

From 11/18/20:

general

$$K = \int_{\xi_1=-1}^1 \int_{\xi_2=-1}^1 \begin{bmatrix} -\frac{(1-\xi_1)}{4} & -\frac{(1-\xi_1)}{4} \\ \frac{(1-\xi_2)}{4} & -\frac{(1+\xi_1)}{4} \\ \frac{(1+\xi_2)}{4} & \frac{(1+\xi_1)}{4} \\ -\frac{(1+\xi_2)}{4} & \frac{(1-\xi_1)}{4} \end{bmatrix} \left( \sigma^T k_{2 \times 2} \sigma^{-1} \det \sigma \right) \begin{bmatrix} -\frac{(1-\xi_2)}{4} & \frac{1-\xi_2}{4} & \frac{1+\xi_2}{4} & -\frac{(1+\xi_2)}{4} \\ -\frac{(1-\xi_1)}{4} & -\frac{1+\xi_1}{4} & \frac{1+\xi_1}{4} & \frac{1-\xi_1}{4} \end{bmatrix} d\xi_1 d\xi_2$$

$\sigma^T k_{2 \times 2} \sigma^{-1} \det \sigma$  (2x2)

$\int_{\xi_1, \xi_2}$

$$\sigma^T k_{2 \times 2} \sigma^{-1} \det \sigma = \frac{8k}{4+\xi_1+\xi_2} \begin{bmatrix} \frac{3+\xi_1}{4} & -\frac{(1+\xi_1)}{4} \\ -\frac{(1-\xi_2)}{4} & \frac{3+\xi_2}{4} \end{bmatrix} \begin{bmatrix} \frac{3+\xi_1}{4} & -\frac{(1-\xi_2)}{4} \\ -\frac{(1+\xi_1)}{4} & \frac{3+\xi_1}{4} \end{bmatrix}$$

$k_{2 \times 2} = k \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$  isotropic (W) for ONLY □

Last time full integration order = 2 in  $\xi_1$  &  $\xi_2$

$\alpha_{\xi_1} = 2, \alpha_{\xi_2} = 2$

$\xi_2$  is const for  $\xi_1$  integral

$$K_{4 \times 4} = \int_{\xi_2=-1}^1 \int_{\xi_1=-1}^1 I(\xi_1, \xi_2) d\xi_1$$

order  $\alpha_{\xi_1} = 2$

Gauss Quad  $\alpha_{\xi_1} = 2 \rightarrow \eta_{\xi_1} = \cos\left(\frac{\alpha_{\xi_1} + 1}{2}\right) = \cos(1.5) = 2$

$$K_{4 \times 4} = \int_{\xi_2=-1}^1 d\xi_2 \left( w_1 \cdot I(\xi_{p1}, \xi_2) + w_2 \cdot I(\xi_{p2}, \xi_2) \right)$$

$\int(\xi_2)$  is 2nd order in  $\xi_2$

$\int_{-1}^1 \frac{1}{\sqrt{3}}$   
 $\int_{-1}^1 \frac{1}{\sqrt{3}}$

TABLE 5.6 Sampling points and weights in Gauss-Legendre numerical integration (interval -1 to +1)

n	$r_i$	$\alpha_i$
1	0. (15 zeros)	2. (15 zeros)
2	$\pm 0.57735$ 0.2691 89626	1.00000 00000 00000
3	$\pm 0.77459$ 66692 41483 0.00000 00000 00000	0.55555 55555 55556 0.88888 88888 88889
4	$\pm 0.86113$ 63115 94053 $\pm 0.33998$ 10435 84856	0.34785 48451 37454 0.65214 51548 62546
5	$\pm 0.90617$ 98459 38664 $\pm 0.53846$ 93101 05683 0.00000 00000 00000	0.23692 68850 56189 0.47862 86704 99366 0.56888 88888 88889
6	$\pm 0.93246$ 95142 03152 $\pm 0.66120$ 93864 66265 $\pm 0.23861$ 91860 83197	0.17132 44923 79170 0.36076 15730 48139 0.46791 39345 72691

$\alpha_{\xi_2} = 2 \rightarrow \eta_{\xi_2} = \cos\left(\frac{1+2}{2}\right) = 2$

$$= \omega_1 \mathcal{J}(f_2 = f_{q_{p_1}}) + \omega_2 \mathcal{J}(f_2 = f_{q_{p_2}})$$

replace for  $\mathcal{J}$

→

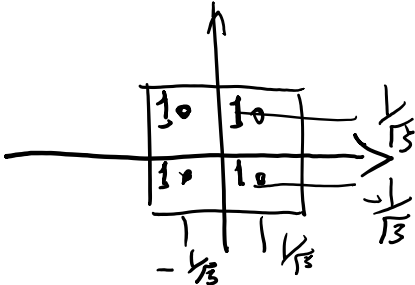
$$K = \omega_1^2 \mathcal{I}(f_{q_{p_1}}, f_{q_{p_1}}) + \omega_1 \omega_2 \mathcal{I}(f_{q_{p_1}}, f_{q_{p_2}})$$

$$+ \omega_2 \omega_1 \mathcal{I}(f_{q_{p_2}}, f_{q_{p_1}}) + \omega_2^2 \mathcal{I}(f_{q_{p_2}}, f_{q_{p_2}})$$

