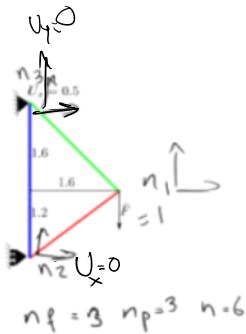


From last time

1

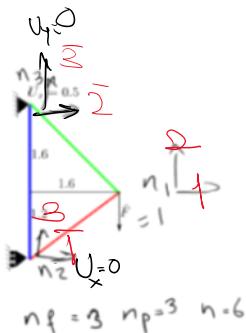


node	P	pos	V	f
1	0	0	0?	0
2	1	0	0?	0?
3	1	0.5	0.5	0?
	1	0.0	0.0	0?

$$\begin{aligned} U_f &= \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} & k_{np \times np} & F_n = \begin{bmatrix} \end{bmatrix} \\ \text{size } np & & F_p & = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} \end{aligned}$$

e	LEM	dof Map	dofs	fe

Steps 6 &amp; 7

Step 6: dof positions; Step 7: Set  $\mathbf{F}(\mathbf{F}_f)$ 

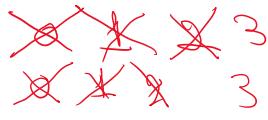
node	P	pos	V	f
1	0	1	0?	0
2	0	2	0?	0
3	1	1	0.0	0?
	0	3	0?	-1
3	1	2	0.5	0?
	1	3	0.0	0?

$$\begin{aligned} U_f &= \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} & k_{np \times np} & F_n = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \\ \text{size } np & & F_p & = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} \end{aligned}$$

e	LEM	dof Map	dofs	fe

free corner

prescribed corner



```
posf = 0, posp = 0
for n = 1:nNodes
```

```
for dof = 1: node(n).nndof num dof for node (n)
if node(n).ndof(dof).p == true prescribed dof
    posp = posp - 1;
    node(n).ndof(dof).pos = posp;
else free dof
```

in C++, Python  
dof positions shift from 0  
(in Fortran, Matlab) ~ 1

```

posf = 0, posp = 0
for n = 1:nNodes
    for dof = 1: node(n).nndof num dof for node (n)
        if node(n).ndof(dof).p == true prescribed dof
            posp = posp - 1;
            node(n).ndof(dof).pos = posp;
        else free dof
            posf = posf + 1;
            node(n).ndof(dof).pos = posf;
            F(posf) = node(n).ndof(dof).f
        end
    end
end

```

in Fortran, Matlab

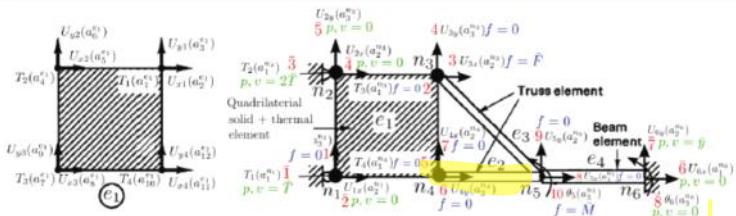
~ 1

end

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Step 8:  
Setting dofMap of elements

### Step 8: Element dof maps $M_t^e$



- As mentioned,  $M_t^e$  is a vector of size  $n_{\text{dof}}^e$  that maps elements dofs to global positions.
- For element 1, dofs are ordered as (loop over nodes, then loop over dofs for the node):

$$a_1^e = [a_1^{e_1} \quad a_2^{e_1} \quad \dots \quad a_{12}^{e_1}] \\ = [T_1 \quad U_{x1} \quad U_{y1} \mid T_2 \quad U_{x2} \quad U_{y2} \mid T_3 \quad U_{x3} \quad U_{y3} \mid T_4 \quad U_{x4} \quad U_{y4}]$$

