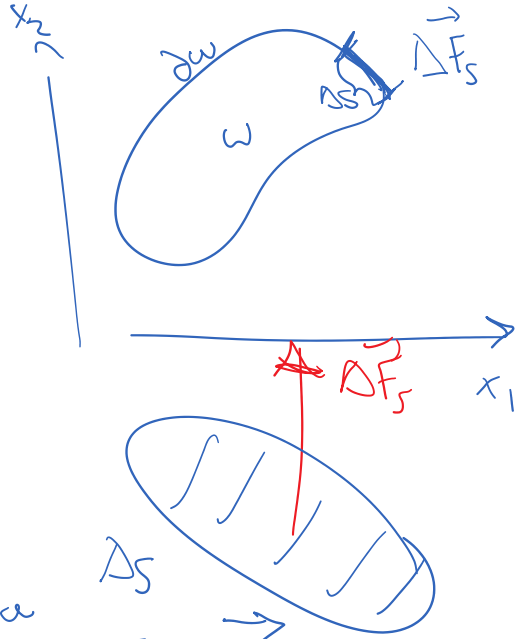
Surface force

$$\vec{F}_s = \sum \Delta \vec{F}_s$$

$$= \sum \frac{\Delta \vec{F}_s}{\Delta S} \Delta S$$

let $\Delta S \rightarrow 0$

$$= \int_{\partial \omega} \left[\lim_{\Delta S \rightarrow 0} \left(\frac{\Delta \vec{F}_s}{\Delta S} \right) \right] dS$$



intensity of force
 "force per area" $\lim_{\Delta S \rightarrow 0} \frac{\Delta \vec{F}_s}{\Delta S} = \vec{t}$

Pa
 $\frac{N}{m^2}$
 psi

$$\vec{F}_s = \int_{\partial \omega} \vec{t} dS$$

$$\vec{t} = \sigma \cdot \vec{n}$$

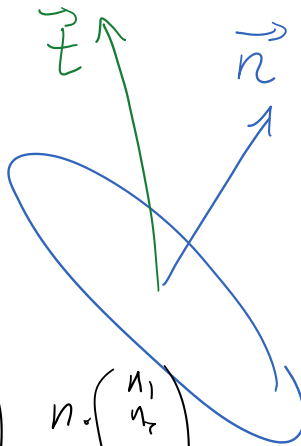
stress tensor

$$\sigma = \begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & - & - \\ & & \sigma_{33} \end{pmatrix}$$

stress tensor

$$t_s = \begin{pmatrix} t_1 \\ t_2 \\ t_3 \end{pmatrix}$$

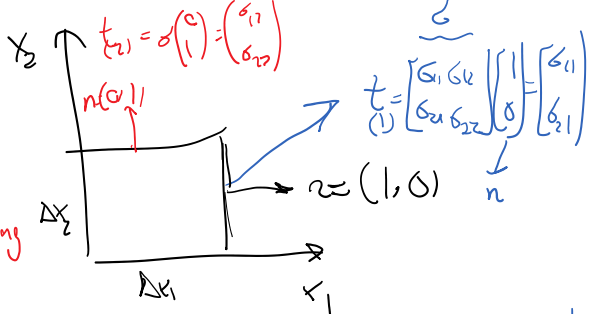
$$n = \begin{pmatrix} n_1 \\ n_2 \\ n_3 \end{pmatrix}$$



2D

$$\sigma = \begin{pmatrix} \sigma_{11} & \sigma_{12} \\ \sigma_{21} & \sigma_{22} \end{pmatrix}$$

traction
 for a surface with normal along x_1 axis



$$t_1 = \begin{pmatrix} \sigma_{11} & \sigma_{12} \\ \sigma_{21} & \sigma_{22} \end{pmatrix} \begin{pmatrix} 1 \\ 0 \end{pmatrix} = \begin{pmatrix} \sigma_{11} \\ \sigma_{21} \end{pmatrix}$$