$\omega_1 = \omega_2 = 1$

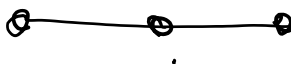
$f_{q_{p_1}} = -\frac{1}{\sqrt{3}}, f_{q_{p_2}} = \frac{1}{\sqrt{3}}$

4pt full  
Quad scheme



what if we had used NC?

$$n_{f_1} = 2 \rightarrow n_{f_2} = 2 + 1 = 3$$

$$f_{q_{p_1}} = -1 \quad f_{q_{p_2}} = 0 \quad f_{q_{p_3}} = 1$$


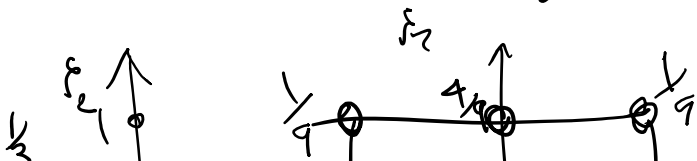
$$\omega_1 = 2 \times \frac{1}{6} \quad \omega_2 = 2 \times \frac{4}{6} \quad \omega_3 = 2 \times \frac{1}{6} \quad L_f = 2$$

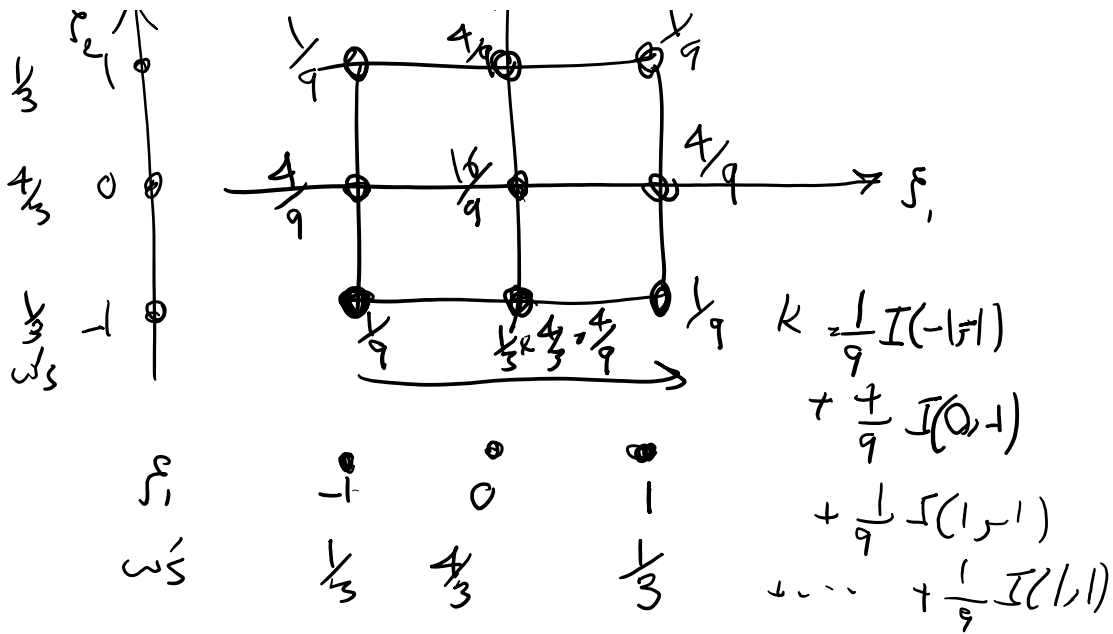
same applies in  $f_2$  direction

$$f_{q_{p_1}} = -1 \quad f_{q_{p_2}} = 0 \quad f_{q_{p_3}} = 1$$

$$\omega_1 = \frac{1}{3} \quad \omega_2 = \frac{4}{3} \quad \omega_3 = \frac{1}{3}$$

very much like Gauss Quad example  
Quad schemes "multiply each other"

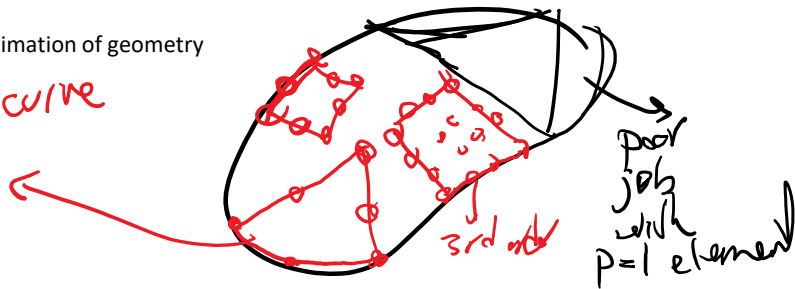




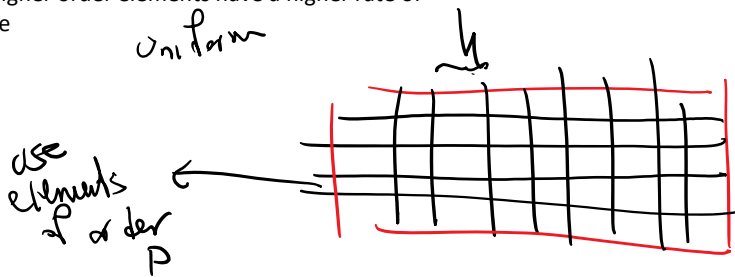
Higher order elements in 2D and 3D. Motivation:

Reason 1: better approximation of geometry

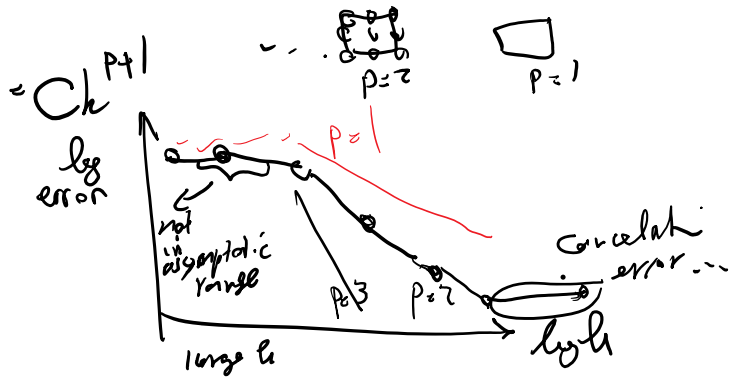
2nd order curve  
parabola  
for  $p=2$

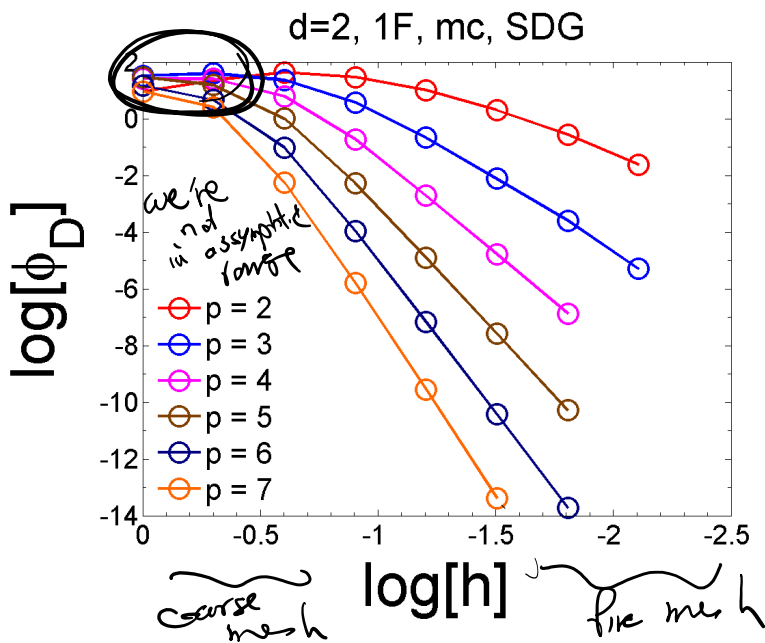


Reason 2: Higher order elements have a higher rate of convergence



$\|u_h - u\|_2 = C h^{p+1}$   
 log error =  $C \underbrace{(p+1)}_{\text{slope}} \log h$





If the solution is sufficiently smooth (more on this below) for low accuracy solutions low order FEM can be more efficient (lowers wall clock time for the same accuracy) whereas for high accuracy solutions often higher order FEMs are more economical.

Lohner\_2011\_Error\_and\_work\_estimates\_for\_high\_order\_elements

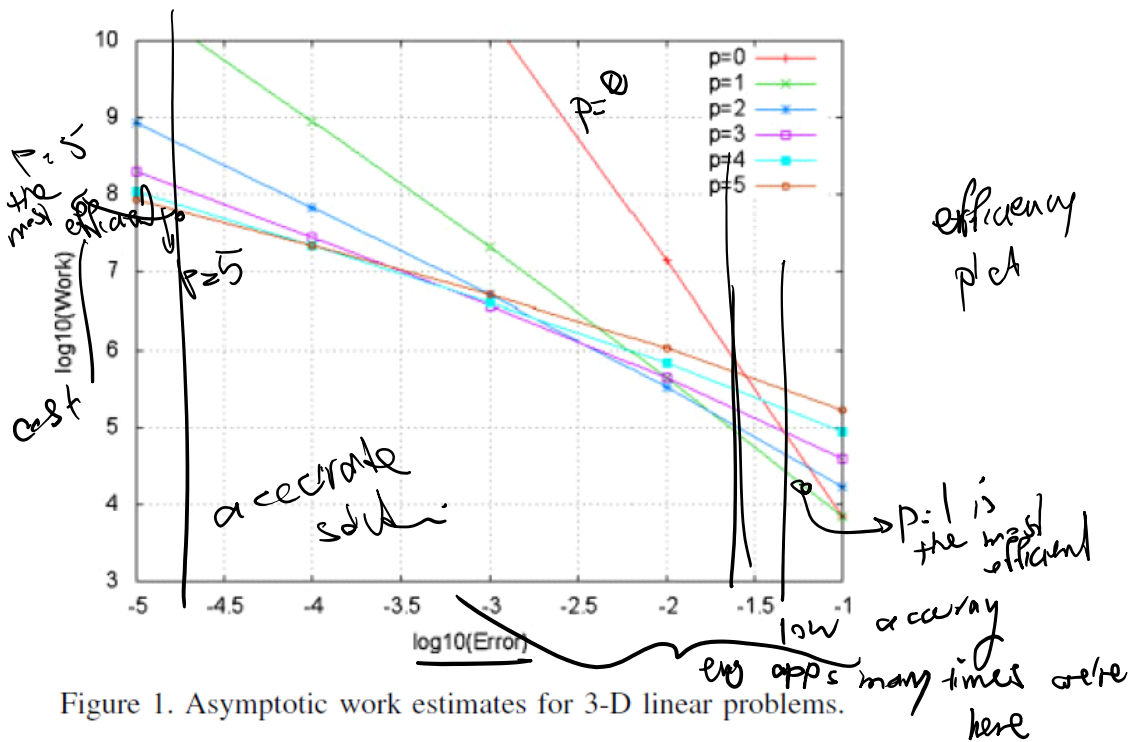


Figure 1. Asymptotic work estimates for 3-D linear problems.