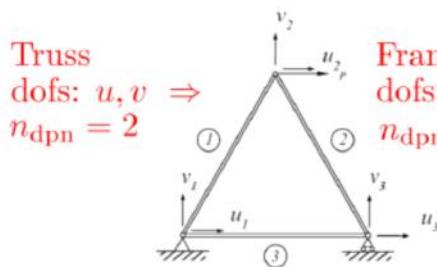
- We need to map these dofs to global dofs and have their position in  $M_t^e$  vector. For example, 1st dof of node 1 ( $a_1^{e_1} = T_1$ ) is mapped to first dof of  $n_3$  which has position 2.
- 2nd dof of node 3 ( $a_8^{e_1} = U_{y2}$ ) is mapped to 2nd dof of  $n_1$  which has position 2(-2).
- The map for element  $e_1$  is:

$$M^{e_1} = [2 \quad 3 \quad 4 \quad 3 \quad 4 \quad 5 \quad 1 \quad 2 \quad 1 \quad 5 \quad 6 \quad 7]$$

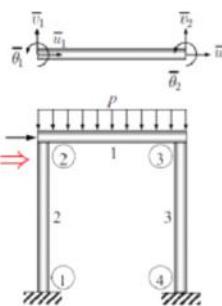
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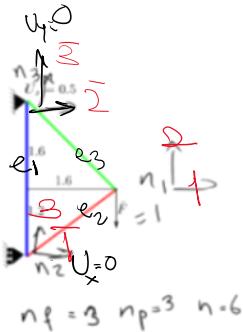
Not needed for the term project

### Step 8: Element dof maps $M_t^e$ : Simplified limited case



Frame  
dofs:  $u, v, \theta \Rightarrow n_{\text{dpn}} = 3$





node	P	pos	v	f
1	0	1	0?	0
	0	2	0?	0
2	1	1	0.0	0?
	0	3	0?	-1
3	1	2	0.5	0?
	1	3	0.0	0?

$$U_F = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

$$F_F = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

$$K_{np \times np} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$F_N = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

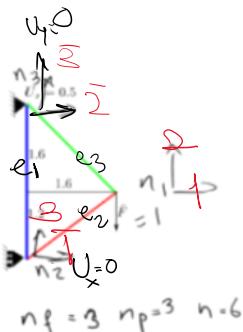
e	LEM	dof Map	dofs	fe
1	[2,3]	[1 3 2 3]		
2	[2,1]	[1 3 1 2]		
3	[3,1]	[2 3 1 2]		

Be careful with indices stored in dofMap, in C++ I subtract 1 from prescribed dofs. For example, for e2 without the subtraction, I would have had

0 2 0 1, this becomes -1, 2 0 1  
Similarly element 1 will have dofMap -1, 2, -2, -3

needed for  $f_{\text{D}}^e = K_e^e a^e$

#### Step 9: Set element dofs $a^e$



node	P	pos	v	f
1	0	1	0?	0
	0	2	0?	0
2	1	1	0.0	0?
	0	3	0?	-1
3	1	2	0.5	0?
	1	3	0.0	0?

$$U_F = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

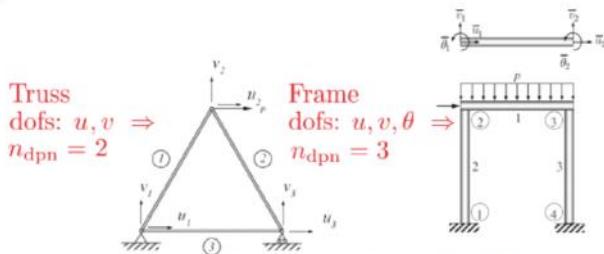
$$F_F = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

$$K_{np \times np} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$F_N = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

e	LEM	dof Map	dofs	fe
1	[2,3]	[1 3 2 3]	[0.0 0 .5 0]	
2	[2,1]	[1 3 1 2]	[0.0 0 0 0]	
3	[3,1]	[2 3 1 2]	[.5 0 0 0]	

## Step 9: Set element dofs $a^e$ : Simplified limited case



- Similar to steps 1, 2, and 8, step 9 can be greatly simplified if we assume all nodes share exactly the same set of dofs.

