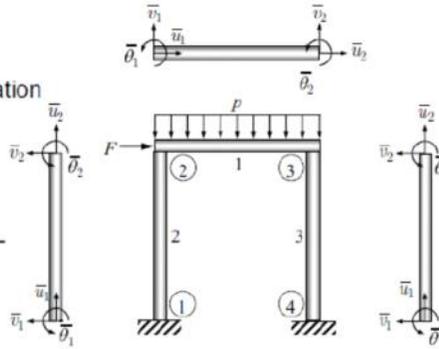


Frames

Frames: 2D frame elements

- Beam
  - Vertical deflection and slope. No axial deformation
- Frame structure
  - Can carry axial force, transverse shear force, and bending moment (Beam + Truss)
- Assumption
  - Axial and bending effects are uncoupled
  - Reasonable when deformation is small
- 3 DOFs per node
  - $\{u_i, v_i, \theta_i\}$
- Need coordinate transformation like plane truss



source: Nam-Ho Kim, Raphael T. Haftka; <http://www2.mae.ufl.edu/nkim/eml5526/> sec. 5 381 / 456

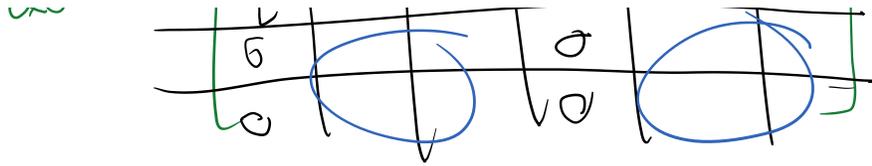
Handwritten diagrams and a stiffness matrix for a beam element. The diagrams show a beam with forces  $a_1, a_2$  and moments  $a_3, a_4$  at one end, and forces  $a_5, a_6$  and moments  $a_7, a_8$  at the other end. The stiffness matrix is given as:

$$k = \frac{AE}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

and

$$k_{4 \times 4} = \frac{EI}{L^3} \begin{bmatrix} 12 & 6L & 0 & 0 \\ 6L & 4L^2 & 0 & 0 \\ 0 & 0 & 12 & 6L \\ 0 & 0 & 6L & 4L^2 \end{bmatrix}$$

The matrix is shown in a grid format with nodes 1-6 and degrees of freedom 1-6. The matrix is symmetric and has zeros in the upper right and lower left quadrants.



## 2D frame element: axial and bending stiffness matrices

- Axial deformation (in local coord.)

$$\frac{EA}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} \bar{u}_1 \\ \bar{u}_2 \end{Bmatrix} = \begin{Bmatrix} f_{\bar{x}1} \\ f_{\bar{x}2} \end{Bmatrix}$$

- Beam bending

$$\frac{EI}{L^3} \begin{bmatrix} 12 & 6L & -12 & 6L \\ 6L & 4L^2 & -6L & 2L^2 \\ -12 & -6L & 12 & -6L \\ 6L & 2L^2 & -6L & 4L^2 \end{bmatrix} \begin{Bmatrix} \bar{v}_1 \\ \bar{\theta}_1 \\ \bar{v}_2 \\ \bar{\theta}_2 \end{Bmatrix} = \begin{Bmatrix} f_{\bar{y}1} \\ \bar{c}_1 \\ f_{\bar{y}2} \\ \bar{c}_2 \end{Bmatrix}$$

- Basically, it is equivalent to overlapping a beam with a bar
- A frame element has 6 DOFs

source: Nam-Ho Kim, Raphael T. Haftka; <http://www2.mae.ufl.edu/nkim/eml5526/> sec. 5

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## 2D frame: local & global coordinate stiffness matrices

- Element matrix equation (local coord.)