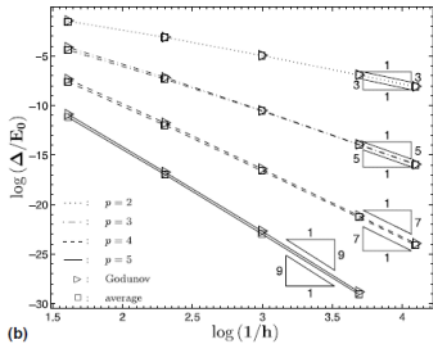
2nd point about efficiency is the regularity of solution

$$\|e^h - u_{\text{exact}}\|_h = C h^{N_u(p,s) + 1}$$

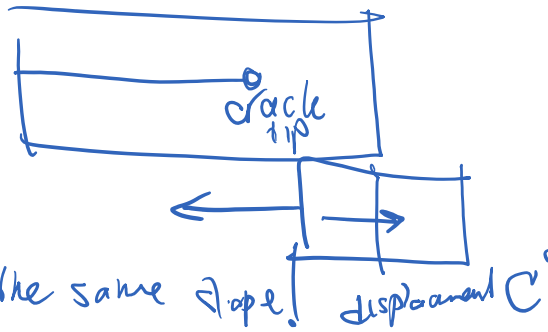
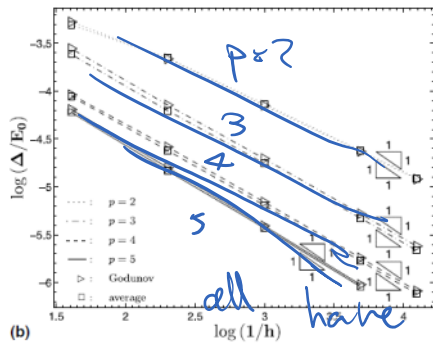
$N_u(p,s)$   
 $\downarrow$   
 reg.

$$\|u_h - u_{\text{exact}}\|_2 = C h^p$$

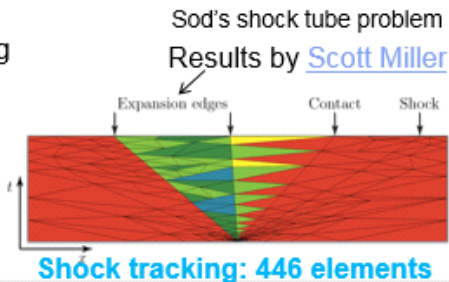
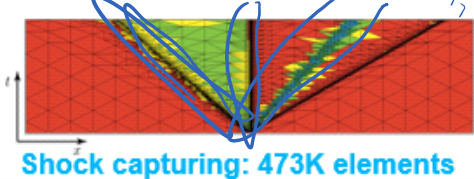
$\downarrow$   
 regularity  
 of the exact solution