- Noting  $n_{dpn}$  ( $ndofpn$ ) = Number of dof. per node, simplified merged steps 8 & 9 are:  
dofs = zeros(ndof) element dofs (edof) resized to number of element dofs and zeroed  
ec dof = 1 dof counter for element

for en = 1: neNodes number of element nodes

```
gn = LEM(en) global node number for element node en
for endof = 1: ndofpn This number is fixed now, e.g., 2 for 2D trusses
  if (node(gn).dof(endof).p == true) gndof = endof, we bypass some steps here
    dofs(ecdof) = node(gn).dof(endof).value; e dof val = corresponding global val
  end
  dofMap(ecdof) = node(gn).dof(endof).pos
  ecdof = ecdof + 1 increment counter
end
end
```

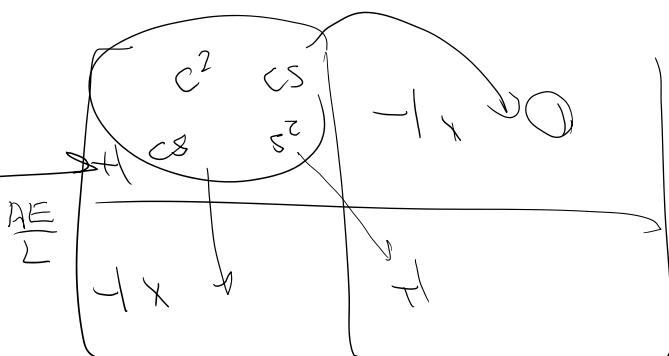
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## Step 10: Compute element stiffness/force

Example: Truss element

```
class PhyElementTruss : public PhyElement
{
public:
  virtual void setInternalMaterialProperties(PhyMaterial*
  pMat);
  virtual void Calculate_ElementStiffness_Force();
```

```
void PhyElementTruss::Calculate_ElementStiffness_Force()
{
  // compute stiffness matrix:
  ke.resize(4, 4);
  double factor = A * E / L;
  for (int I = 0; I < 2; ++I)
    for (int J = 0; J < 2; ++J)
    {
      double f2 = factor;
      if ((I + J) % 2 != 0)
        f2 = -factor;
      ke(2 * I, 2 * J) = c * c * f2;
      ke(2 * I + 1, 2 * J) = ke(2 * I, 2 * J + 1) = c * s * f2;
      ke(2 * I + 1, 2 * J + 1) = s * s * f2;
    }
  cout << "ke\n" << ke << endl;
}
```



We need to have a few things for this element

(@ A, E → Material properties)

⑥ L, C, S

⑦ A, E :

1 2 10 10000  
2 3 0.01 100 0.3

- In the sample data input, material refers to truss element material parameters  
 $A = 10, E = 10000$  while material 2 is for 2D solid with  
 $t(\text{thickness}) = 0.01, E = 100, \nu(\text{Poisson ratio}) = 0.3$ .
- At element level a matID refers to global {mats}; e.g.,

For  $e_3$ , matID = 1,  $\Rightarrow A = \{\text{mats}\}(1)(1) = 10, E = \{\text{mats}\}(1)(2) = 10000$  (450)

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eType = 1 : bar element	eType = 2 : beam element	(451)
eType = 3 : truss element	eType = 4 : frame element	(452)
eType = 5 : 2D thermal element	eType = 6 : 2D solid element	(453)

eType = 1	Bar	$\text{mat}\{en\} = [E \ A]$	(454a)
eType = 2	Beam	$\text{mat}\{en\} = [E \ I]$	(454b)
eType = 3	Truss	$\text{mat}\{en\} = [E \ A]$	(454c)
eType = 4	Frame	$\text{mat}\{en\} = [E \ A \ I]$	(454d)
eType = 5	2D thermal	$\text{mat}\{en\} = [\kappa \ t]$	(454e)
eType = 6	2D solid	$\text{mat}\{en\} = [E \ \nu \ t]$	(454f)

material #1

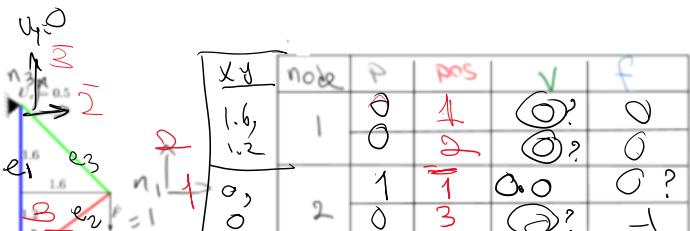
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Materials  
nMat 1  
id numPara Paras  
1 2 1 0 1 0  
2 3 0 0 1 0 1 0  
2 3 0 0 1 0 1 0

