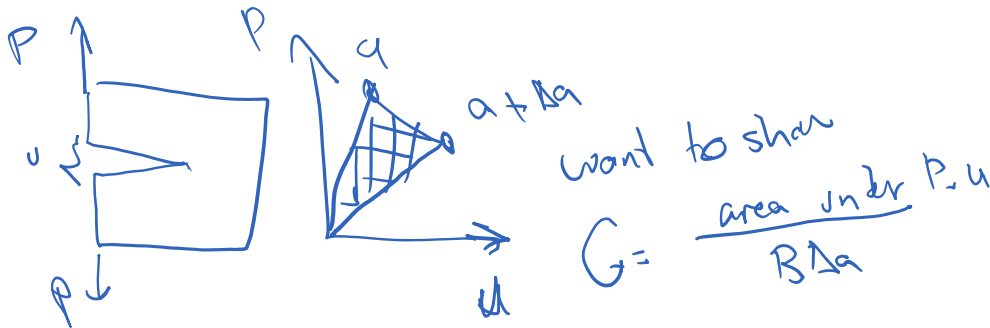


Continuing from the last time

- The condition G (energy release rate) = R (resistance) is needed for crack propagation.
- There are several methods to calculate G based on given data.
- One of those is when we have a P versus u (displacement) system.



We first show this for two simple loading cases:

A) Fixed grip:

$$U_1 = \frac{1}{2} P_1 u$$

$$U_2 = \frac{1}{2} P_2 u$$

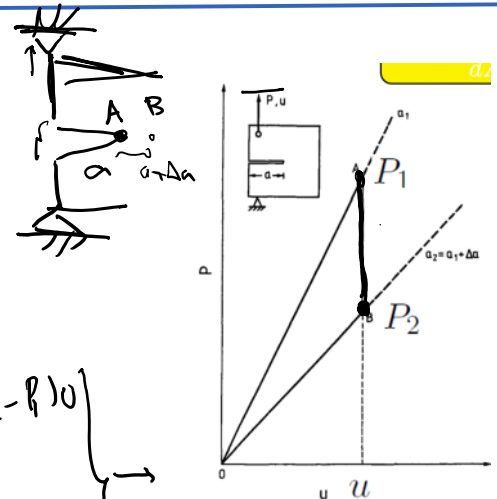
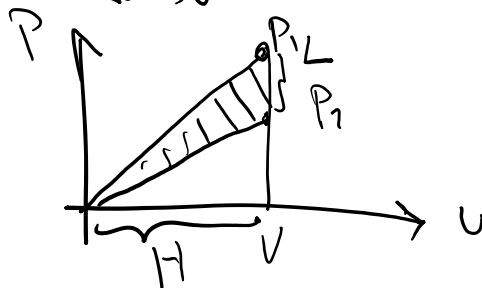
$$\Delta U_e \text{ change of internal energy} = \frac{1}{2} P_2 u - \frac{1}{2} P_1 u = \frac{1}{2} (P_2 - P_1) u$$

$$\Delta W \text{ change of external work} = 0$$

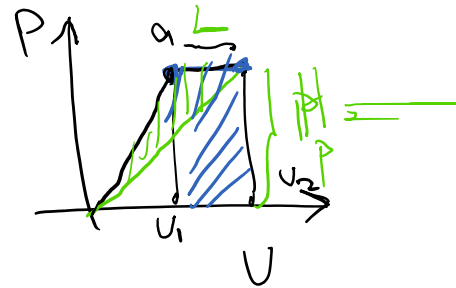
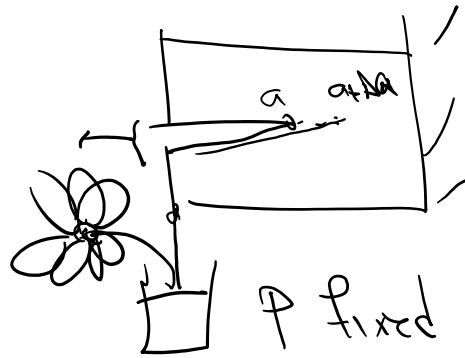
$$G = -\frac{d\Pi}{dA} = \lim_{\Delta a \rightarrow 0} \frac{(\Delta U_e - \Delta W)}{\Delta A}$$