$$\begin{bmatrix} a_1 & 0 & 0 & -a_1 & 0 & 0 \\ 0 & 12a_2 & 6La_2 & 0 & -12a_2 & 6La_2 \\ 0 & 6La_2 & 4L^2a_2 & 0 & -6La_2 & 2L^2a_2 \\ -a_1 & 0 & 0 & a_1 & 0 & 0 \\ 0 & -12a_2 & -6La_2 & 0 & 12a_2 & -6La_2 \\ 0 & 6La_2 & 2L^2a_2 & 0 & -6La_2 & 4L^2a_2 \end{bmatrix} \begin{Bmatrix} \bar{u}_1 \\ \bar{v}_1 \\ \bar{\theta}_1 \\ \bar{u}_2 \\ \bar{v}_2 \\ \bar{\theta}_2 \end{Bmatrix} = \begin{Bmatrix} \bar{f}_{x1} \\ \bar{f}_{y1} \\ \bar{c}_1 \\ \bar{f}_{x2} \\ \bar{f}_{y2} \\ \bar{c}_2 \end{Bmatrix} \quad \begin{aligned} a_1 &= \frac{EA}{L} \\ a_2 &= \frac{EI}{L^3} \end{aligned}$$

## 2D frame element: coordinate transformation

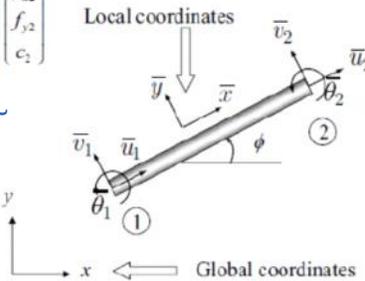
- Element-fixed local coordinates  $\bar{x}-\bar{y}$
- Local DOFs  $\{\bar{u}, \bar{v}, \bar{\theta}\}$       Local forces  $\{\bar{f}_x, \bar{f}_y, \bar{c}\}$
- Transformation between local and global coord.

$$\begin{Bmatrix} f_{T1} \\ f_{T2} \\ \bar{c}_1 \\ f_{T2} \\ f_{T2} \\ \bar{c}_2 \end{Bmatrix} = \begin{bmatrix} \cos\phi & \sin\phi & 0 & 0 & 0 & 0 \\ -\sin\phi & \cos\phi & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & \cos\phi & \sin\phi & 0 \\ 0 & 0 & 0 & -\sin\phi & \cos\phi & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{Bmatrix} f_{S1} \\ f_{S1} \\ c_1 \\ f_{S2} \\ f_{S2} \\ c_2 \end{Bmatrix}$$

$$\{\bar{\mathbf{f}}\} = [\mathbf{T}]\{\mathbf{f}\}$$

$$\{\bar{\mathbf{q}}\} = [\mathbf{T}]\{\mathbf{q}\}$$

transfer matrix



source: Nam-Ho Kim, Raphael T. Haftka; <http://www2.mae.ufl.edu/nkim/eml5526/> sec. 5  
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## 2D frame: local & global coordinate stiffness matrices

- Element matrix equation (local coord.)

$$\begin{bmatrix} a_1 & 0 & 0 & -a_1 & 0 & 0 \\ 0 & 12a_2 & 6La_2 & 0 & -12a_2 & 6La_2 \\ 0 & 6La_2 & 4L^2a_2 & 0 & -6La_2 & 2L^2a_2 \\ -a_1 & 0 & 0 & a_1 & 0 & 0 \\ 0 & -12a_2 & -6La_2 & 0 & 12a_2 & -6La_2 \\ 0 & 6La_2 & 2L^2a_2 & 0 & -6La_2 & 4L^2a_2 \end{bmatrix} \begin{Bmatrix} \bar{u}_1 \\ \bar{v}_1 \\ \bar{\theta}_1 \\ \bar{u}_2 \\ \bar{v}_2 \\ \bar{\theta}_2 \end{Bmatrix} = \begin{Bmatrix} \bar{f}_{x1} \\ \bar{f}_{y1} \\ \bar{c}_1 \\ \bar{f}_{x2} \\ \bar{f}_{y2} \\ \bar{c}_2 \end{Bmatrix}$$

$$a_1 = \frac{EA}{L}$$

$$a_2 = \frac{EI}{L^3}$$

$$[\bar{\mathbf{k}}]\{\bar{\mathbf{q}}\} = \{\bar{\mathbf{f}}\}$$

- Element matrix equation (global coord.)