id elementType matID neNodes eNodes  
1 3 1 2 2 3  
2 3 1 2 2 1  
3 3 1 2 3 1

⑧ L, C, S

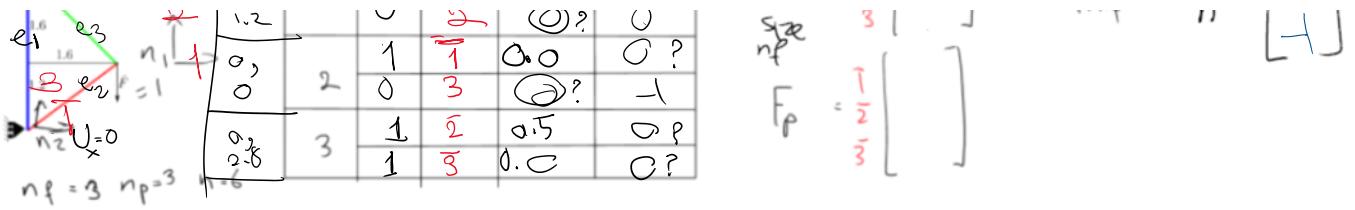
How do we calculate these?



$$U_F = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

$$K_{\text{frame}} = \begin{bmatrix} 1 & 2 & 3 \\ 2 & 1 & 3 \\ 3 & 3 & 1 \end{bmatrix}$$

$$F_N = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$



e	LEM	def Map	def S	fe
1	[2,3]	[1 3 2 3]	[0.0 0 0]	
2	[2,1]	[1 3 1 2]	[0.0 0 0]	
3	[3,1]	[2 3 1 2]	[0.5 0 0]	

LEM

$e_2$  node(1)  $\rightarrow$  2 crd 0,0  
 node(2)  $\rightarrow$  1 crd 1.6,1.2

Diagram of a truss element with nodes at  $(1.0, 1.2)$  and  $(0.0, 0.0)$ . The length  $L$  is calculated as:

$$L = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2}$$

$$C = \frac{x_1 - x_0}{L} \quad S = \frac{y_1 - y_0}{L}$$

First, we add the extra data for each particular element type:

```
class PhyElementTruss : public PhyElement
{
public:
    virtual void setInternalMaterialProperties(PhyMaterial* pMat);
    virtual void Calculate_ElementStiffness_Force();

    virtual void SpecificOutput(ostream& out) const;

    double L;
    double A;
    double E;
    double c;
    double s;
};
```

```
void PhyElementTruss::setInternalMaterialProperties(PhyMaterial* pMat)
```

```
{
    A = pMat->paras(mpb_A);
    E = pMat->paras(mpb_E);
}
```

```
void PhyElementTruss::setGeometry()
```

```
{
    VECTOR *crd0, *crd1;
    crd1 = &eNodePtrs[1]->coordinate;
    crd0 = &eNodePtrs[0]->coordinate;
```

```
int sz = crd1->size();
```

```

if (sz != 2)
    THROW("implementation only for 2D truss");
double delX, delY;
delX = (*crd1)(0) - (*crd0)(0);
delY = (*crd1)(1) - (*crd0)(1);
L = sqrt(delX * delX + delY * delY);
c = delX / L;
s = delY / L;
}

