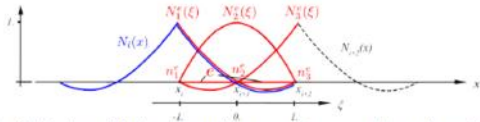


Element shape functions to global shape functions

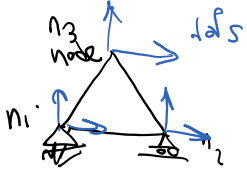


- While the global view of finite element has some advantages in mathematical analysis, we often form the shape functions at the local level and if needed form global shape functions.
- It was this local perspective that first was employed in engineering finite element analysis.
- For example, in the figure the 1D bar element has **three nodes with one being internal node** and has **interpolation order $p = 2$** .
- We observe that,

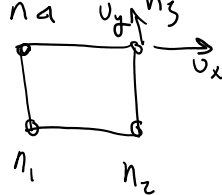
$$N_i^e(n_j^e) = \delta_{ij} \Rightarrow N_I(n_J) = \delta_{IJ}$$
 which was the condition we first stipulated for finite elements in global view.
- As an example, we observe that the global shape function $N_i(x)$ is formed from local element shape functions.
- Notice that while local element order is $p = 2$ the global shape functions are still C^0 (piece-wise quadratic in this case).
- Elements can have internal nodes. This generally occurs for higher than linear elements ($p > 1$).

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Nodes and dofs are distinct. In many problems there are more than 1 dof / node



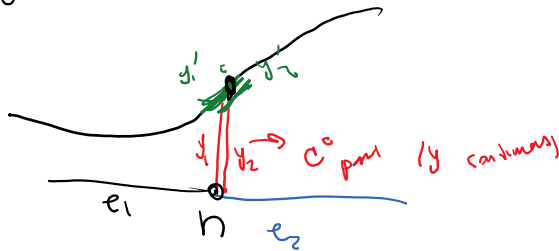
2 dofs/node



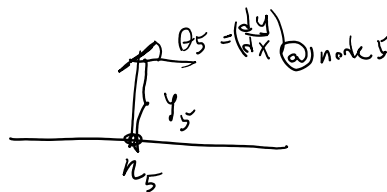
2 dofs/node
 ↓
 displacement
 2D elasticity

2D / 3D problems

beam: PDE $(EI y'')'' + q = 0$ $M = 4 \rightarrow m = 2$ $C^{m-1} = C^1$
 Recall $\int w^T E I y''$...



2 dofs per node



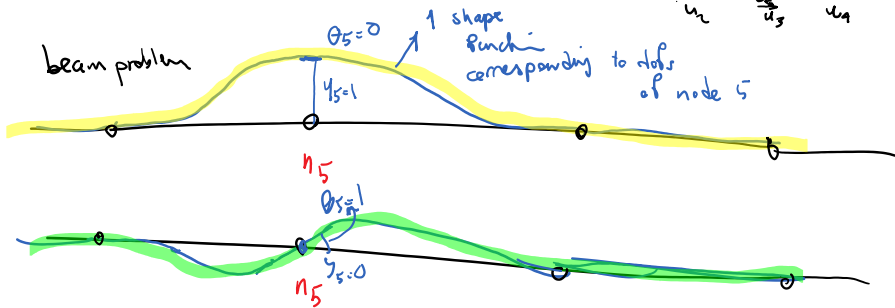
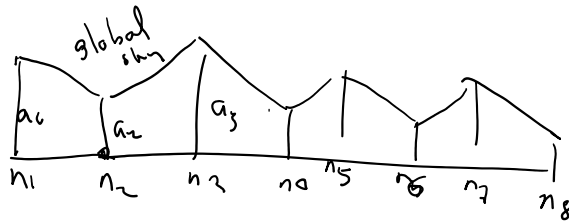
C^1
 continuity needed

$m > 1$

is shape function \downarrow @ one \times and zero @ other \times s

other X_s

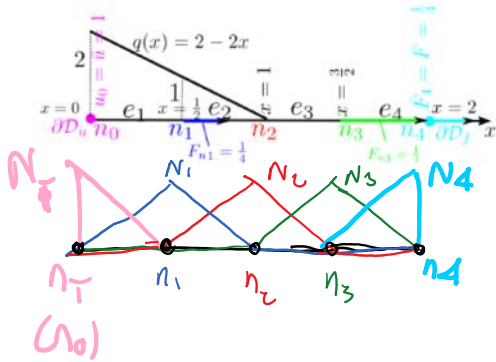
- ① X_i : dof
- ② X_i : node



all dofs are zero except 1st dof of node 5

all dofs are zero except 2nd dof of node 5

We solved this problem using the global approach:



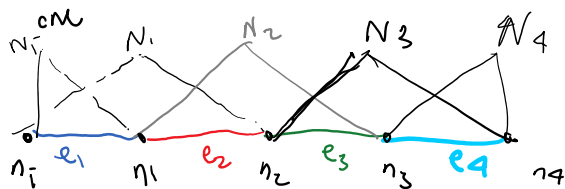
Global or node/dof centered

You are not going to use this anymore because it's cumbersome

$$K = \int_0^2 B^T B dx \rightarrow K_{12} = \int_0^2 B_1^T E A B_2 dx = \int_0^2 B_1 B_2 dx$$

$$K_{11} = \int_{e_1} B_1 B_1 dx + \int_{e_2} B_1 B_1 dx$$

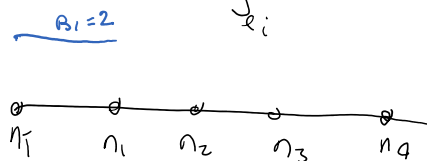
in the "local" or "element-centered" approach we take care of all things pertained to an element and then move to the next



$$K = \int B^T B dx = K_{e1} + K_{e2} + K_{e3} + K_{e4}$$

$$K_{e_i} = \int_{e_i} B^T B dx$$

$$K_{e1} = \int_{e_1} \begin{bmatrix} B_1 \\ B_2 \\ B_3 \\ B_4 \end{bmatrix} \begin{bmatrix} B_1 & B_2 & B_3 & B_4 \end{bmatrix} dx = \int_{e_1} \begin{bmatrix} 2 \\ 0 \\ 0 \\ 0 \end{bmatrix} \begin{bmatrix} 2 & 0 & 0 & 0 \end{bmatrix} dx = \begin{bmatrix} 2 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

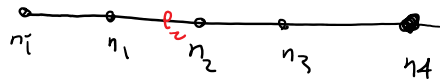


$B_2=2$

$$= \int_{e_1} \begin{pmatrix} 1 \\ 0 \\ 0 \\ 0 \end{pmatrix} [2 \ 0 \ 0 \ 0] = \begin{pmatrix} 2 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

$$K_{e_2} = \int_{e_2} \begin{pmatrix} B_1 \\ B_2 \\ B_3 \\ B_4 \end{pmatrix} [B_1 \ B_2 \ B_3 \ B_4] dx =$$

$$B_2 = 2$$



$$\int_{e_2} \begin{pmatrix} -2 \\ 2 \\ 0 \\ 0 \end{pmatrix} [2 \ 2 \ 0 \ 0] dx = \begin{pmatrix} 2 & -2 & 0 & 0 \\ -2 & 2 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

$$B_1 = -2$$

$$B_3 = 2$$

$$K_{e_3} = \int_{e_3} B^T B = \int_{e_3} \begin{pmatrix} 0 \\ -2 \\ 2 \\ 0 \end{pmatrix} [0 \ -2 \ 2 \ 0] = \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & 2 & -2 & 0 \\ 0 & -2 & 2 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

$$B_1 = -2$$

$$B_4 = 2$$

$$K_{e_4} = \int_{e_4} B^T B = \int_{e_4} \begin{pmatrix} 0 \\ 0 \\ -2 \\ 2 \end{pmatrix} [0 \ 0 \ -2 \ 2] = \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 2 & -2 \\ 0 & 0 & -2 & 2 \end{pmatrix}$$

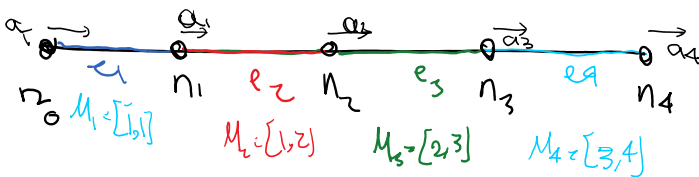
$$B_3 = -2$$

$$K = K_{e_1} + K_{e_2} + K_{e_3} + K_{e_4} = \begin{pmatrix} 2+2 & -2 & & \\ -2 & 2+2 & -2 & \\ & -2 & 2+2 & -2 \\ & & -2 & 2 \end{pmatrix}$$

$$K = \begin{pmatrix} 4 & -2 & & \\ -2 & 4 & -2 & \\ & -2 & 4 & -2 \\ & & -2 & 2 \end{pmatrix}$$