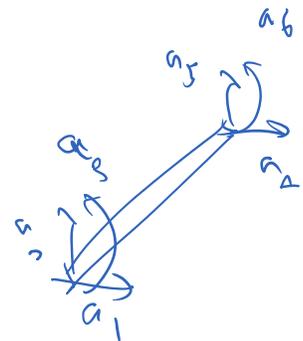
$$[\bar{\mathbf{k}}][\mathbf{T}]\{\mathbf{q}\} = [\mathbf{T}]\{\mathbf{f}\} \Rightarrow [\mathbf{T}]^T[\bar{\mathbf{k}}][\mathbf{T}]\{\mathbf{q}\} = \{\mathbf{f}\} \Rightarrow [\mathbf{k}]\{\mathbf{q}\} = \{\mathbf{f}\}$$

$$[\mathbf{k}] = [\mathbf{T}]^T[\bar{\mathbf{k}}][\mathbf{T}]$$

- Same procedure for assembly and applying BC

source: Nam-Ho Kim, Raphael T. Haftka; <http://www2.mae.ufl.edu/nkim/eml5526/> sec. 5

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HW

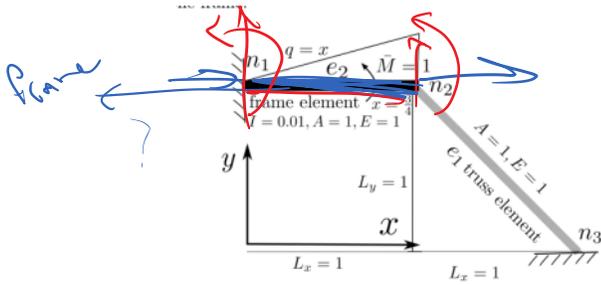


Figure 3: Frame and truss example.

but treat it as if there a bar & beam element at the same local.

Coding:

For your term project you can use the incomplete C++ code I provide (10% extra credit) or use Matlab, Python (5%), etc. to write your code.  
Need to read and write in the formats I provide  
You can work in groups of 2 or 3 (C++, Python)

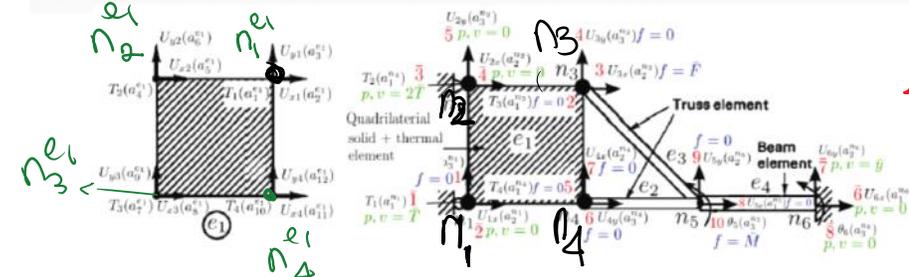
Part A:

Classes relevant to FEM (Object-oriented programming)

For each class, we discuss Data and functions

### FEM Solver Objects: 1. Element: Data

→ dof numbers



Data

- id
- nNodes
- eNodes (LEM)

1  
4

[ 3 2, 1, 4 ]

- edof (a) : vector of unknowns [ T1, Ux1, Uy1 | T2, Ux2, Uy2 | T3, Ux3, Uy3 | T4, Ux4, Uy4 ]

- dofMap (M) : [ 2 3 4 | 3 7 5 | 1 2 11 5 6 ]

- dof Map (M) : [ 2 3 4 | 3 7 5 | 1 2 1 | 5 6 ]

- forces  $f_e^e, f_o^e, f_D^e, f_N^e, \dots$

$$f_e^e = \underbrace{(f_o^e + f_N^e + \dots)}_{f_o^e \rightarrow \text{other}} - f_D^e$$