1/9/2018

for a surface with normal along x_1 axis

$$\sigma = \sigma^T, \quad \sigma_{12} = \sigma_{21}$$

(Balance of angular momentum)

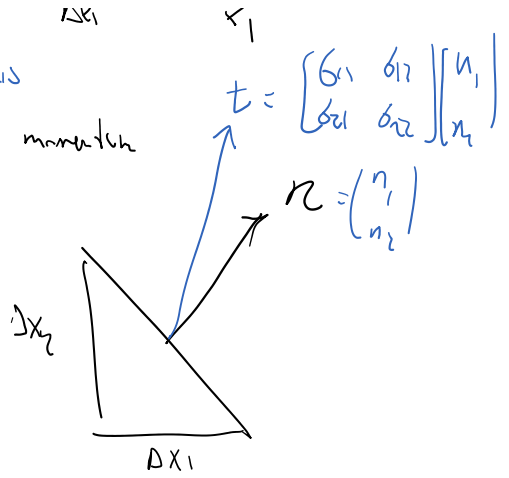
for arbitrary direction

force per area
T (traction)

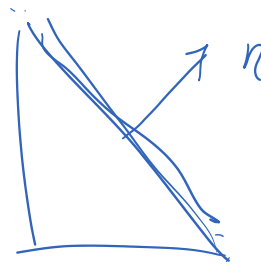
$$t = \sigma \cdot n$$

↓ stress tensor

normal vector



heat conduction



q

energy flux per surface area for normal n

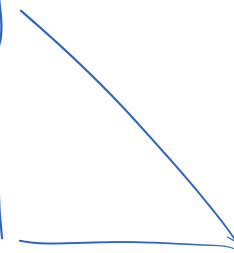
$$q \cdot n = \begin{pmatrix} q_1 \\ q_2 \end{pmatrix} \cdot \begin{pmatrix} n_1 \\ n_2 \end{pmatrix} = q_1 n_1 + q_2 n_2$$

In general

spatial flux density

$$\left(\frac{P}{x} \right)_n = \frac{P}{x} \cdot n$$

always one tensor order higher



Let's continue with balance of forces

$$\Sigma F = F_v + F_s$$

$$\int_{\omega} \rho b dV + \int_{\partial \omega} \sigma \cdot n dS = 0$$

integral over interior of ω

boundary of ω



Divergence / Gauss theorem

$$\int_{\partial \omega} \phi \cdot n \, dS = \int_{\omega} \nabla \cdot \phi \, dV \quad (2)$$

$$\text{ZF} \Rightarrow \int_{\omega} p b \, dV + \int_{\omega} \nabla \cdot \phi \, dV = 0$$

$$\forall \omega \subset D \int_{\omega} (\nabla \cdot \phi + p b) \, dV = 0$$

Integrand

Integral = 0

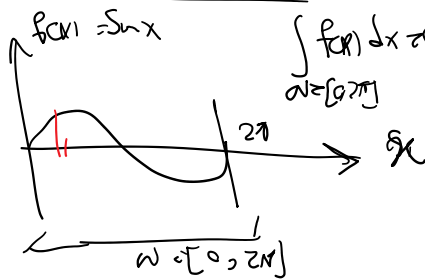
$$\forall \omega \int_{\omega} (\text{Integrand}) \, dV = 0$$

