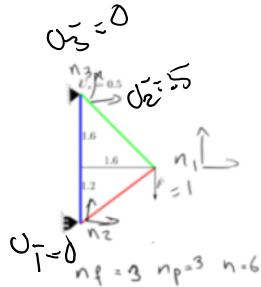


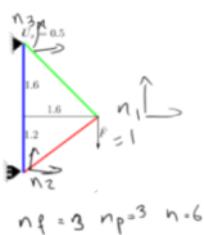
Step 4: Set global prescribed nodal dof



node	P	pos	v	f
1				
2				
3				

$$\begin{aligned} \text{max} &= 3 \\ U_p &= \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} \quad K_{n_f \times n_f} \\ \text{size} &= 3 \\ F_p &= \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} \quad F_N = \begin{bmatrix} \end{bmatrix} \\ n_f &= 3 \end{aligned}$$

e	LEM	dof Map	dofs	β_e



node	P	pos	v	f
1	0	?	?	?
2	0	?	?	?
3	1	0.0	?	?
1	0	0.5	?	?
2	0	0.5	?	?
3	0	0.0	?	?

$$\begin{aligned} \text{max} &= 3 \\ U_p &= \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} \quad K_{n_f \times n_f} \\ \text{size} &= 3 \\ F_p &= \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} \quad F_N = \begin{bmatrix} \end{bmatrix} \\ n_f &= 3 \end{aligned}$$

e	LEM	dof Map	dofs	β_e

np 3

node node_dof_index value

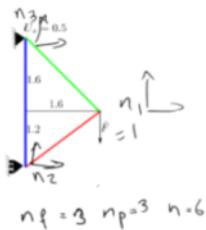
2 1 0.0

3 1 0.5

3 2 0.0

Step 5: Set global free nodal dof

All dofs in FEM are by default FREE with ZERO "force". Since from step 4, we already know which dofs are prescribed (-> we'd know which ones are free), here we only need to provide free dofs with nonzero force



node	P	pos	V	F
1	0	?	0	?
1	0	?	0	-1.0?
2	1	0	0	?
2	0	?	0	?
3	1	0.5	0	?
3	0	0.0	0	?

$$U_p = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

$$k_{npnf} = \begin{bmatrix} 1 & & \\ & 2 & \\ & & 3 \end{bmatrix}$$

$$F_p = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

$$F_N = \begin{bmatrix} ? \\ ? \\ ? \end{bmatrix}$$

e	LEM	dof Map	dofs	fe

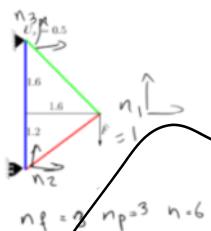
FreeDofs

nNonZeroForceDOFs 1

node node_dof_index value

1 2 -1.0

Step 6: dof positions; Step 7: Set $\mathbf{F}(\mathbf{F}_f)$



node	P	pos	V	F
1	0	?	0	?
1	0	?	0	-1.0?
2	1	0	0	?
2	0	?	0	?
3	1	0.5	0	?
3	0	0.0	0	?

$$U_p = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

$$k_{npnf} = \begin{bmatrix} 1 & & \\ & 2 & \\ & & 3 \end{bmatrix}$$

$$F_p = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

$$F_N = \begin{bmatrix} ? \\ ? \\ ? \end{bmatrix}$$

e	LEM	dof Map	dofs	fe

FreeDofs

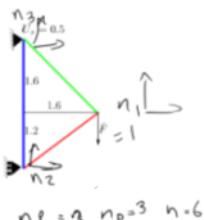
nNonZeroForceDOFs 1

node node_dof_index value

1 2 -1.0

free ones ~~1~~ ~~2~~ ~~3~~
prescribed ones ~~1~~ ~~2~~ ~~3~~

Step 7: Set \mathbf{F}_f



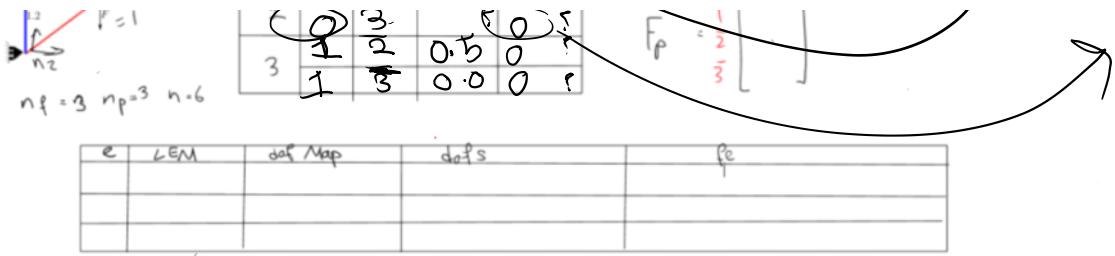
node	P	pos	V	F
1	0	1	?	?
1	0	2	?	-1.0?
2	1	1	0	?
2	0	3	0	?
3	1	2	0.5	?
3	0	3	0.0	?