```

Non-object oriented calculation of stiffness matrix

if ( $\text{type} == 1$ )  $\rightarrow$  bar

$$k = \frac{AE}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

elseif ( $\text{type} == 2$ )  $\rightarrow$  beam

$$k : \begin{bmatrix} & & & \\ & & & \\ & & & \\ & & & \end{bmatrix} \quad 4 \times 4$$

or  
cases

### Step 11: Assembly from local to global system

# Truss example: Assembly of global system

$e$	$e_1$	$e_2$	$e_3$
	$\begin{matrix} u_4 & u_3 \\ u_3 & 0 \\ U_3 = 0 \\ U_2 = 0.5 \\ \theta = 90^\circ \\ c = 0 \\ s = 1 \\ u_2 & u_3 \\ u_2 + U_1 = 0 \end{matrix}$	$\begin{matrix} u_4 & u_3 \\ u_3 & 1.2 \\ u_2 & u_1 \\ L = \sqrt{2} \\ \theta = \tan^{-1}(\frac{3}{4}) \\ c = 0.8 \\ s = 0.6 \\ U_3 = 0 \\ U_1 = 0 \end{matrix}$	$\begin{matrix} u_2 & u_1 \\ u_2 & 1.6 \\ u_3 & u_4 \\ L = 1.6\sqrt{2} \\ \theta = -45^\circ \\ c = \frac{1}{\sqrt{2}} \\ s = -\frac{1}{\sqrt{2}} \\ U_3 = 0 \\ U_2 = 0.5 \\ U_1 = 0.5 \end{matrix}$
$k_e$	$k^{e_1} = \frac{(1)(1)}{2.8} \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}$	$k^{e_2} = \frac{(1)(1)}{2.8} \begin{bmatrix} 0.64 & 0.48 & -0.64 & -0.48 \\ 0.48 & 0.36 & -0.48 & -0.36 \\ -0.64 & -0.48 & 0.64 & 0.48 \\ -0.48 & -0.36 & 0.48 & 0.36 \end{bmatrix}$	$k^{e_3} = \frac{(1)(1)}{1.6\sqrt{2}} \begin{bmatrix} 0.5 & -0.5 & 0.5 & 0.5 \\ -0.5 & 0.5 & 0.5 & 0.5 \\ 0.5 & 0.5 & 0.5 & 0.5 \\ 0.5 & -0.5 & 0.5 & 0.5 \end{bmatrix}$
	$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0.3571 & 0 & -0.3571 & 0 \\ 0 & 0.3571 & 0 & -0.3571 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0.3571 \end{bmatrix}$	$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0.24 & 0.18 & -0.24 & -0.18 \\ 0.24 & 0.18 & -0.24 & -0.18 \\ -0.32 & -0.24 & 0.32 & 0.24 \\ -0.24 & -0.18 & 0.24 & 0.18 \end{bmatrix}$	$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0.221 & 0.221 & -0.221 & -0.221 \\ 0.221 & 0.221 & -0.221 & -0.221 \\ -0.221 & -0.221 & 0.221 & 0.221 \\ -0.221 & -0.221 & 0.221 & 0.221 \end{bmatrix}$
$f_D^e$	$f_e^{e_1} = f_{r^e}^{e_1} + f_N^{e_1} - f_D^{e_1} = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$	$f_e^{e_2} = f_{r^e}^{e_2} + f_N^{e_2} - f_D^{e_2} = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$	$f_e^{e_3} = f_{r^e}^{e_3} + f_N^{e_3} - f_D^{e_3} = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$
$f_e^e$	$f_e^e = f_e^{e_1} + f_e^{e_2} - f_e^{e_3} = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$	$f_e^e = f_{r^e}^e + f_N^e - f_D^e = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$	$f_e^e = f_{r^e}^e + f_N^e - f_D^e = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$
		$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0.32+0.221 & 0.24-0.221 & -0.24 & -0.24 \\ 0.24-0.221 & 0.18+0.221 & 0.18 & -0.18 \\ -0.24 & 0.18 & 0.24 & 0.18 \\ -0.24 & -0.18 & 0.24 & 0.18 \end{bmatrix} = \begin{bmatrix} 0.5410 & 0.019 & -0.24 & -0.24 \\ 0.019 & 0.401 & 0.18 & -0.18 \\ -0.24 & 0.5371 & -0.1105 & 0.1105 \\ -0.24 & -0.1105 & 0.1105 & -0.1105 \end{bmatrix}$	$K = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0.1105 & 0 & 0 & 0 \\ 0 & 0.1105 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \Rightarrow U = K^{-1}F = \begin{bmatrix} U_1 \\ U_2 \\ U_3 \end{bmatrix} = \begin{bmatrix} -0.2123 \\ -3.2980 \\ -1.200 \end{bmatrix}$

row column  
only  $f_f$  components of  
 $K_e$  go to  $K$  (global)  
which one contribute to  $f_D^e$

only  $f_f$  matters  
 $f_f$   
 $f_p$   
 $p_f$   
 $pp$

$f_f$   
 $K^e$   
 $F^e$   
 $F_D^e$

- Numbers encircled in the computation of essential BC force are displacements corresponding to free dofs. As mentioned before, in reality we do not consider them in computation of this force, but in hand calculation we just put zero for those values.