Smooth exact soln  
C<sub>s</sub> x 5m x

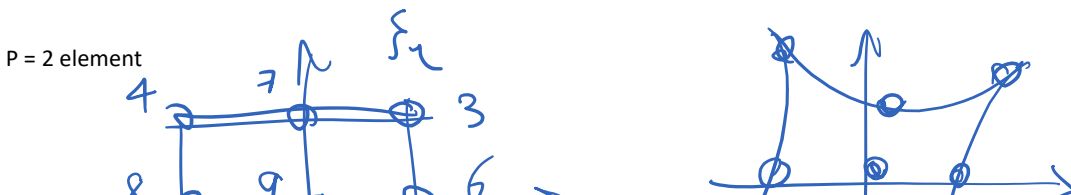


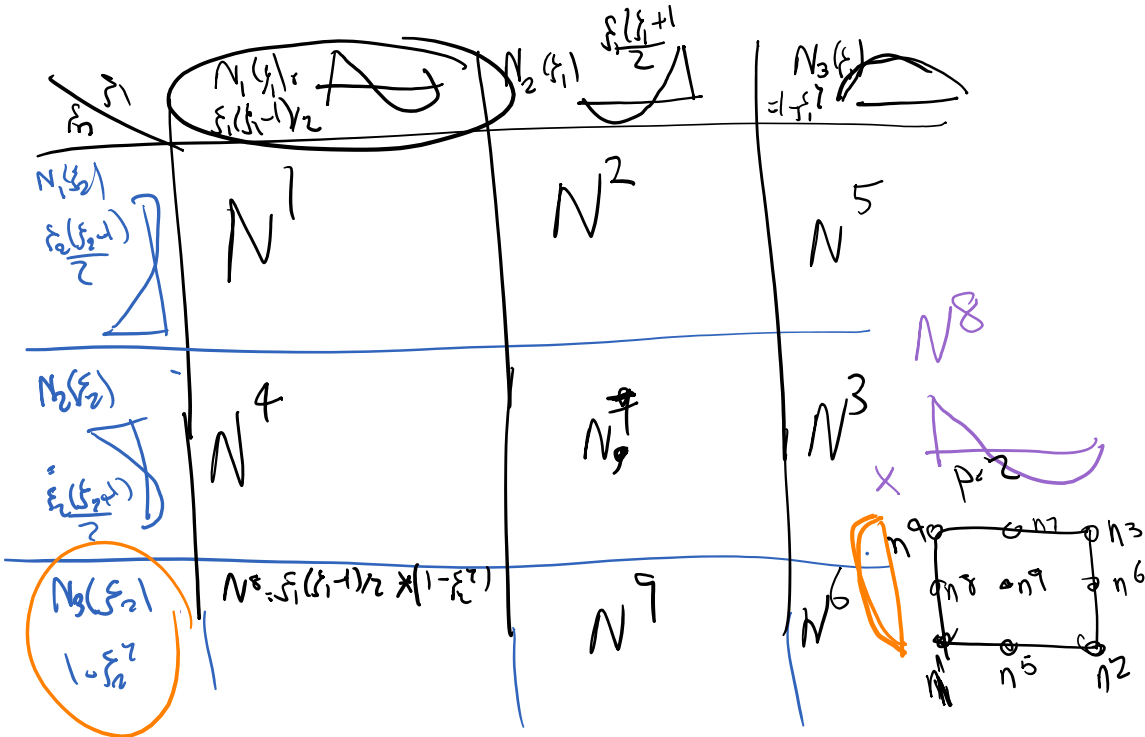
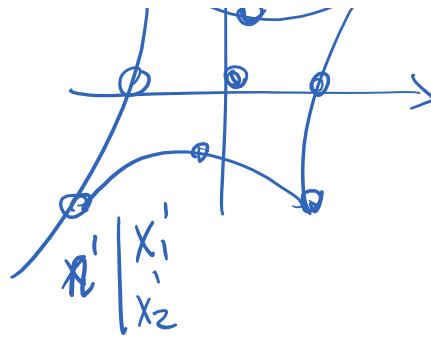
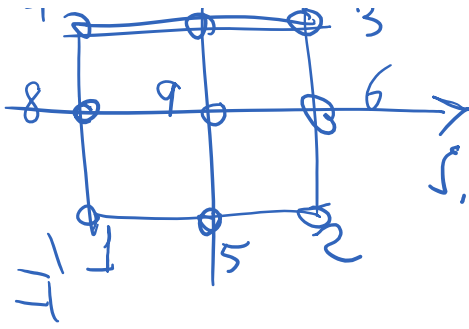
- Adaptive operations in spacetime:
  - Front-tracking better than shock capturing
  - hp-adaptivity better than h-adaptivity



Message: when the solution is nonsmooth (shocks, crack tip fields, etc) higher order elements do not result in higher convergence rate ->

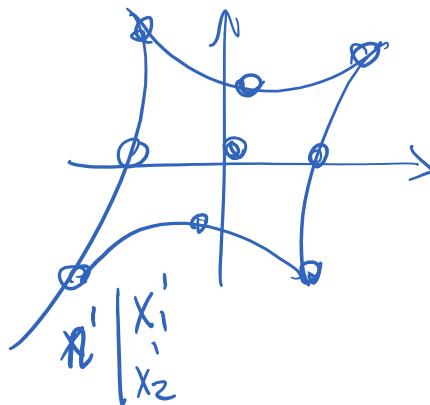
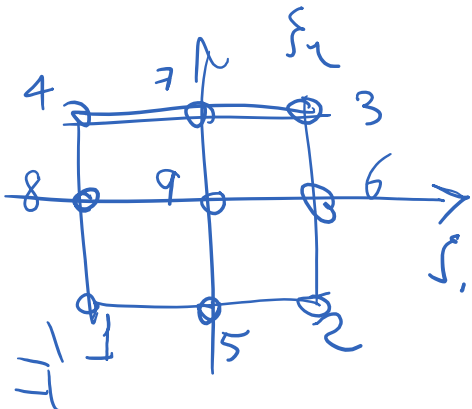
- The method may be more efficient with lower order element there.
- In nonlinear problems (e.g. fluids) the method may not even work if high order elements are used in the shock, ...





Geometry

Isoparametric formulation:



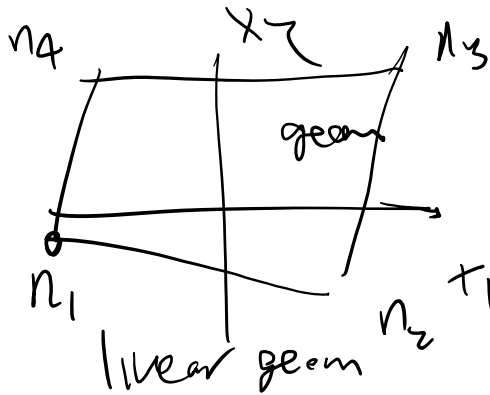
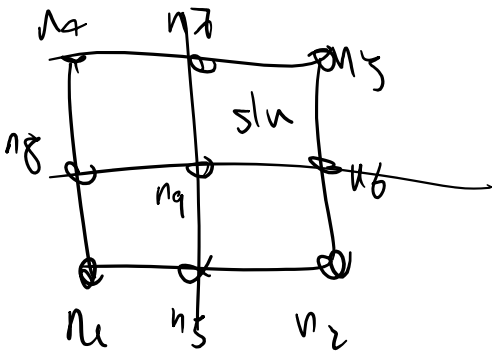
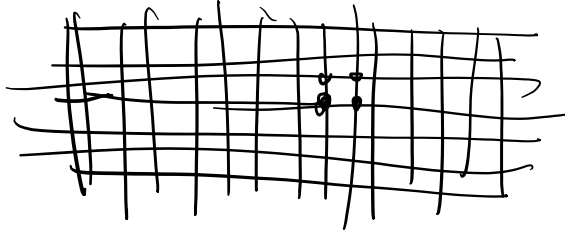
$$T(\xi, \eta) = T^1 N^1(\xi, \eta) + \dots + T^9 N^9(\xi, \eta)$$