$$U_p = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

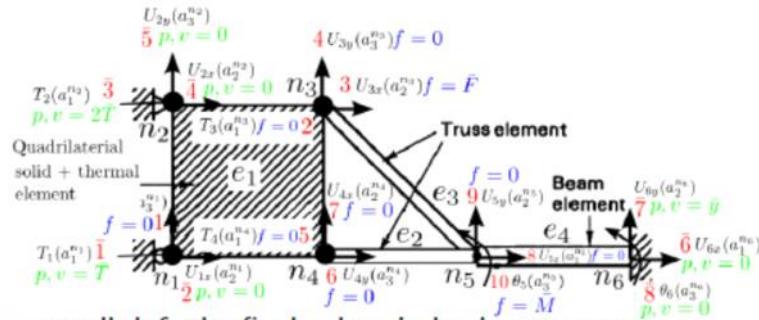
$$k_{npnf} = \begin{bmatrix} 1 & & \\ & 2 & \\ & & 3 \end{bmatrix}$$

$$F_p = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

$$F_N = \begin{bmatrix} 0.0 \\ -1.0 \\ 0.0 \end{bmatrix}$$



Step 6: dof positions; Step 7: Set $\mathbf{F}(\mathbf{F}_f)$



- After looping over all dofs the final values in load vector are:

$$\mathbf{F} = [0 \ 0 \ \bar{F} \ 0 \ 0 \ 0 \ 0 \ 0 \ 0 \ \bar{M}]$$

posf = 0, posp = 0

for n = 1:nNodes

```

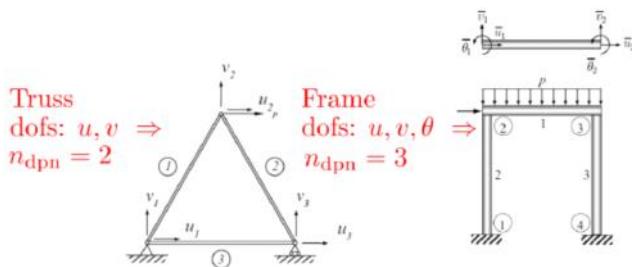
    for dofi = 1: node(n).nndof num dof for node (n)
        if node(n).ndof(dofi).p == true prescribed dof
            posp = posp - 1;
            node(n).ndof(dofi).pos = posp;      Step 6
        else free dof
            posf = posf + 1;
            node(n).ndof(dofi).pos = posf;
            F(posf) = node(n).ndof(dofi).f
        end
    end
end

```

415 / 456

Step 8: Element dof maps \mathbf{M}_t^e

Step 8: Element dof maps \mathbf{M}_t^e : Simplified limited case

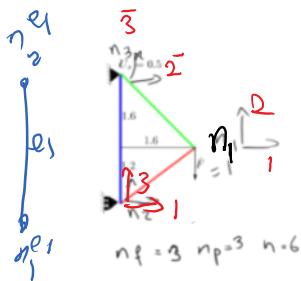


n_{dof}^e \bar{s}



Γ Γ

Δ



node	P	pos	v	f
1	0	1	?	0
0	0	2	?	-1.0
1	1	?	0	0
2	2	3	0	?
3	3	2	0.5	0
1	1	3	0.0	0

$$U_p = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} \quad K_{np \times np} \quad F_p = \begin{bmatrix} 0.0 \\ -1.0 \\ 0.0 \end{bmatrix}$$

e	LEM	dofMap	dofs	fe
1	[2 3]	[1 3 2 3]		
2	[2 1]	[1 3 1 2]		
3	[3 1]	[2 3 1 2]		

For step 8, to form dofMap, we first need to know the map between element nodes and the global domain nodes -> NodalMap or LEM.

How do we get this?