$$\lim_{\Delta a \rightarrow 0} \frac{\frac{1}{2} (P_2 - P_1) u}{B \Delta a}$$

$$= \lim_{\Delta a \rightarrow 0} \frac{\frac{1}{2} (P_1 - P_2) u}{B \Delta a}$$



Other simple case:
B) Dead load



like before $U_1 = \frac{1}{2} P u_1$, $U_2 = \frac{1}{2} P u_2 \rightarrow \Delta U = \frac{1}{2} P (u_2 - u_1)$

$$\Delta W = \int_1^2 P du = P (u_2 - u_1)$$

$$G = \frac{-\Delta \Pi}{\Delta A \rightarrow 0} = \frac{-\Delta U + \Delta W}{\Delta A} = \frac{-\frac{1}{2} P (u_2 - u_1) + P (u_2 - u_1)}{B \Delta a}$$

$$\frac{1}{2} \frac{P (u_2 - u_1)}{B \Delta a}$$

Finally, we do this for the most general case:

$$\Delta \Pi = \Delta U_e - \Delta W$$

$$\Delta U_e = U_2 - U_1$$

$$= \frac{1}{2} P_2 u_2 - \frac{1}{2} P_1 u_1$$

$$\Delta W = \int_{u_1}^{u_2} P(u) du$$

force displacement
increment

$$\approx (u_2 - u_1) \left\{ \frac{1}{2} (P_1 + P_2) \right\}$$

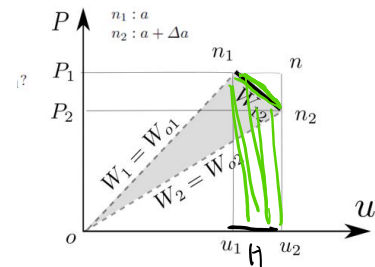
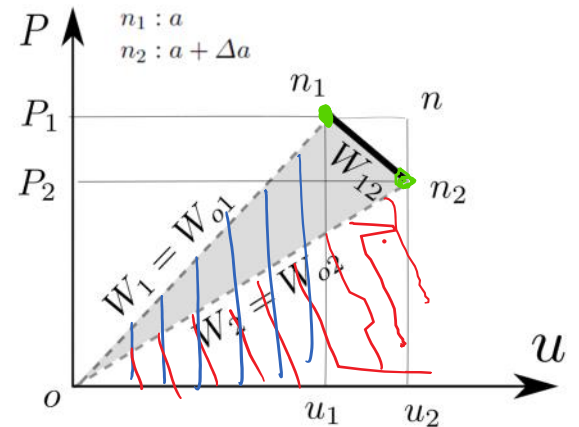
$$\Delta \Pi = \Delta U_e - \Delta W =$$

$$\frac{1}{2} P_2 u_2 - \frac{1}{2} P_1 u_1 - (u_2 - u_1) \left\{ \frac{1}{2} (P_1 + P_2) \right\}$$

$$= \frac{1}{2} P_2 u_2 - \frac{1}{2} P_1 u_1 - \frac{1}{2} P_1 u_2 - \frac{1}{2} P_2 u_2 + \frac{1}{2} P_1 u_1 + \frac{1}{2} P_2 u_1$$

$$\Delta \Pi = -\frac{1}{2} (P_1 u_2 - P_2 u_1)$$

$$\hookrightarrow -\Delta \Pi = \Delta \Pi$$



Algebraic

$$G = \frac{1}{2} \frac{(P_1 u_2 - P_2 u_1)}{B \Delta a}$$

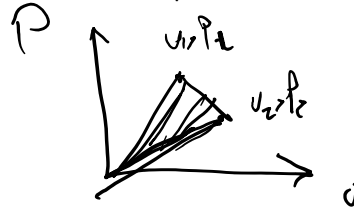


$$G = -\frac{\Delta T}{\Delta A} = \frac{\Delta T}{B \Delta a} \rightarrow$$

$$G = \frac{\sum (u_i^2 - u_i)}{B \Delta a}$$

Simple relation to calculate G from a pair of u and P measurements; useful for HW1, problem 2