↓ Dirichlet

for term project  $f_o^e = 0$

- Stiffness

$k^e$

- e Type

square

- { Physics }

→ list of physics the element solves  
Solid & Thermal

## Examples of functions

① Virtual

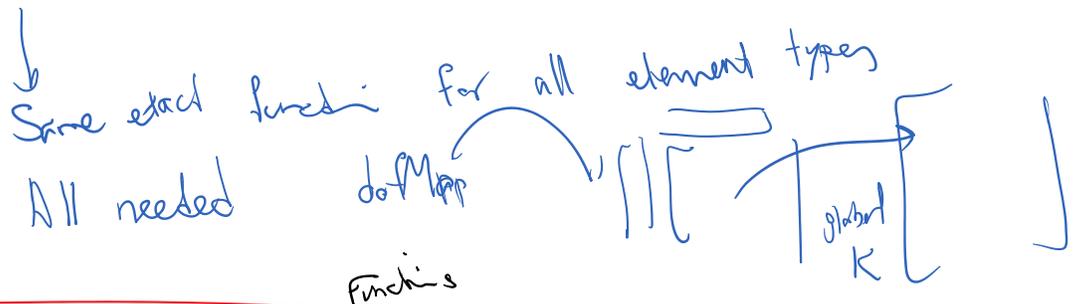
Calculate Stiffness

Different functions for different element types

$$\left( \begin{array}{l} \text{bar } k^e = \frac{AE}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \\ \text{truss } k^e = \frac{AE}{L} \begin{bmatrix} k_b & -k_b \\ -k_b & k_b \end{bmatrix} \\ \text{beam } k^e = \frac{AE}{L^3} F \end{array} \right)_{4 \times 4}$$

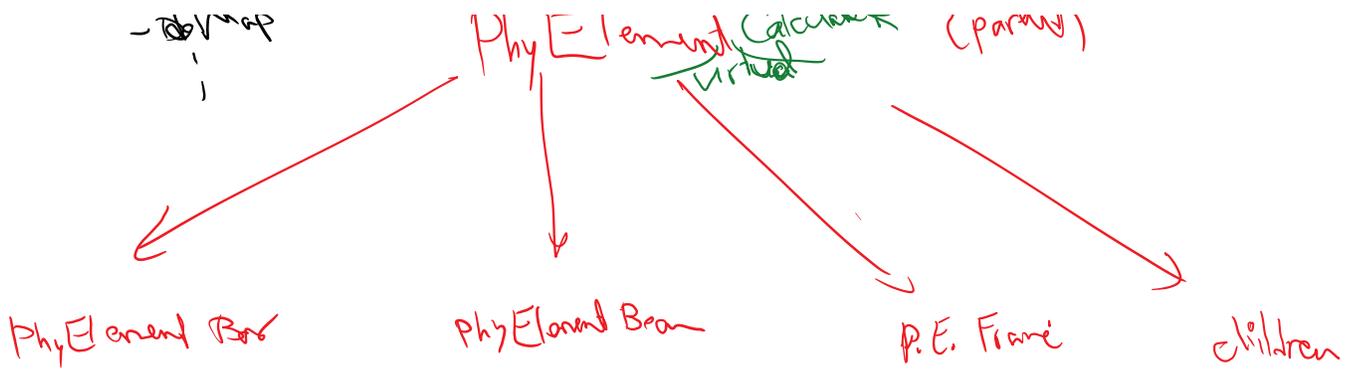
②

Assemble Stiffness

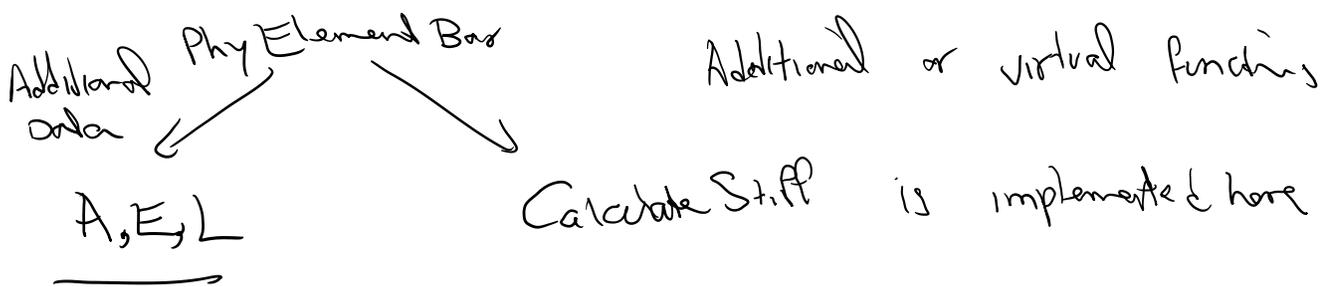


Do not - id  
- nN do  
- doMap  
...