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Function  
(rows) for  $i = 1 : n_{\text{dof}}$  #  $e \text{ dof}$   
 $I = \text{dofMap}(i)$   
if  $I < 0$       / row is prescribed  
  continue;  
end  
  
(columns) for  $j = 1 : n_{\text{dof}}$       ↓ free rows  
   $J = \text{dofMap}(j)$   
  if  $J > 0$       free columns  
     $K(I, J) = K(I, J) + k_e(i, j)$  ff  
  else      (  $J < 0$  )  
     $f_D(i) = f_D(i) + k_e(i, j) + a_e(j);$  fp case  
  end

```

    end
    fee(i) = fee(i) - fed(i)
    F(I) = F(I) + fee(i)
end

```

## Step 11: Assembly from local to global system

- $K$  and  $F$  (global stiffness and force) are already sized and set to zero.
- Element level (local) stiffness and force is calculated (Step 10).
- Element local to global dof  $M_t^e$  is already set (Step 8).
- Using dof map, we assemble local values to global values.
- Clearly, only free dofs are added to stiffness matrix and force vector.
- Element dof values (dofs:  $a^e$  is also set (Step 9).
- $f_D^e = k^e a^e$  may not need to be formed and can be directly added to  $f_e^e$ .

for  $e = 1:ne$  loop over elements

```

fee = feo element total force = element all forces except essential force
for i = 1:nedof loop over rows of ke; nedof = element # dof
    I = dofMap(i) local to global dof map  $M_t^e$ 
    if (I > 0) I corresponds to a free dof, we skip prescribed dofs
        for j = 1:nedof loop over columns of ke
            J = dofMap(j) global dof corresponding to j
            if (J > 0) now both I and J are free and can add ke(i,j) to global K
                K(I, J) = K(I, J) + ke(i, j)
            else J < 0, prescribed dof j; add contributions of  $f_D^e = k^e a^e$  to  $f_e^e$ 
                fee(i) = fee(i) - ke(i, j) * edofs(j) edofs: element dofs =  $a^e$ 
            end
        end
        F(I) = F(I) + fee(i) element's total force fee component i'th is computed→added to F(I)
    end
end
end

```

## Step 11: Assembly from local to global system

- **Rows:** In loop over edof (element dofs) we skip prescribed dofs i.
- **Columns:** free columns j: Stiffness is assembled  
 $K(I, J) = K(I, J) + ke(i, j)$ .
- **Columns:** prescribed columns j:  $f_D^e$  is added to total element force  
 $f_e^e: f_{\text{ee}}(i) = f_{\text{ee}}(i) - ke(i, j) * \text{edofs}(j)$ .
- **Force:** Once  $f_{\text{ee}}$  is updated with  $f_{\text{de}}$  (essential BD force), it is assembled to global F:  $F(I) = F(I) + f_{\text{ee}}(i)$ .
- **Both K and k are symmetric:**
  - ① K can be stored into a symmetric matrix → almost half the storage.
  - ②  $ke$  symmetric: can be stored in symmetric matrix → almost half the storage.
  - ③  $ke$  symmetric: half the loop computation: instead of looping (i: 1 → nedof; j: 1 → nedof) we can loop (i: 1 → nedof; j: i → nedof).  
How?