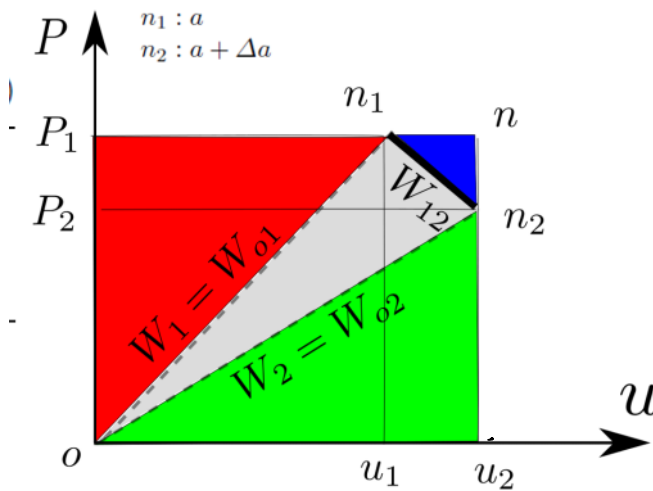
But why $\frac{1}{2}(P_2 u_2 - P_1 u_1)$ is equal to the shaded area?



From the above derivation, we had:

$$\Delta T = \Delta U_e - \Delta w = \frac{1}{2} R_2 u_2 - \frac{1}{2} R_1 u_1 - (u_2 - u_1) \left\{ \frac{1}{2} (R_1 + R_2) \right\}$$

We continue from here:

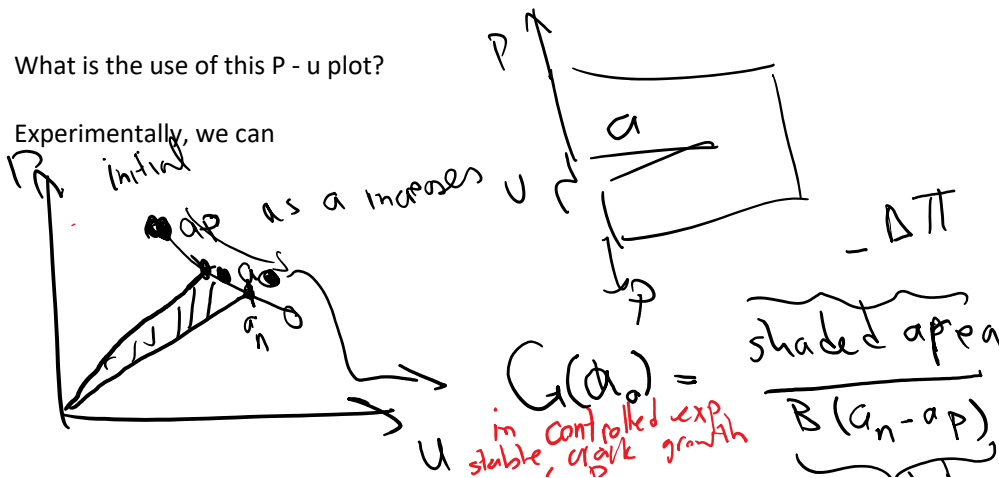


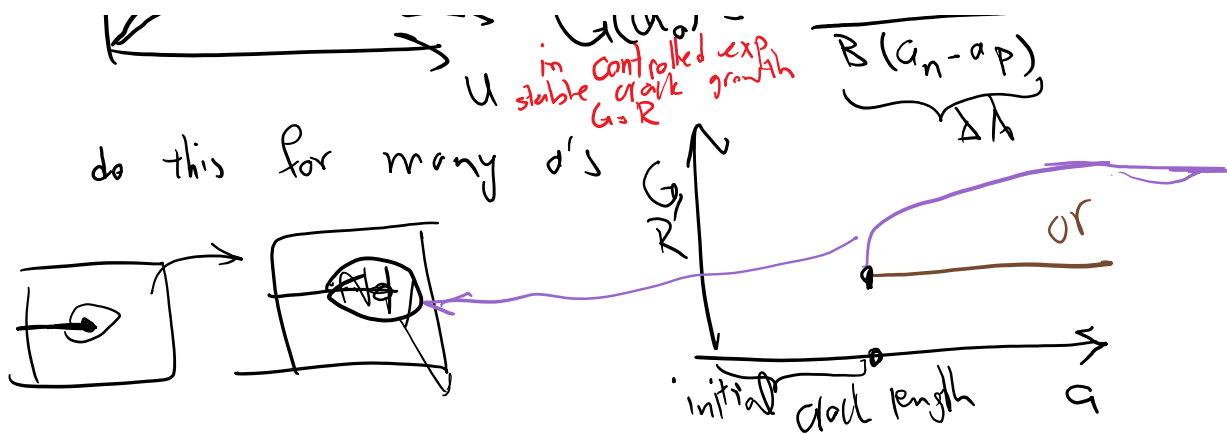
so in fact $-\Delta T$ is the shaded area "usual interpretation"

$$G = \frac{1}{B \Delta a} \left(P_1 u_2 - \frac{P_1 u_1}{2} - \frac{P_2 u_2}{2} - \frac{(P_1 - P_2)(u_2 - u_1)}{2} \right) = \frac{\text{Grey area}}{B \Delta a}$$

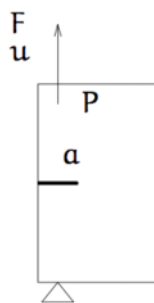
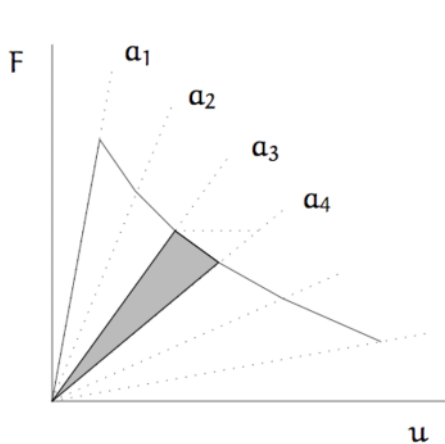
What is the use of this P - u plot?

Experimentally, we can





This plastic region around it can get to an almost the same size after some crack propagation.

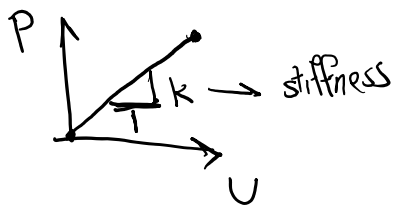


$$G(a_3) = \frac{1 \text{ shaded area}}{B (a_4 - a_3)}$$

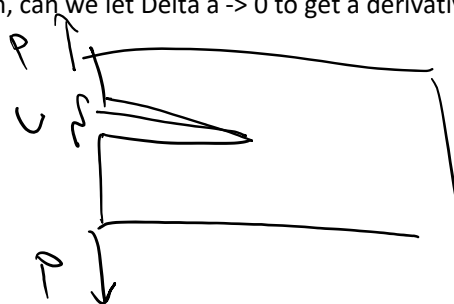
89

So, instead of this Finite Difference approximation, can we let $\Delta a \rightarrow 0$ to get a derivative expression for G ?

fixed a



$$P = k u$$




$$u = \frac{1}{k} P$$

compliance

$$U = CP$$

We want to get the derivative expression for G as $\Delta a \rightarrow 0$

Case A) Fixed grip
U is fixed



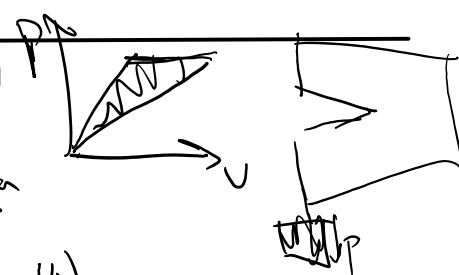
$$G = \frac{\text{shaded area}}{B \Delta a} = \frac{\frac{1}{2}(P_1 + P_2)U}{B \Delta a}$$

$$= \frac{\Delta \left(\frac{U}{C} \right) U}{2 B \Delta a} = \frac{-d \frac{U^2}{2C}}{2 B \Delta a} = -\frac{U^2}{2B} \frac{dC}{da}$$