PDE / Strong form

$$\nabla \cdot \phi + p b = 0$$

Integrand = 0

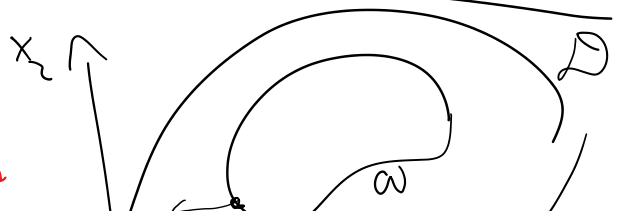
Example 1D



General Balance law

$$\forall \omega \subset D$$

f : quantity to be **balanced**



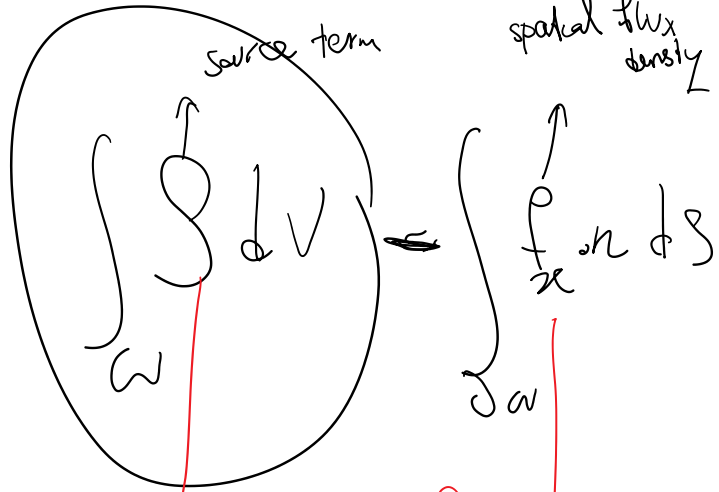
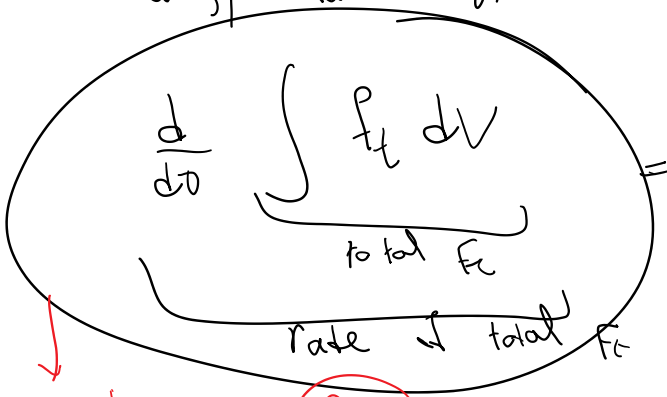
$$v \omega = v$$

f_t : quantity to be **balanced**
density



$$F_t = \int_{\omega} f_t dV$$

\downarrow energy \downarrow volume \downarrow energy density



example heat conduction: $\nabla \cdot \mathbf{q}$

$$\frac{d}{dt} \int_{\omega} \rho e dV = \int_{\omega} Q dV - \int_{\partial \omega} q_n dS$$

$$\frac{d}{dt} \int_{\omega} f_t dV = \int_{\omega} S dV - \int_{\partial \omega} f_x \cdot n dS$$

$$\int_{\omega} \frac{d}{dt} f_t dV = \int_{\omega} S dV - \int_{\omega} \nabla \cdot \mathbf{f}_x dV$$

3a) Dynamic Balance law for $F_t = \int_{\omega} f_t dV$

First dynamic: $\forall \omega \int_{\omega} \left(\frac{d}{dt} f_t + \nabla \cdot \mathbf{f}_x - S \right) dV = 0$

$$\frac{d}{dt} f_t + \nabla \cdot \mathbf{f}_x - S = 0 \quad (3b) \quad \text{Dynamic PDE}$$

$$\left[\frac{d}{dt} f_b + \nabla \cdot f_x - S = 0 \right] \textcircled{3b}$$

heat eqn

$e = cT$ q Q

Dynamic PDE

$$\left[\frac{d}{dt} (cTv) + \nabla \cdot q - Q = 0 \right] \textcircled{3c}$$

$f_b = p = \rho v$ $f_x = -\sigma$ $S = \rho b$

- Example 1 heat conduction

Example 2 solid mechanics

$$\frac{d}{dt} \rho v + \nabla \cdot (-\sigma) - \rho b = 0$$

Equation of motion

Static / ~~steady~~ steady state problems

~~$$\frac{d}{dt} \int_{\omega} f_x dV = \int_{\partial\omega} f_{onx} ds + \int_{\omega} S dV$$