iso geometry is the same

$$\mathcal{X}_1(\xi_1, \xi_2) = X_1^1 N^1(\xi_1, \xi_2) + \dots + X_1^9 N^9(\xi_1, \xi_2)$$

Same for  $X_2$

$$X_2 \quad , \quad X_2^1 \quad , \quad X_2^9 \quad ,$$



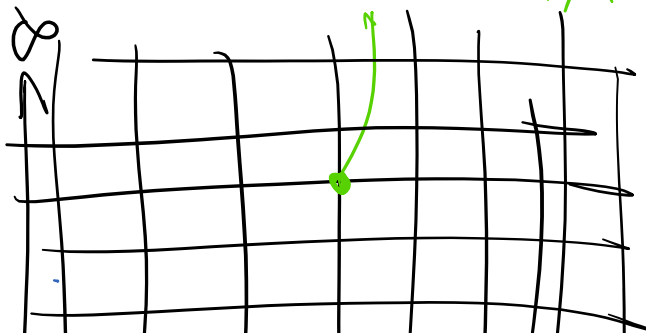
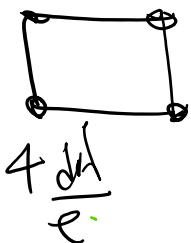
$$T = \sum_{i=1}^4 N^i(\xi_1, \xi_2)$$

$$X_i = \sum_{j=1}^4 X_i^j (N^j)^{P=1}(\xi_1, \xi_2)$$

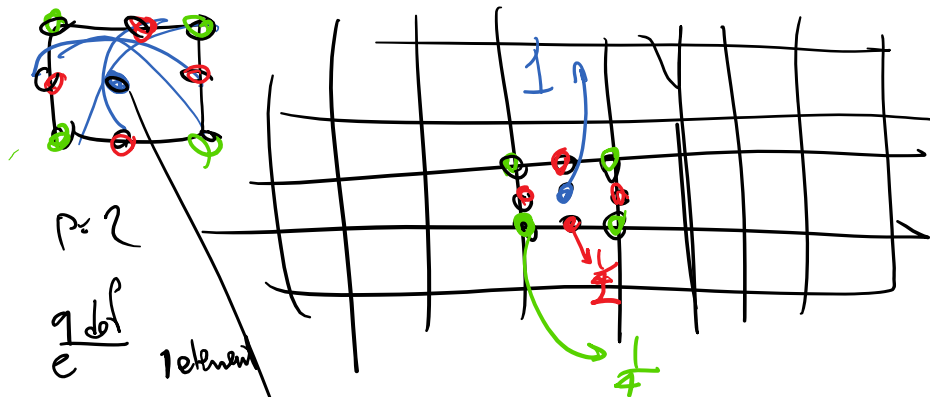
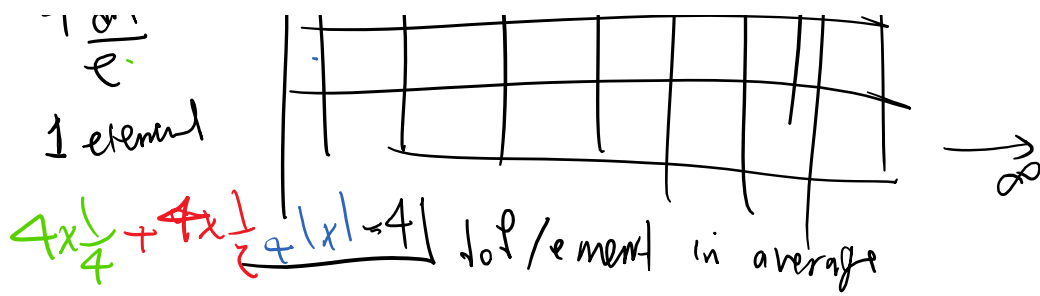
Subparametric formula