Phy Element Calculate Virtual (param) → Assemble K



Children inherit all parent class Data & Functions  
 in addition they can have their additional Data & Funct.



**class PhyElement**

```

{
  friend ostream& operator<<(ostream& out, const PhyElement& dat);
public:
  virtual void setGeometry() = 0;
  virtual void setInternalMaterialProperties(PhyMaterial* pMat) = 0;
  void setNodeConnectivity_Sizes(int nNodeInElement, int ndofpnIn, vector<int>& eNodesIn,
  vector <PhyNode*>& eNodePtrsIn);

  void print(ostream& out);
  // Step 8: Element dof maps Me
  // Step 9: Set element dofs ae
  void setElementDofMap_ae(int ndofpn);

  // Step 10: Compute element sti
  ness/force (ke, foe (fre: source term; fNe: Neumann BC))
  virtual void Calculate_ElementStiffness_Force() = 0;
  // Step 11: Assembly from local to global system
  void AssembleStiffnessForce(MATRIX& globalK, VECTOR& globalF);

  // Step 14: Compute prescribed dof forces
  void UpdateElementForces_GlobalFp(VECTOR& Fp);

  // Step 15: Compute/output element specific data
  virtual void SpecificOutput(ostream& out) const {THROW("does not have implementation");};
}

```

children will provide their implementation  
 All element types are assembled the same way, so the implementation is here

// Step 15: Compute/output element specific data

```
virtual void SpecificOutput(ostream& out) const {THROW("does not have implementation");}
```

```
int id;  
int neNodes; // # element nodes  
vector<int> eNodes; // element node vector  
vector<PhyNode*> eNodePtrs;  
int nedof; // # element dof  
VECTOR edofs; // element dofs  
vector<int> dofMap;  
ElementType eType;  
int matID;  
MATRIX ke; // element stiffness matrix  
VECTOR foe; // element force vector from all sources other than essential BC  
VECTOR fde; // element essential BC force  
VECTOR fee; // all element forces  
};
```

Function

Data

Look a child of PhyElement

```
class PhyElementBar : public PhyElement  
{  
public:  
    virtual void setGeometry();  
    virtual void  
    setInternalMaterialProperties(PhyMaterial* pMat);  
    virtual void Calculate_ElementStiffness_Force();  
    virtual void SpecificOutput(ostream& out) const;  
    double L;  
    double A;  
    double E;  
};
```

PhyElementBar is a child of PhyElement

Whenever we go to subclasses (children) we only need to add new + virtual functions and new data. All the other things are inherited.

Element has its own declaration & implementation (C++, C++)

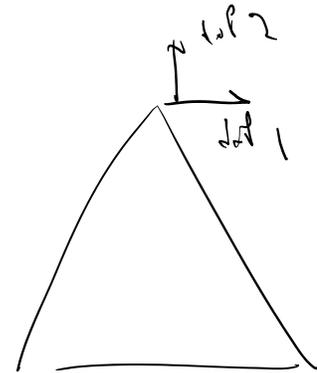
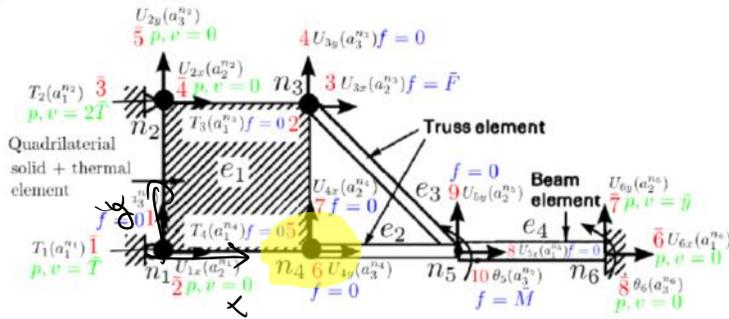
new data