Elements
ne 3

id elementType matID neNodes eNodes

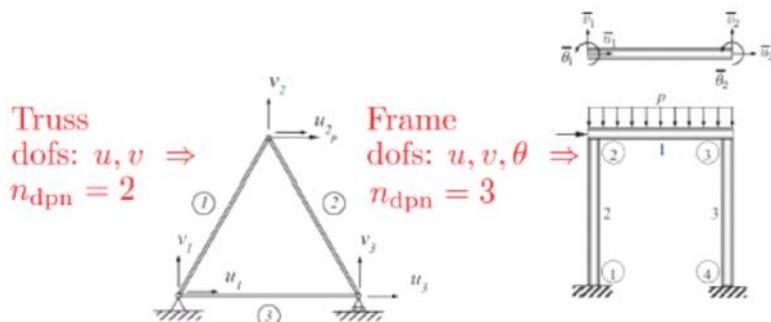
1	1	2	2 3
2	3	1	2 1
3	3	1	3 1

material id
element type
nodes for element

1. bar
2. beam
3. truss
4. frame

Slide 420:

Step 8: Element dof maps M_t^e : Simplified limited case



A simplified pseudo code looks like: ec dof = 1 dof counter for element
for en = 1: neNodes number of element nodes

gn = LEM(en) global node number for element node en

for endof = 1: ndofpn This number is fixed now, e.g., 2 for 2D trusses

dofMap(ec dof) = node(gn).dof(endof).pos

gndof = endof, we bypass some steps here

ec dof = ec dof + 1 increment counter

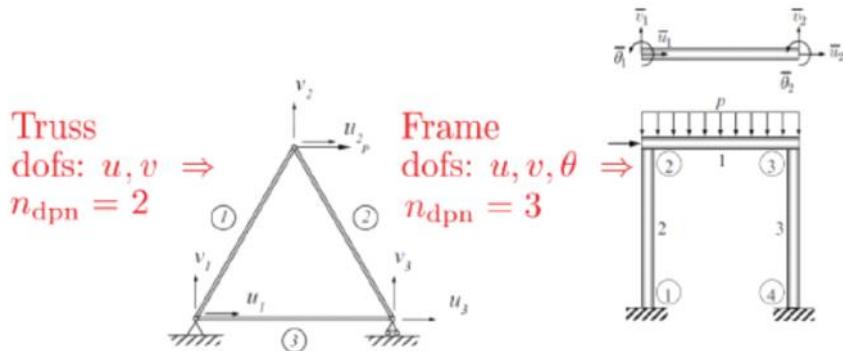
end
end

```

end
end

```

Step 9: Set element dofs a^e : Simplified limited case



Handwritten notes include:
 - A 3D coordinate system with axes labeled 1, 2, 3.
 - A 3x3 matrix for node 1 with values: $\begin{bmatrix} 0 & 1 & ? \\ 0 & 2 & ? \\ 1 & 1 & 0 \end{bmatrix}$.
 - A 6x6 global stiffness matrix K_{global} with circled entries: $\begin{bmatrix} 10.0 & 0 & 0 & 0 & 0 & 0 \\ 0.0 & 10.0 & 0 & 0 & 0 & 0 \\ 0.0 & 0.0 & 16.0 & 0 & 0 & 0 \\ 0.0 & 0.0 & 0 & 10.0 & 0 & 0 \\ 0.0 & 0.0 & 0 & 0 & 10.0 & 0 \\ 0.0 & 0.0 & 0 & 0 & 0 & 10.0 \end{bmatrix}$.
 - A note: "we need this".

$$f^e = K^e a^e$$

Steps 8&9

dofs = zeros(ndof) element dofs (edof) resized to number of element dofs and zeroed
ec dof = 1 dof counter for element

for en = 1: neNodes number of element nodes

gn = LEM(en) global node number for element node en

for endof = 1: ndofpn This number is fixed now, e.g., 2 for 2D trusses

if (node(gn).dof(endof).p == true) gndof = endof, we bypass some steps here
 dofs(ec dof) = node(gn).dof(endof).value; e dof val = corresponding global val
 end

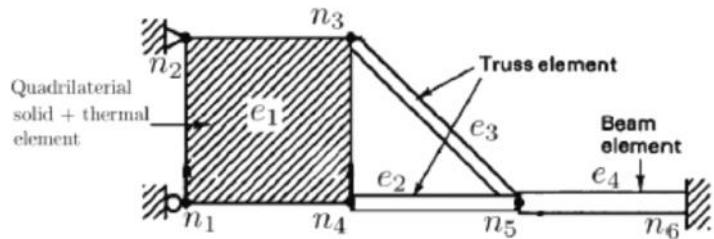
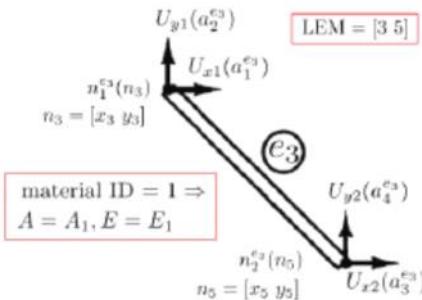
dofMap(ec dof) = node(gn).dof(endof).pos
 ec dof = ec dof + 1 increment counter

end

end

added for step 9
 a^e (dofs) is updated

Step 10: Compute element stiffness/force



Every element has its own implementation of stiffness calculation.

