

J integral: 2. EDI: Derivation

Divergence theorem: Line/Surface (2D/3D) integral **Surface/Volume Integral**

Application in FEM meshes

Original J integral contour

Surface integral after using divergence theorem

- Contour integral added to create closed surface
- By using $q=0$ this integral in effect is zero

$\Gamma_o \rightarrow 0$ → 2D mesh covers crack tip

$$\bar{J} = \int_{\Gamma_o} \left[(\omega + T) \delta_{ij} - \sigma_{ij} \frac{\partial u_j}{\partial x_i} \right] n_i d\Gamma$$

on Γ_o $q(x) = 1$ will be $q=0$ on Γ_i

$$-\bar{J} = \int_{\Gamma_o} \left[(\omega + T) \delta_{ij} - \sigma_{ij} \frac{\partial u_j}{\partial x_i} \right] m_i q d\Gamma + \int_{\Gamma_i} \pm m_i q d\Gamma$$

+ $\int_{\Gamma_i} \pm m_i q d\Gamma$ $\int_{\Gamma_i} \pm m_i q d\Gamma$

$$= \int_{A^*} \left[(\omega + T) \delta_{ij} - \sigma_{ij} \frac{\partial u_j}{\partial x_i} \right] q m_i dA$$

Use Gauss theorem

$$= -\bar{J} + \int_{\Gamma_i} \left[(\omega + T) \delta_{ij} - \sigma_{ij} \frac{\partial u_j}{\partial x_i} \right] q m_i d\Gamma$$

$$\bar{J} = \int_{A^*} \left[\sigma_{ij} \frac{\partial u_j}{\partial x_i} - (\omega + T) \delta_{ij} \right] q dV + \int_{\Gamma_i} \left[(\omega + T) \delta_{ij} - \sigma_{ij} \frac{\partial u_j}{\partial x_i} \right] q m_i d\Gamma$$

let $\Gamma_o \rightarrow 0$

Application in FEM meshes

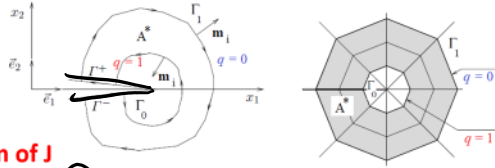
Application in FEM meshes

crack surface contribution

$$J = \int_{A^*} \frac{\partial}{\partial x_i} \left[\left[\sigma_{ij} \frac{\partial u_j}{\partial x_i} - w \delta_{ij} \right] q \right] dA - \int_{\Gamma_i} \sigma_{2j} \frac{\partial u_j}{\partial x_1} q d\Gamma$$

$$J = \int_{A^*} \frac{\partial}{\partial x_i} \left[\left(\sigma_{ij} \frac{\partial u_j}{\partial x_i} - w \delta_{ii} \right) q \right] dA - \int_{\Gamma_+ \cup \Gamma_-} \sigma_{2j} \frac{\partial u_j}{\partial x_1} q d\Gamma$$

$$\underbrace{\frac{\partial}{\partial x_i} \left(\sigma_{ij} \frac{\partial u_j}{\partial x_i} - w \delta_{ii} \right) q}_{\text{Often is zero}} + \left(\sigma_{ij} \frac{\partial u_j}{\partial x_i} - w \delta_{ii} \right) \frac{\partial q}{\partial x_i}$$



General form of J

$$J = \int_{A^*} \left\{ \left[\sigma_{ij} \frac{\partial u_j}{\partial x_i} - w \delta_{ii} \right] \frac{\partial q}{\partial x_i} + \left[\sigma_{ij} \frac{\partial \epsilon_{ij}^p}{\partial x_i} - \frac{\partial w^p}{\partial x_i} + \alpha \sigma_{ii} \frac{\partial \Theta}{\partial x_i} - F_i \frac{\partial u_j}{\partial x_i} \right] q \right\} dA - \int_{\Gamma_+ \cup \Gamma_-} \sigma_{2j} \frac{\partial u_j}{\partial x_1} q d\Gamma$$