From PhyElement.cpp

```
void PhyElementBar::Calculate_ElementStiffness_Force()  
{  
    // compute stiffness matrix:  
    ke.resize(2, 2);  
    double factor = A * E / L;  
    ke(0, 0) = ke(1, 1) = factor;  
    ke(1, 0) = ke(0, 1) = -factor;  
}
```

Other classes:

## FEM Solver Objects: 4. Node: Data



Data

id

coordinate

dofs

nndof

$n_4$

4

$[1, 0]$

{ PhyDofs }

3

we have a vector of dofs

PhyNode.h

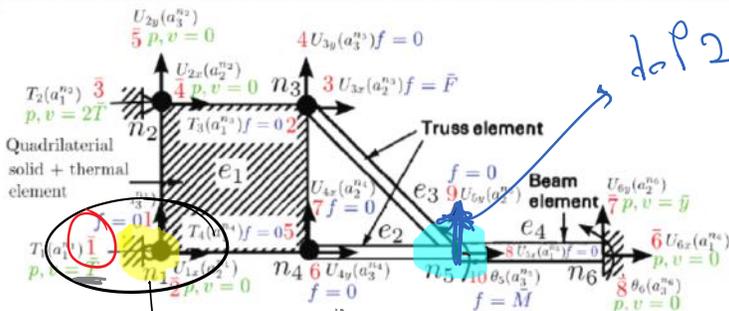
class PhyNode

```

{
public:
    void set_nndof(int nndofIn);
    void UpdateNodePrescribedDofForces(VECTOR& Fp);
    ID id;
    VECTOR coordinate;
    vector<PhyDof> ndof;
    int nndof; // number of dofs
};
    
```