Parent class: PhyElement (this is a generic element)

```
class PhyElement
{
// Step 10: Compute element stiffness/force (ke, foe (fre: source term; fNe: Neumann BC))
virtual void Calculate_ElementStiffness_Force() = 0;
}
```

parent does not have
any implementation

Children (bar, beam, ..) may have different implementations

Child (subclass)

PhyElementBar.h

```
class PhyElementBar : public PhyElement
{
...
virtual void Calculate_ElementStiffness_Force();
}

void PhyElementBar::Calculate_ElementStiffness_Force()
{
    // compute stiffness matrix:
    ke.resize(2, 2);
    double factor = A * E / L;
    ke(0, 0) = ke(1, 1) = factor;
    ke(1, 0) = ke(0, 1) = -factor;
}
```

```
void PhyElementTruss::Calculate_ElementStiffness_Force()
{
    // compute stiffness matrix:
    ke.resize(4, 4);
    double factor = A * E / L;
    for (int i = 0; i < 2; ++i)
        for (int j = 0; j < 2; ++j)
```

$$K_0 = \frac{AE}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

```

double factor = A * E / L;
for (int I = 0; I < 2; ++I)
    for (int J = 0; J < 2; ++J)
    {
        double f2 = factor;
        if ((I + J) % 2 != 0)
            f2 = -factor;
        ke(2 * I, 2 * J) = c * c * f2;
        ke(2 * I + 1, 2 * J) = ke(2 * I, 2 * J + 1) = c * s * f2;
        ke(2 * I + 1, 2 * J + 1) = s * s * f2;
    }
    cout << "ke\n" << ke << endl;
}

```

$$K = \frac{AE}{L}$$

Subroutine ~~rate~~

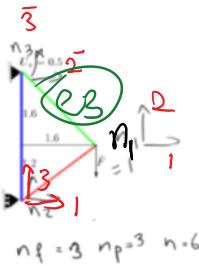
Calculate Stiffness()

```

{
    if (eType == 1) // bar
    {
        K = [ 1 -1 ]
        -1 1
    }
    else if (eType == 2)
    {
        S
    }
}

```

How do you get L, c, s for a truss element w/o a figure?

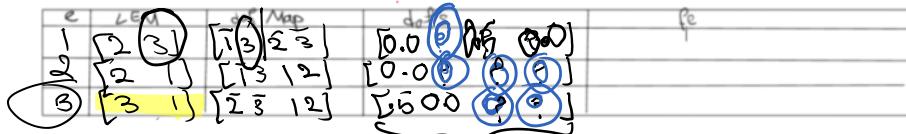


node	P	pos	V	F
1	0	1	?	0 ?
	0	2	?	-1.0 ?
2	1	1	0.0	0 ?
3	1	3	?	0 ?
	1	2	0.5	0 ?
3	1	3	0.0	0 ?

$$U_p = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

$$F_p = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

$$K_{\text{neqnf}} F_p = \begin{bmatrix} 0.0 \\ -1.0 \\ 0.0 \end{bmatrix}$$



we need this

Input file

...