Plasticity effects
Thermal effects
Body force

Nonzero crack surface traction

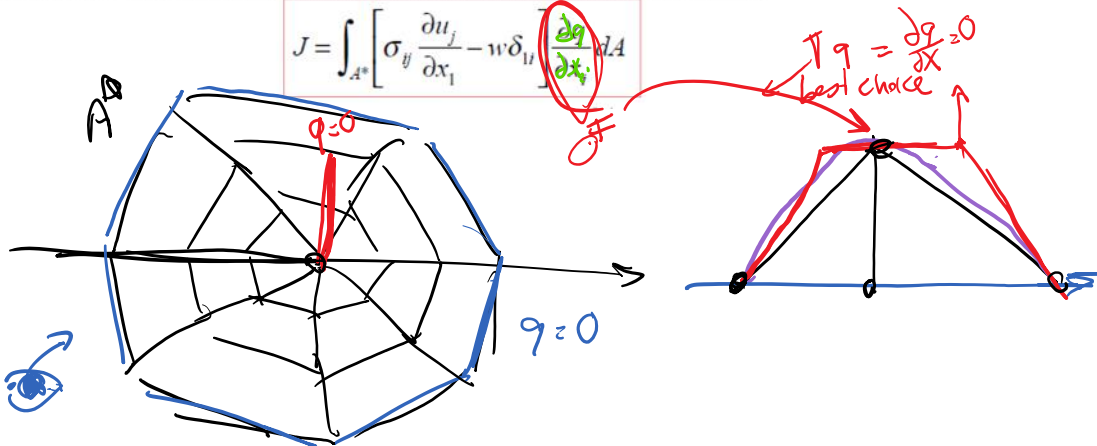
often these terms are zero

many problem these go away

Simplified Case:

(Nonlinear) elastic, no thermal strain, no body force, traction free crack surfaces

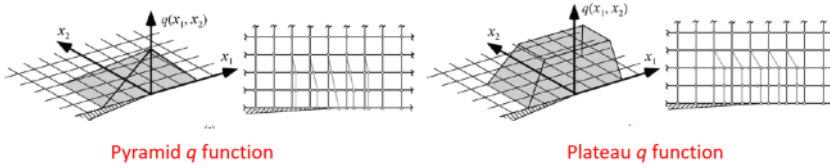
$$J = \int_{A^*} \left[\sigma_{ij} \frac{\partial u_j}{\partial x_i} - w \delta_{ii} \right] \frac{\partial q}{\partial x_i} dA$$



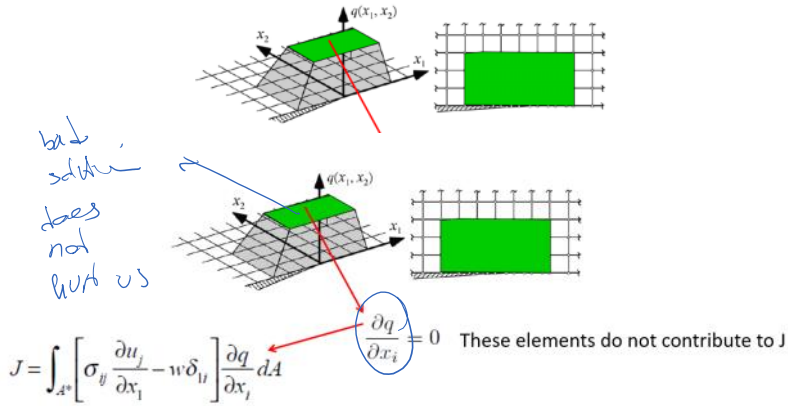
for simplified case

$$J = \int_{A^*} \left[\sigma_{ij} \frac{\partial u_j}{\partial x_i} - w \delta_{ii} \right] \frac{\partial q}{\partial x_i} dA$$

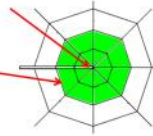
- Shape of decreasing function q :



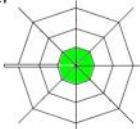
- Plateau q function useful when inner elements are not very accurate: e.g. when singular/quarter point elements are not used



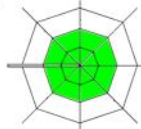
- Since $J_0 \rightarrow 0$ the inner J_0 collapses to the crack tip (CT)
- J_1 will be formed by element edges
- By using **spider web (rozet) meshes** any reasonable number of layers can be used to compute J :



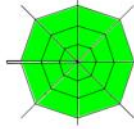
1 layer



2 layer



3 layer



- Spider web (rozet) mesh:
 - One layer of triangular elements (preferably singular, quadrature point elements)
 - Surrounded by quad elements