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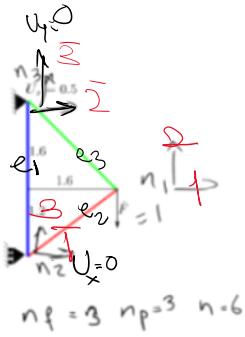
## Step 12: Solve global (free) dof a from $Ka = F$

- Two major computational costs during FEM solve are:
  - ① **Assembly:** Refers to: all node, element, and dof set up; computation of local  $ke$  and  $fe$ ; assembly of those to global system. This step scales linearly versus  $n_e$  ( $ne$ )
  - ② **Linear algebra solution:**  $Ka = F$ : We solve for unknown a. Although conceptually simple, this step is a major source of computational cost. It scales higher than linear versus  $n_e$  ⇒ As the problem size increases this term becomes more dominant.
- Solution of  $Ka = F$ :
  - WE DO NOT OBTAIN a from  $a = K^{-1}F$ : We do not invert K.
  - We only solve the problem for the specific RHS of F.
  - In Comparison  $K^{-1}$  corresponds to the solution of  $Ka = F$  for  $n_f$  RHS of  $F = e_i, i = 1, \dots, n_f$  where  $n_f$  is the number of rows (and columns) of K.
  - We employ methods such as LU factorization that computationally only solve the problem for the given RHS F.
  - We take advantage of the structure of stiffness matrix: symmetry, bandedness, sparsity in choosing the right solution technique.
  - order of free dofs affects band of the matrix → various algorithms reorder free dofs such that the matrix band get smaller and the solution cost is optimized.
  - In your term projects you can simply employ simply compute

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$$a \leftarrow K^{-1}F \quad \xrightarrow{\text{or}} \quad K \setminus F$$

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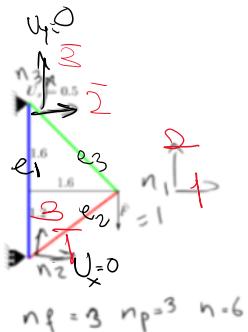
node	P	pos	v	f
1	0	1	0	0
	0	2	0	0
2	1	1	0	?
	0	3	0	-1
3	1	2	0.5	0
	1	3	0.0	0

$$\begin{aligned} U_F &= \begin{bmatrix} 1 & -2123 \\ 2 & -3.29 \\ 3 & -1.2 \end{bmatrix} \\ \text{size}_F &= \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} \\ F_F &= \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} \end{aligned}$$

$$K_{\text{neqnf}} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

e	LEM	dof Map	dofs	fe
1	[2,3]	[1 3 2 3]	[0.0 0.5 0]	
2	[2,1]	[1 3 1 2]	[0.0 0.0 0.0]	
3	[3,1]	[2 3 1 2]	[-0.5 0 -2123 -3.29]	

### Step 13: Assign a to nodes and elements



node	P	pos	v	f
1	0	1	-2123	0
	0	2	-3.29	0
2	1	1	0.0	?
	0	3	-1.2	-1
3	1	2	0.5	0
	1	3	0.0	0

$$\begin{aligned} U_F &= \begin{bmatrix} 1 & -2123 \\ 2 & -3.29 \\ 3 & -1.2 \end{bmatrix} \\ \text{size}_F &= \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} \\ F_F &= \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} \end{aligned}$$

$$K_{\text{neqnf}} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

e	LEM	dof Map	dofs	fe
1	[2,3]	[1 3 2 3]	[0.0 -1.2 0]	
2	[2,1]	[1 3 1 2]	[0.0 -1.2 -2123 -3.29]	
3	[3,1]	[2 3 1 2]	[-0.5 0 -2123 -3.29]	

for  $n = 1:n\text{Nodes}$

```

for dof = 1: node(n).nndof num dof for node (n)
    if node(n).ndof(dof).p == false free dof
        posn = node(n).ndof(dof).pos position of dof in global free F
        node(n).ndof(dof).v = dofs(posn) set free dof val to corresponding val in global dofs (a)      Node a,
    end
end
end

```

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```

for e = 1:ne loop over elements
  for i = element(e).nedof loop over element dofs; nedof = # dof ( $n_{dof}^e$ )
    posn = element(e).dofMap(i) corresponding global position using dofMat ( $M_t^e$ )
    if (posn > 0) free dof
      element(e).edofs(i) = dofs(posn)
      set free element dof  $a^e$  to corresponding val in global dofs (a)
    end
  end
end

```

element ↗

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