HW

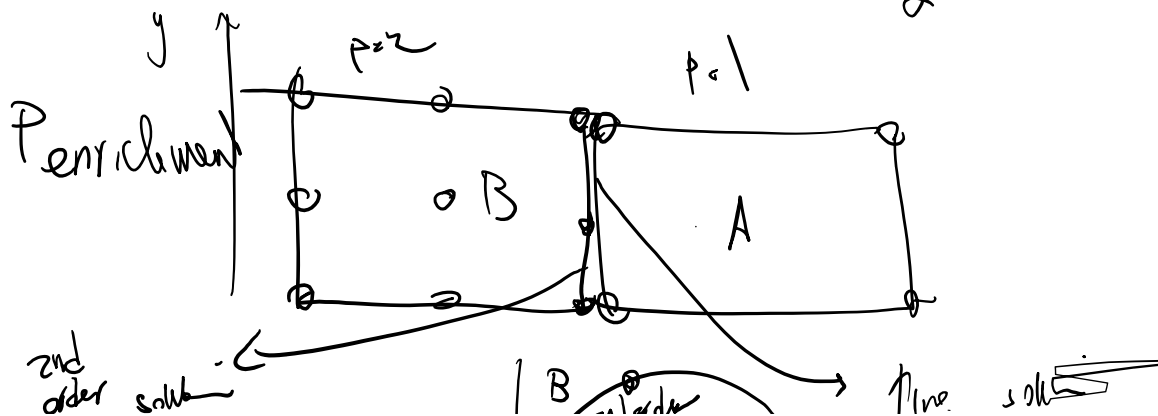
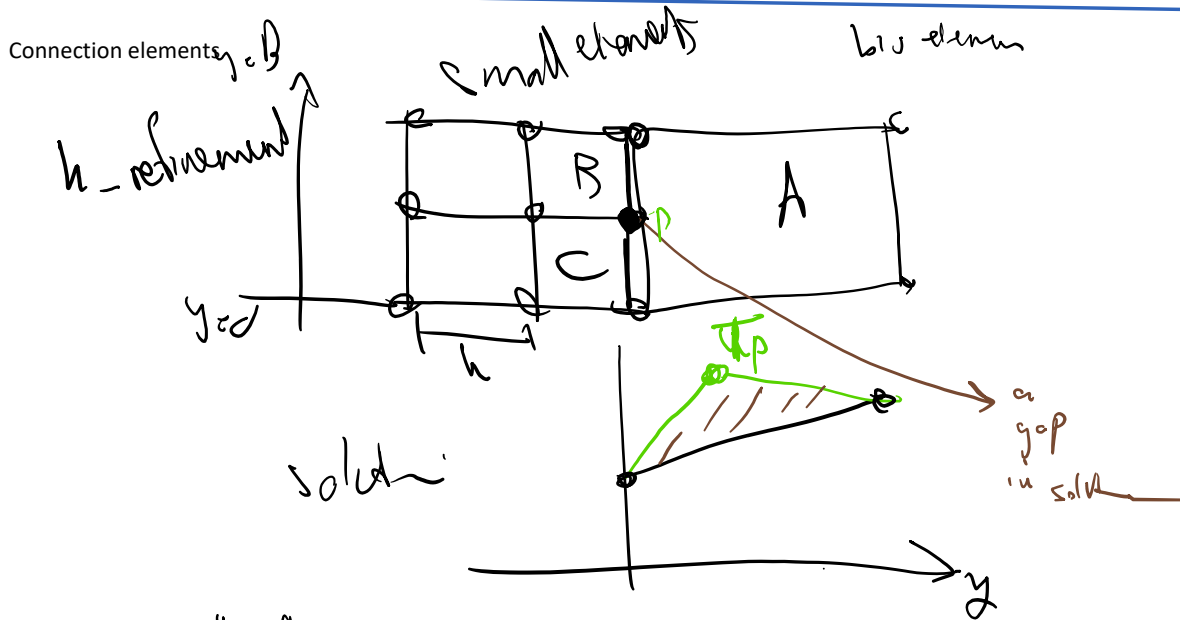
I'll ask you to compute average dof  
it's shared by 4 element



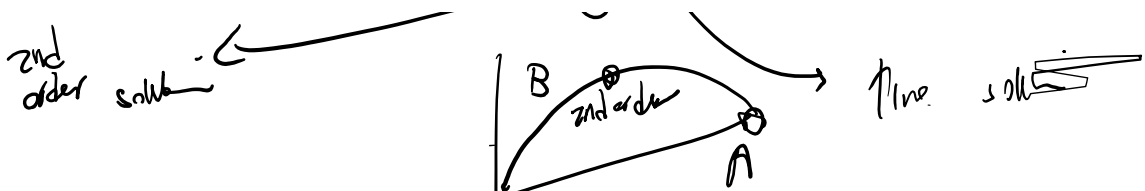
$$4 \times \frac{1}{4} = 1$$



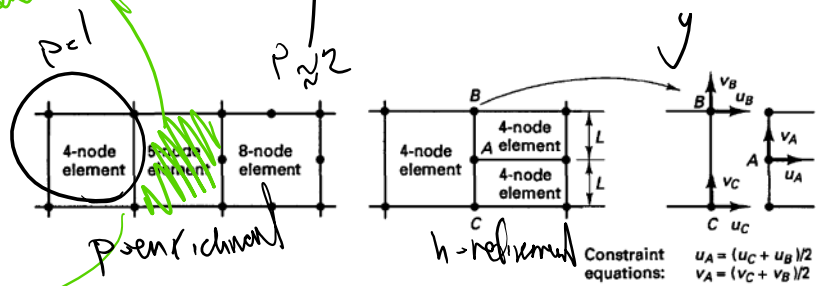
we can get rid of this by static condensation