nNodes 3

id crd

1 1.6 1.2

2 0.0

3 0.2.8

$$\cancel{e_3} \times \cancel{\text{node}(1)} - \text{card(nodes)}$$

$$= [1.6, 1.2] - [0, 2.8]$$

$$= [1.6, -1.6]$$

$$L_{e3} = \sqrt{(1.6)^2 + (1.6)^2}$$

$$\cos_{e3} = \frac{(De_3)(1)}{L} = \frac{1.6}{L} = \frac{\sqrt{2}}{2}$$

Step 11: Assembly from local to global system

Truss example: Assembly of global system

truss example

e_1	e_2	e_3
u_4, u_3 $U_3 = 0$ $U_1 = 0.5$ $c_1 \theta = 90^\circ$ $c = 0$ $s = 1$ u_2, U_3 $U_4, U_1 = 0$	u_4, u_3 $U_2 = 1.2$ $U_1 = 1.6$ $\theta = \tan^{-1}(\frac{1}{2})$ $c = 0.8$ $s = 0.6$	$U_3 = 0$ $U_2 = 0.5$ $\theta = -45^\circ$ $c = \frac{1}{\sqrt{2}}$ $s = -\frac{1}{\sqrt{2}}$ U_4, U_3 $U_2, U_1 = 0$
k_e $k_e e_1 = \frac{(1)(1)}{2.8} \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}$ $= \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0.3571 & 0 & -0.3571 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0.3571 \end{bmatrix}$	$k_e e_2 = \frac{(1)(1)}{2} \begin{bmatrix} 0.64 & 0.48 & -0.64 & -0.48 \\ 0.48 & 0.36 & -0.48 & -0.36 \\ -0.64 & -0.48 & 0.64 & 0.48 \\ -0.48 & -0.36 & 0.48 & 0.36 \end{bmatrix}$ $= \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0.32 & 0.24 & -0.32 & -0.24 \\ 0.24 & 0.18 & -0.24 & -0.18 \\ 1 & -0.32 & -0.24 & 0.32 \\ 2 & -0.24 & -0.18 & 0.24 \end{bmatrix}$	$k_e e_3 = \frac{(1)(1)}{1.6\sqrt{2}} \begin{bmatrix} 0.5 & -0.5 & 0.5 & 0.5 \\ -0.5 & 0.5 & 0.5 & -0.5 \\ 0.5 & 0.5 & 0.5 & -0.5 \\ 0.5 & -0.5 & -0.5 & 0.5 \end{bmatrix}$ $= \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0.221 & 0.221 & -0.221 & -0.221 \\ -0.221 & 0.221 & 0.221 & -0.221 \\ 0.221 & -0.221 & 0.221 & 0.221 \end{bmatrix}$
f_D^e $f_D^e = f_r^{e_1} + f_N^{e_1} - f_D^{e_1} = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$	f_r^e $f_r^e = f_r^{e_2} + f_N^{e_2} - f_D^{e_2} = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$	f_r^e $f_r^e = f_r^{e_3} + f_N^{e_3} - f_D^{e_3} = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$
f_e^e $f_e^e = f_r^{e_1} + f_N^{e_1} - f_D^{e_1} = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$	f_e^e $f_e^e = f_r^{e_2} + f_N^{e_2} - f_D^{e_2} = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$	f_e^e $f_e^e = f_r^{e_3} + f_N^{e_3} - f_D^{e_3} = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$

K &
F any
row is
prescribed
useless

- Numbers encircled in the computation of essential BC force are displacements corresponding to free dofs. As mentioned before, in reality we do not consider them in computation of this force, but in hand calculation we just put zero for those values.

323 / 456

Summary:

Prescribed rows \rightarrow useless

\Rightarrow

Only work with prescribed ROWS

Free column \rightarrow Stiffness is updated

else

Prescribed column \rightarrow



for $e = 1:ne$ loop over elements

fee = feo element total force = element all forces except essential force

for $i = 1:nedof$ loop over rows of ke; nedof = element # dof

I = dofMap(i) local to global dof map M_t^e

if ($I > 0$) I corresponds to a free dof, we skip prescribed dofs

for $j = 1:nedof$ loop over columns of ke

J = dofMap(j) global dof corresponding to j

if ($J > 0$) now both I and J are free and can add $ke(i, j)$ to global K

$K(I, J) = K(I, J) + ke(i, j)$

else $J < 0$, prescribed dof j; add contributions of $f_D^e = k^e a^e$ to f_e^e

$fee(i) = fee(i) - ke(i, j) * edofs(j)$ edofs: element dofs = a^e

end

end

$F(I) = F(I) + fee(i)$ element's total force fee component i'th is computed added to F(I)

```

for e = 1:ne loop over elements
    fee = feo element total force = element all forces except essential force
    for i = 1:nedof loop over rows of ke; nedof = element # dof
        I = dofMap(i) local to global dof map  $M_t^e$ 
        if (I > 0) I corresponds to a free dof, we skip prescribed dofs
            for j = 1:nedof loop over columns of ke
                J = dofMap(j) global dof corresponding to j
                if (J > 0) now both I and J are free and can add  $ke(i,j)$  to global K
                     $K(I, J) = K(I, J) + ke(i, j)$ 
                else J < 0, prescribed dof j; add contributions of  $f_D^e = k^e a^e$  to  $f_e^e$ 
                    fee(i) = fee(i) -  $ke(i, j) * edofs(j)$  edofs: element dofs =  $a^e$ 
                end
            end
            F(I) = F(I) + fee(i) element's total force fee component i'th is computed→added to F(I)
        end
    end
end

```

431 / 456