To fully utilize element-centered approach we define 2 maps

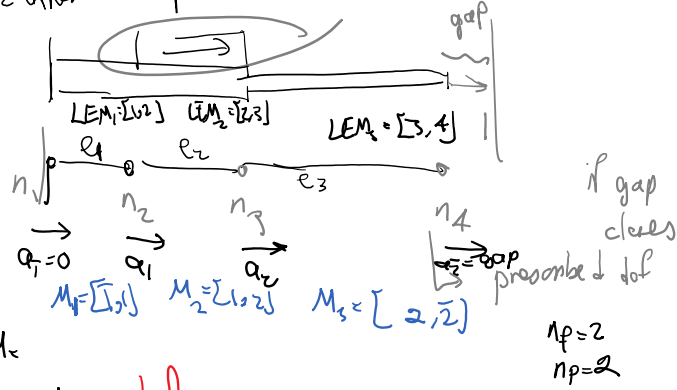
$$LEM_1 = [0,1] \quad LEM_2 = [1,2] \quad LEM_3 = [2,3] \quad LEM_4 = [3,4]$$



there are
 - 4 free d.o.f ($ch_f = 4$)
 - 1 prescribed d.o.f ($ch_p = 1$)

M_e or dof is the map of element dofs

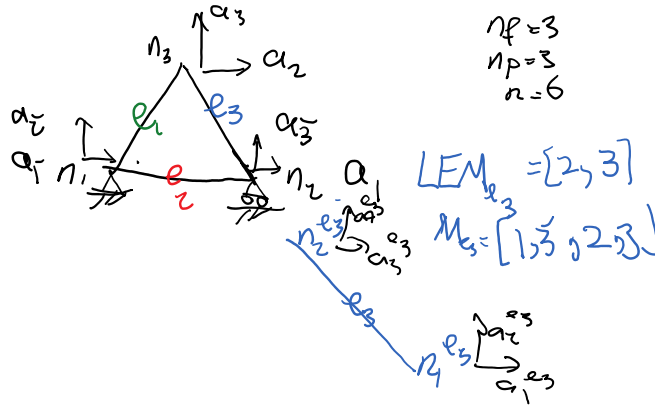
2 dbar example



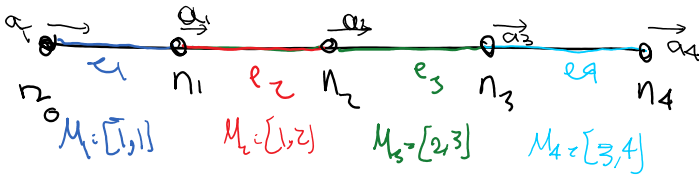
element **nodal** map

M element dof map

we'll use this now

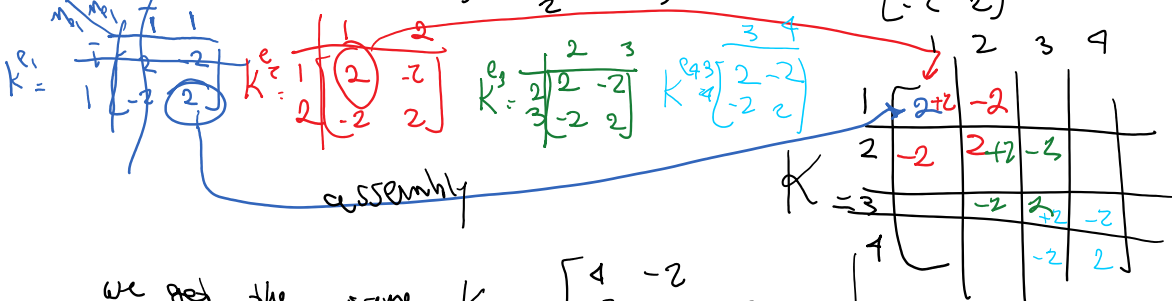


example map $n=6$ utilize element-centered app
 $LEM_1=[1,1]$ $LEM_2=[1,2]$ $LEM_3=[2,3]$ $LEM_4=[3,4]$



we'll show
$$K^e = \frac{(EA)^e}{L^e} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

for all elements here $EA=1, L=\frac{1}{2} \rightarrow k^1 = \dots = k^4 = \begin{bmatrix} 2 & -2 \\ -2 & 2 \end{bmatrix}$