U is constant \rightarrow goes out of derivative

$$= \frac{U^2}{2B} \left(-\frac{1}{C^2} \frac{dC}{da} \right) = \frac{1}{2B} \left(\frac{U}{C} \right)^2 \frac{dC}{da} = \frac{P^2}{2B} \frac{dC}{da}$$

Case B) Dead load



$$G = \frac{\text{shaded area}}{B \Delta a} = \frac{\frac{1}{2} P (U_2 - U_1)}{B \Delta a}$$

$$= \frac{\frac{1}{2} \Delta P (U_2 - U_1)}{B \Delta a} = \frac{P}{2B} \frac{U_2 - U_1}{\Delta a}$$

$\Delta a \rightarrow 0$ P is fixed

$$= \frac{P}{2B} \frac{dU}{da} = \frac{P}{2B} \frac{d(CP)}{da}$$

but P is fixed

$$= \frac{P^2}{2B} \frac{dC}{da}$$

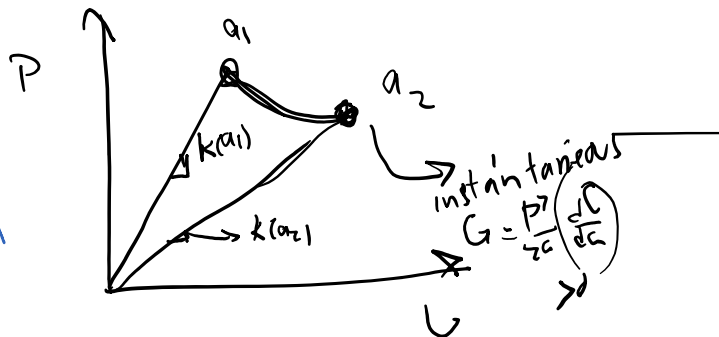
So, whether we have fixed grip (u fixed) or dead load (P fixed), the differential expression for G is



$$G = \frac{P^2}{2B} \frac{dC}{da} \quad C \text{ is compliance}$$

In fact, this is true even for more general loading

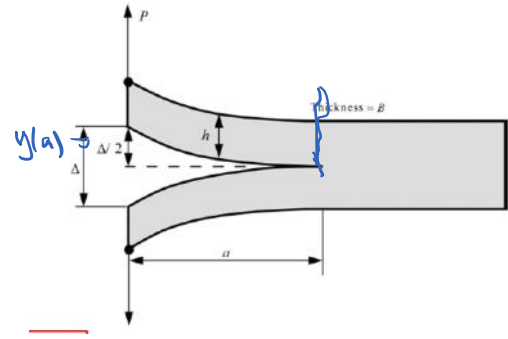
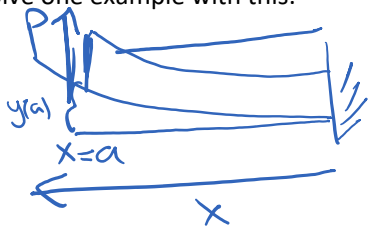
Hint use
 $G \approx \frac{1}{2} \frac{(P_1 U_2 - P_2 U_1)}{\Delta a}$
 or other hint in the assignment



How do we use this equation?