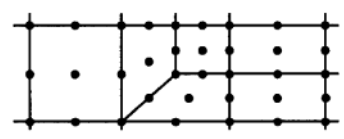


5 node transition element



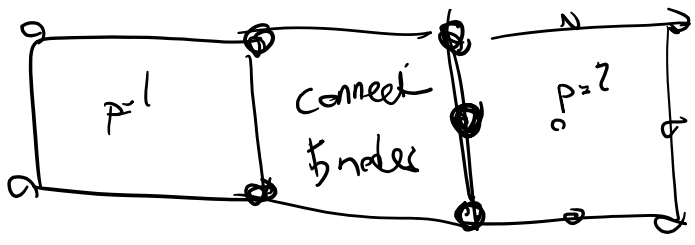
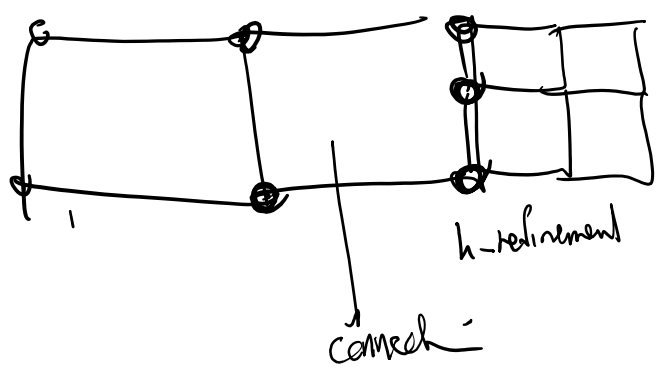
(a) 4-node to 8-node element transition region

(b) 4-node to 4-node element transition; from one to two layers



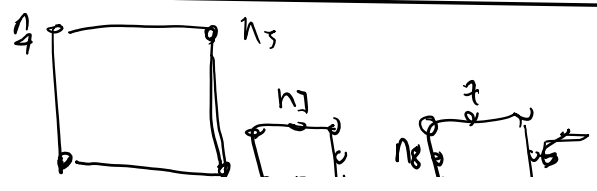
(c) 9-node to 9-node element transition region; from one to two layers

in CFEM to change  $h$  or  $p$  we generally need connective elements



How do we form the shape functions for these connective elements?

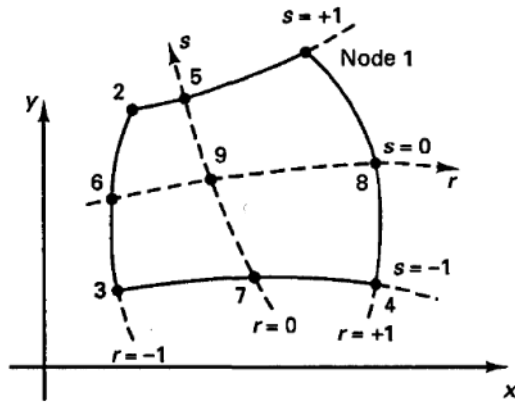
Idea: start from linear elements



Idea: start from linear elements

		5 node element	6 node element	7 node	
	$\frac{(1-\xi_1)(1-\xi_2)}{4}$	$-\frac{1}{2} N_5$	—	—	$\frac{1}{2} N_8$
	$\frac{(1+\xi_1)(1-\xi_2)}{4}$	$-\frac{1}{2} N_5$	$-\frac{1}{2} N_6$	—	—
	$\frac{(1+\xi_1)(1+\xi_2)}{4}$	—	$-\frac{1}{2} N_6$	$-\frac{1}{2} N_7$	—
	$\frac{(1-\xi_1)(1+\xi_2)}{4}$	—	—	$-\frac{1}{2} N_7$	$\frac{1}{2} N_8$
	$\frac{(1-\xi_1^2)\xi_2(\xi_2+1)}{2}$	—	—	—	$\frac{1}{2} N_8$
	$\frac{(1-\xi_2^2)\xi_1(\xi_1+1)}{2}$	—	—	—	$\frac{1}{2} N_8$

$N_5 = (1 - \xi_1^2) \left[ \xi_2 \frac{(1 + \xi_2)}{2} \right]$



(a) 4 to 9 variable-number-nodes two-dimensional element

Include only if node  $i$  is defined

	$i = 5$	$i = 6$	$i = 7$	$i = 8$	$i = 9$
$h_1 = \frac{1}{4}(1+r)(1+s)$	$-\frac{1}{2}h_5$			$-\frac{1}{2}h_8$	$-\frac{1}{4}h_9$
$h_2 = \frac{1}{4}(1-r)(1+s)$	$-\frac{1}{2}h_5$	$-\frac{1}{2}h_6$			$-\frac{1}{4}h_9$
$h_3 = \frac{1}{4}(1-r)(1-s)$		$-\frac{1}{2}h_6$	$-\frac{1}{2}h_7$		$-\frac{1}{4}h_9$
$h_4 = \frac{1}{4}(1+r)(1-s)$			$-\frac{1}{2}h_7$	$-\frac{1}{2}h_8$	$-\frac{1}{4}h_9$
$h_5 = \frac{1}{2}(1-r^2)(1+s)$					$-\frac{1}{2}h_9$
$h_6 = \frac{1}{2}(1-s^2)(1-r)$					$-\frac{1}{2}h_9$
$h_7 = \frac{1}{2}(1-r^2)(1-s)$					$-\frac{1}{2}h_9$
$h_8 = \frac{1}{2}(1-s^2)(1+r)$					$-\frac{1}{2}h_9$
$h_9 = (1-r^2)(1-s^2)$					

(b) Interpolation functions