we add the ... $\begin{bmatrix} 4 & -2 \\ -2 & 2 \end{bmatrix}$

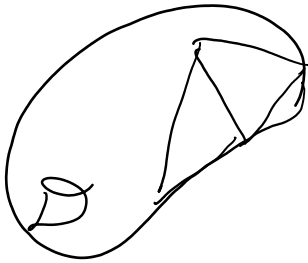
we get the same $K = \begin{bmatrix} 4 & -2 & & & & \\ -2 & 4 & -2 & & & \\ & -2 & 4 & -2 & & \\ & & -2 & 4 & -2 & \\ & & & -2 & 4 & -2 \\ & & & & -2 & 4 \end{bmatrix}$

we'll discuss this next

$$f_D^e = k a^e$$

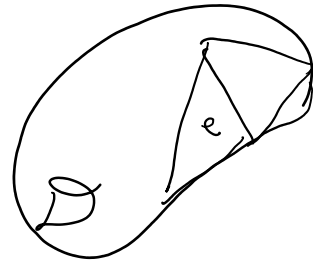
Global Approach

$$K = \int_{\mathcal{D}} B^T D B dv$$



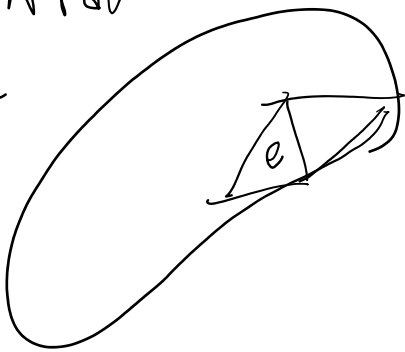
Local (element) approach

$$k^e = \int_e B^{eT} D B^e dv$$



$$F = \underbrace{(f_r + f_N - f_D)}_{\text{Element contributions } F_e} + f_n \downarrow \text{nodal forces}$$

$$f_r = \int_{\mathcal{D}} N^T r dv$$

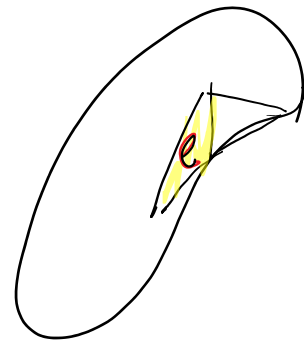


$$F = F^e + f^n$$

$$f^e = f_r^e + f_N^e - f_D^e$$

↪ "assembled" to F_e

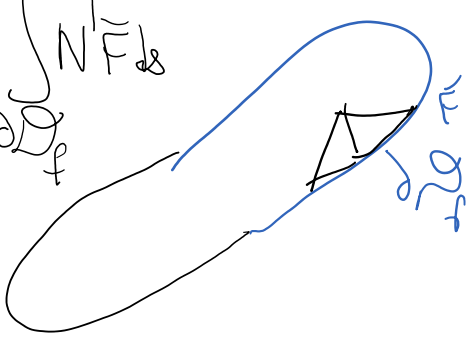
$$f_r^e = \int_e N^{eT} r dv$$

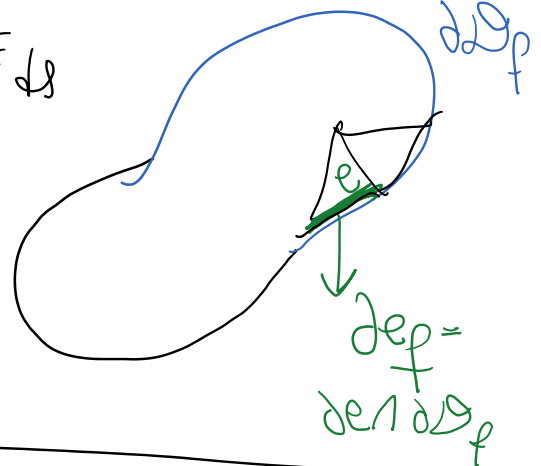


$$F_i = \int_{\mathcal{D}} N_i^T r dv$$

$$f_{n,i}^e = \int_e N_i^{eT} r dv$$

$d\mathcal{D}_p$

$$\mathbf{F}_N = \int_{\partial\Omega_f} \mathbf{N}^T \mathbf{F} d\Omega$$


$$f_N^{pe} = \int_{\partial\Omega_f} \mathbf{N}^e \mathbf{T}^T \mathbf{F} d\Omega$$


$$\mathbf{F}_D = \mathbf{K}_{fp} \mathbf{a}_p$$

$$\mathbf{K}_{fp} = \int_{\Omega} \mathbf{B}_f^T \mathbf{D} \mathbf{B}_p dV$$

$$f_D = \mathbf{k}^e \mathbf{a}$$

very simple
😊