We are going to solve one example with this:

$$y(a) = \frac{Pa^3}{3EI}$$



$$\frac{\Delta}{2} = \frac{Pa^3}{3EI} \rightarrow \Delta = \frac{2}{3} \frac{Pa^3}{EI} \quad (1)$$

From here in fact we can calculate the compliance and from that compute G:

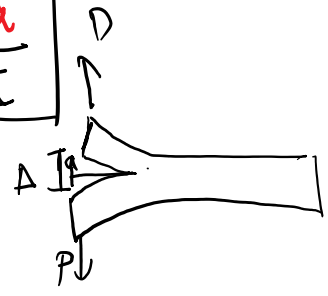
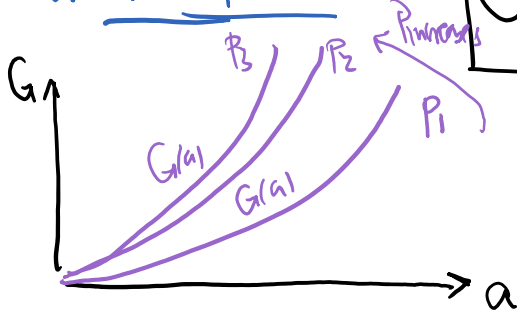
$$\frac{\delta}{\Delta} = CP \rightarrow C = \frac{\Delta}{P} = \frac{2/3 Pa^3/EI}{P} \rightarrow C = \frac{2a^3}{3EI} \quad (2)$$

↑ does not depend on P

$$G = \frac{P^2}{2B} \frac{dC}{da} = \frac{P^2}{2B} \frac{d(2/3 a^3/EI)}{da} = \frac{P^2}{2B} \frac{2}{3} \times \frac{3a^2}{EI}$$

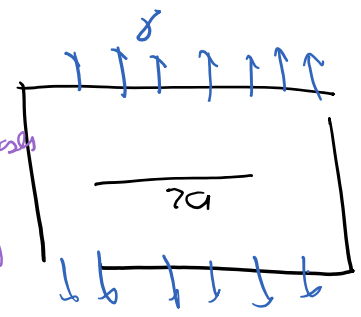
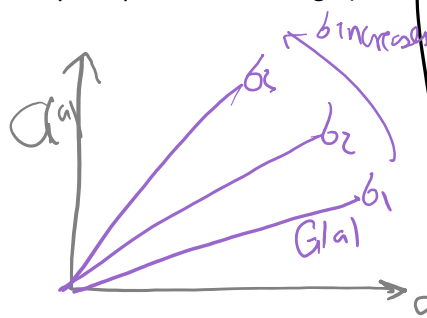
for this problem

$$G = \frac{Pa^2}{EI}$$



G increases as a^2 versus a (relatively fast pace of increasing G)

$$G = \frac{\pi b \delta^2 a}{E}$$



When does the crack grow?

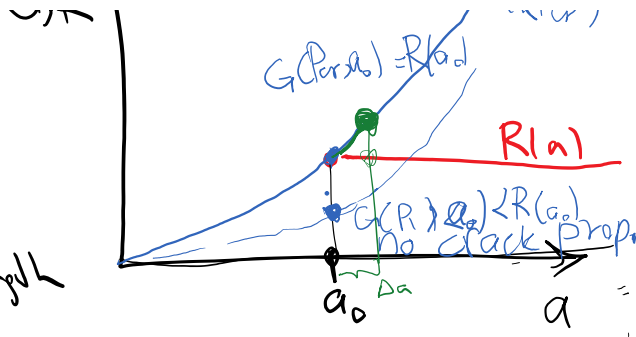
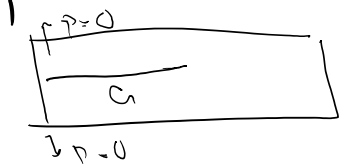


G, R ↑

$$G(P, a) = R(a) \quad G(P, a_c)$$



a_0 initial crack length



$$R < P_{cr}$$

$$G(a_0) = R(a_0)$$

$$G(a_0 + \Delta a) \geq R(a_0 + \Delta a)$$

let $\Delta a \rightarrow 0$

$$\frac{G(a_0 + \Delta a) - G(a_0)}{\Delta a} \geq \frac{R(a_0 + \Delta a) - R(a_0)}{\Delta a}$$

necessary for crack propagation	$G = R$
crack can unstably propagate	$\frac{dG}{da} > \frac{dR}{da}$