Data

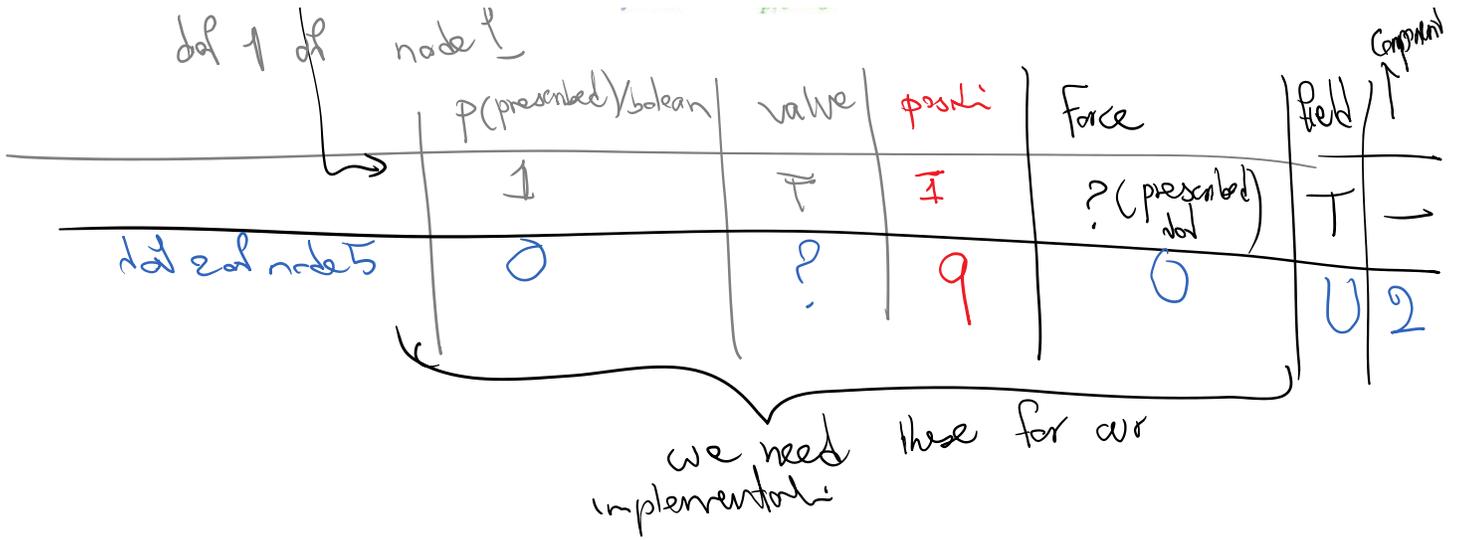
## FEM Solver Objects: 5. Dof: Data



dof 1 of node 1

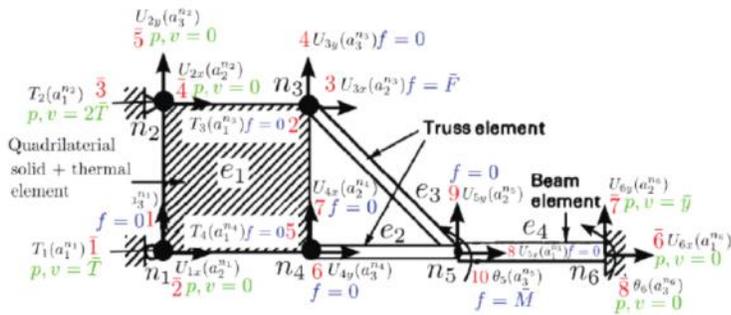
represented in local - - - - -

10/11/17



PhyDof.h

### FEM Solver Objects: 5. Dof



Examples of dof for the structure shown are:

dof	$p$	pos	$v$	$f$	field	index
1 of $n_1$	true	$\bar{1}$	$\bar{T}$	unknown	T	-
3 of $n_1$	false	1	unknown	0	U	2
3 of $n_5$	false	10	unknown	$\bar{M}$	$\theta$	- (a vector in 3D)
2 of $n_6$	true	$\bar{7}$	$\bar{y}$	unknown	U	2

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```
class PhyDof
{
public:
```

```
PhyDof());
```

```
bool p; // boolean: whether the dof is prescribed
int pos; // position in the global system (for free and prescribed)
double v; // value of dof
double f; // force corresponding to dof
```