$$= 0$$~~

no change in time

$$\left[\int_{\partial\omega} f_x \cdot n ds = \int_{\omega} S dV \right] \textcircled{4}$$

balance law for statics

$$\int_{\omega} \nabla f_x = \int_{\omega} S dV \rightarrow$$

$$\boxed{\nabla f_x - S = 0}$$

Differential equation

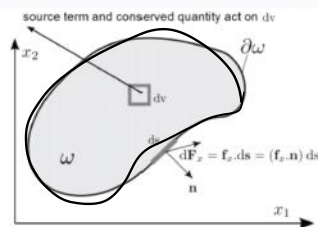
Summary slide

General form of balance laws

For a general conservation law let:

- f_t : conserved quantity = temporal flux
- f_x : total outward spatial flux
- r : source term

then the balance law for dynamics reads:



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$$\forall \omega \subset \mathcal{D} \wedge \forall t: \int_{\omega} \mathbf{r} \, dv - \int_{\partial\omega} \mathbf{f}_x \cdot d\mathbf{s} = \int_{\omega} \mathbf{r} \, dv - \int_{\partial\omega} (\mathbf{f}_x \cdot \mathbf{n}) \, ds = \frac{d}{dt} \int_{\omega} \mathbf{f}_t \, dv \quad (13)$$

For static case the RHS is zero (i.e., the quantity $\int_{\omega} \mathbf{f}_t \, dv$ remains constant). The static balance law reads:

$$\forall \omega \subset \mathcal{D}: \int_{\omega} \mathbf{r} \, dv - \int_{\partial\omega} \mathbf{f}_x \cdot d\mathbf{s} = \int_{\omega} \mathbf{r} \, dv - \int_{\partial\omega} (\mathbf{f}_x \cdot \mathbf{n}) \, ds = \mathbf{0} \quad (14)$$

These can be directly compared to $\mathbf{F} = d\mathbf{P}/dt$ and $\mathbf{F} = 0$ in previous discrete examples.

For any balance law we have

$$\int_{\partial\Omega} \mathbf{F} \cdot \mathbf{n} \, dS = \int_{\Omega} \mathbf{r} \, dV$$

$\partial\Omega$ ↓ spatial (space and time) normal
 Ω ↓ solid term

$\nabla \cdot \mathbf{F} = \mathbf{r}$
 ↓ space (space time divergence)

FIT

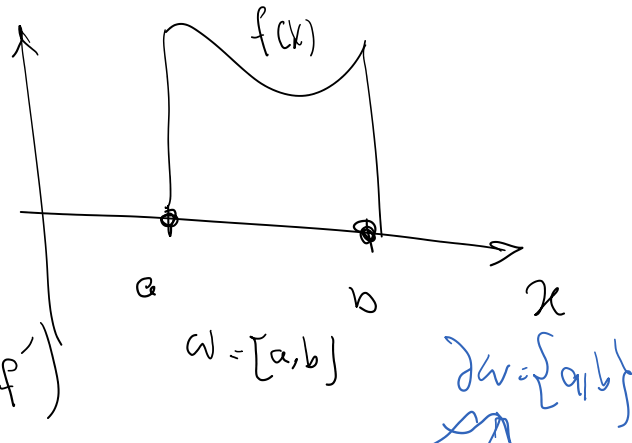
You can skip slides 6-14, except slide 13, the static part of it

We'll discuss divergence theorem and localization theorem

Divergence theorem

$$\int_a^b F(x) \, dx = f(b) - f(a)$$

$$(F = \int F \neq F = f')$$

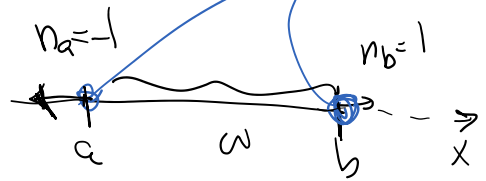


$$(F = \int F \neq F = f')$$

$$v = [a, b] \quad d\omega = [a, b]$$

that is

$$\int_{\omega=[a,b]} f'(x) dx = f(b) \cdot 1 + f(a) \cdot (-1)$$



3

$$\int_{\omega} f'(x) dx = f(a)n_a + f(b)n_b = \int_{\partial\omega} f(x) \cdot n(x) ds$$