```
// F can be stress i can be (0, 1) sigma_{01}
// Field F;
// INDEX i;
};
```

## Steps for solution

### Solution steps

The steps for FEM solution are:

- 1 Set Element nodal dofs.
- 2 Set global dofs using element dofs.
- 3 Compute  $n_f$  from  $n_{dof}$  and  $n_p$  and resize and zero stiffness matrix and force vector.
- 4 Set global prescribed dofs.
- 5 Set global free dofs.
- 6 Set dof (free + prescribed) positions.
- 7 Set  $\mathbf{F}(\mathbf{F}_f)$ .
- 8 Set element dof maps  $\mathbf{M}_t^e$ .
- 9 Set element (prescribed) dofs.
- 10 Compute element stiffness matrix and force vectors.
- 11 Assemble element stiffnesses and forces to global system.
- 12 Solve for (free) dofs  $\mathbf{a}$  from  $\mathbf{K}\mathbf{a} = \mathbf{F}$ .
- 13 Assign  $\mathbf{a}$  to nodes and elements.
- 14 Compute prescribed dof forces:  $\mathbf{F}_p$  (if needed).
- 15 Compute (if needed) output nodes and elements.

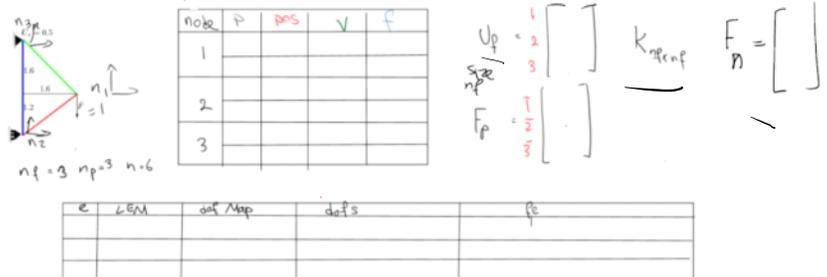
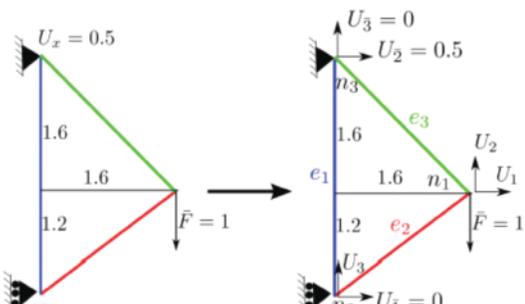
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## Input text file

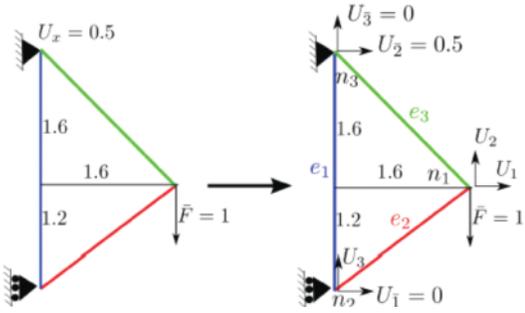
TrussTest.txt

It's for this problem

### Truss Example



# Truss Example



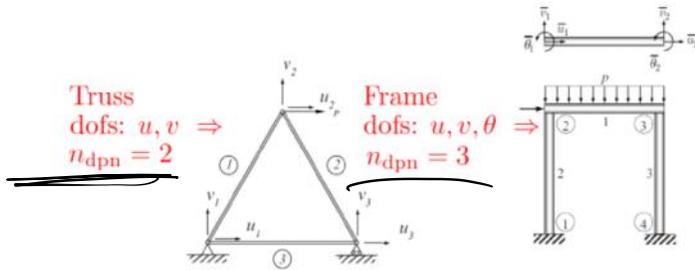
$n_f = 3$   $n_p = 3$   $n = 6$

node	r	v	t
1			
2			
3			

$U_p = \begin{bmatrix} 2 \\ 3 \end{bmatrix}$   $K_{ref}$   $F_p = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$   $F_n = \begin{bmatrix} \end{bmatrix}$

e	LSM	def Map	dofs	fc

## Steps 1 & 2: Simplified limited case



- FEM implementation become considerably simpler for problems where all elements are of the same type (regardless of number of physics per element).
- In this case, we define:

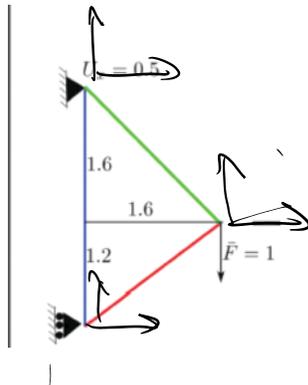
$$n_{dofn} := \text{Number of dof. per node denoted by } \underline{\text{ndofpn}} \quad (448)$$

- There would be identity map between element nodal dof and global nodal dofs. That is, there is the same set of dofs used for both.
- Figure above shows two of such examples:

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TrussTest.txt

dim 2  
ndofpn 2



## Step 3: Set global number of dofs, stiffness, and force.

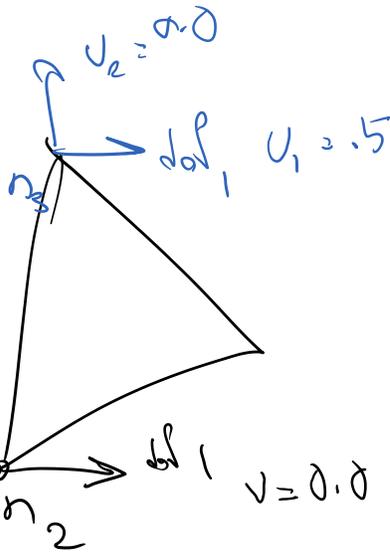
$$n = n_{nodes} \times n_{dofpn}$$

$$3 * 2 = 6$$

Nodes  
 nNodes 3  
 id crd  
 1 1.6 1.2  
 2 0.0  
 3 0.2.8

PrescribedDOF

np	node	node_dof	index	value
2	1	0	0	0.0
3	1	0.5		
3	2	0		0.0



$$n_p = 3$$

$$n = 6$$

$$n_f = n - n_p = 6 - 3 = 3$$

$$K = \begin{bmatrix} & & \\ & & \\ & & \end{bmatrix}_{n_f \times n_f}$$

$$\begin{pmatrix} F \\ P \end{pmatrix}_{n_p \times 1} = \begin{bmatrix} - \\ - \end{bmatrix}$$

$$a_{np} = \begin{bmatrix} - \\ - \end{bmatrix}$$