Compare this with divergence theorem

$$\int_{\omega} \nabla \cdot f(x) dV = \int_{\partial\omega} f(x) \cdot n ds$$

for any of these $\textcircled{*}$ applies

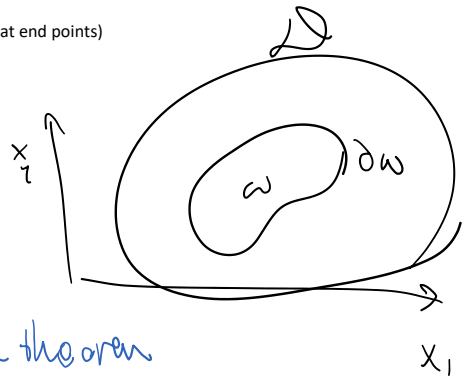
Divergence theorem is multi-dimension version of fundamental theorem of calculus (turning line integral to values at end points)

Which one is more general

Motivation:

$$\int_{\omega} \rho b dV + \int_{\partial\omega} \sigma \cdot n ds$$

using divergence theorem



$$\int_{\omega} \nabla \cdot \sigma dV$$

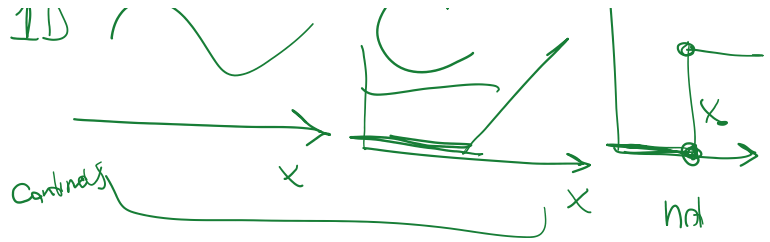
we have derivation $\ddot{\rho}$

For the balance law, all we need is that the spatial flux (sigma here) to be integrable over the boundary of omega.

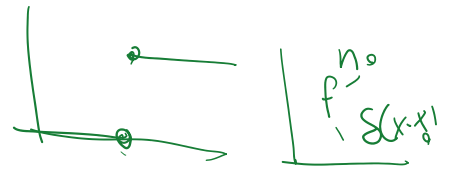
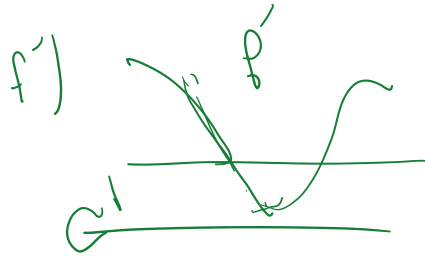
However, for getting to DE, i.e. the blue term divergence of spatial flux should exist and in fact should be continuous.

C^0 function is continuous \rightarrow 1D \rightarrow C^0 \rightarrow not C^0

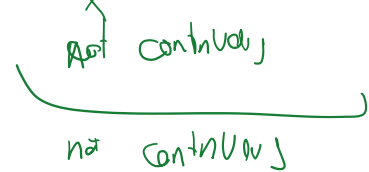
C^0 function is continuous
f:



C^1 if f & f'
are continuous



C^2 if f, f', f''
are continuous



C^n means $f, f', \dots, f^{(n)}$ derivatives exist and all are continuous

(1D)
2D $f, \frac{\partial f}{\partial x_i}, \frac{\partial^2 f}{\partial x_i \partial x_j}, \dots$ n partial derivatives

Divergence theorem

$$\int_{\partial \Omega} f \cdot n \, dS = \int_{\Omega} (\nabla \cdot f) \, dV$$

Divergence theorem requires $\nabla \cdot f$ to exist & to be continuous

$$f \in C^1(\Omega)$$

this is restrictive. For balance law, f should be integrable

this is restrictive. For balance law, f should be integrable